



PLACER COUNTY WATER AGENCY
SINCE 1957

BOARD OF DIRECTORS

Gray Allen, District 1
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BUSINESS CENTER

144 Ferguson Road
MAIL
P.O. Box 6570
Auburn, CA 95604
PHONE
(530) 823-4850
(800) 464-0030
WWW.PCWA.NET

Andrew Fecko, General Manager

June 5, 2026

Jane Ling
State Water Resources Control Board
Division of Water Rights
Water Rights Permitting Unit
P.O. Box 2000
Sacramento, CA 95814

SUBJECT: Placer County Water Agency Permit No. 13856 (Application No. 18085)
2026 Petition for Change Involving Water Transfers

Dear Mr. McFarland,

Placer County Water Agency (PCWA) hereby submits to the State Water Resources Control Board (SWRCB) Division of Water Rights a Petition for Change Involving Water Transfers (Petition) to facilitate a 21,053 acre foot (ac-ft) water transfer (Transfer) to Westlands Water District (WWD) pursuant to Water Code §1725-1732. This transfer would involve surplus water currently stored in PCWA's Middle Fork Project reservoirs pursuant to SWRCB water right Permit No. 13856.

In accordance with Water Code §1728, this Transfer shall occur within one year from the date of approval by the SWRCB. Transfer releases to WWD would be initiated following approval of the Petition by SWRCB and shall be completed prior to November 30, 2026. As shown in Attachment G, the timing and volume of the proposed Transfer will have a beneficial effect on in-stream flows and water temperature in the Lower American River. In addition, the release of Transfer water will provide additional energy generation for the California Independent System Operator to management the electrical grid. This Transfer involves water that would not otherwise be released from storage by PCWA but for the purpose of this Transfer.

The attached petition includes all of the information required under Water Code §1725-1732 to demonstrate that this transfer will not injure any downstream legal user of water and would not unreasonably affect fish, wildlife, or any other in-stream beneficial uses.

Enclosed with this submittal are the following:

- One original and one copy of PCWA's Petition for Change Involving Water Transfers (dated June 5, 2026) including the required Environmental Information Form for Petitions (Attachment A);
- A check in the amount of \$12,521.50 made payable to the State Water Board for Petition filing fees; and
- A check in the amount of \$850 made payable to the California Department of Fish & Wildlife.

PCWA would like to thank SWRCB staff for their continued diligence and expeditious processing of Change Petitions. PCWA is available to assist SWRCB staff with any technical or administrative functions needed to complete the approval process.

If you have any questions or need additional information, please call me at (530) 823-4891. Alternatively, you can reach PCWA's point of contact for water transfers, Benjamin Barker, at (530) 823-1742.

Sincerely,



Darin Reintjes
Director of Resource Management

Enclosures

c: Andrew Fecko, General Manager, Placer County Water Agency
Katarina Campbell, Deputy General Manager - Resources, Westlands Water District
Russ Freeman, Deputy General Counsel, Westlands Water District
Lynn Coster, Program Manager, CVRWQCB Water Quality Certification Division
Morgan Kilgour, Regional Manager - R2, California Department of Fish and Wildlife
Placer County Board of Supervisors
Fresno County Board of Supervisors
Kings County Board of Supervisors

VENDOR NUMBER	VENDOR NAME	CHECK NUMBER	CHECK DATE	CHECK AMOUNT
1731	STATE WATER RESOURCES CONTROL BOARD	208750	05/28/2026	\$12,521.50
INVOICE DATE	INVOICE NUMBER	DESCRIPTION	INVOICE AMOUNT	
05/27/2026	26TRANSFERWESTLANDS	PERMIT FEES	\$12,521.50	

PCWA

Water • Energy • Stewardship

THIS CHECK IS VOID WITHOUT A GREEN BACKGROUND ON THE FRONT AND A TRUE DIAMOND PATTERN & AN ARTIFICIAL FINGERPRINT WATERMARK ON THE BACK



Placer County Water Agency
PO Box 6570
Auburn, CA 95604-6570
530-823-4850

US Bank
Auburn Office
Auburn, CA 95603

Vendor Number
1731

Check Number
208750

Check Date
05/28/2026

VOID 180 DAYS FROM DATE OF ISSUE

*** Twelve Thousand Five Hundred Twenty-One Dollars And Fifty Cents ***

\$12,521.50

Pay To
The
Order Of

STATE WATER RESOURCES CONTROL BOARD
PO BOX 1888
SACRAMENTO, CA 95812-1888

Carrie Parn
Authorized Signature

MP

[Signature]
Authorized Signature

MP

SIGNATURE AREA CONTAINS A KNIGHT & FINGERPRINT CHECK WORDING

⑈00208750⑈ ⑆121122676⑆157531565461⑈

VENDOR NUMBER	VENDOR NAME	CHECK NUMBER	CHECK DATE	CHECK AMOUNT
2649	DEPT OF FISH & WILDLIFE	208683	05/28/2026	\$850.00
INVOICE DATE	INVOICE NUMBER	DESCRIPTION	INVOICE AMOUNT	
05/27/2026	26TRANFERF&W	PERMIT FEES	\$850.00	

PCWA

Water • Energy • Stewardship

THIS CHECK IS VOID WITHOUT A GREEN BACKGROUND ON THE FRONT AND A TRUE DIAMOND PATTERN & AN ARTIFICIAL FINGERPRINT WATERMARK ON THE BACK



Placer County Water Agency

PO Box 6570

Auburn, CA 95604-6570

530-823-4850

US Bank
Auburn Office
Auburn, CA 95603

Vendor Number

2649

Check Number

208683

Check Date

05/28/2026

VOID 180 DAYS FROM DATE OF ISSUE

*** Eight Hundred Fifty Dollars And Zero Cents ***

\$850.00

Pay To
The
Order OfDEPT OF FISH & WILDLIFE
1701 NIMBUS ROAD STE A
RANCHO CORDOVA, CA 95670

Carrie Parns

Authorized Signature

MP

Authorized Signature

MP

SIGNATURE AREA CONTAINS A KNIGHT & FINGERPRINT CHECK WORDING

⑈00208683⑈ ⑆121122676⑆157531565461⑈

Please indicate County where
your project is located here:

PLACER

MAIL FORM AND ATTACHMENTS TO:
State Water Resources Control Board
DIVISION OF WATER RIGHTS
P.O. Box 2000, Sacramento, CA 95812-2000
Tel: (916) 341-5300 Fax: (916) 341-5400
<http://www.waterboards.ca.gov/waterrights>

PETITION FOR CHANGE INVOLVING WATER TRANSFERS

Separate petitions are required for each water right. Mark all areas that apply to your proposed change(s). Incomplete forms may not be accepted. Location and area information must be provided on maps in accordance with established requirements. (Cal. Code Regs., tit. 23, § 715 et seq.) Provide attachments if necessary.

- | | | | |
|---|--|---|---|
| ☐ Point of Diversion
Wat. Code, § 1701 | ☐ Point of Rediversion
Wat. Code, § 1701 | ☐ Place of Use
Wat. Code, § 1701 | ☐ Purpose of Use
Wat. Code, § 1701 |
| ☐ Temporary Urgency
Wat. Code, § 1435 | ☒ Temporary Change
Wat. Code, § 1725 | ☐ Long-term Transfer
Wat. Code, §§ 382, 1735 | ☐ Instream Flow Dedication
Wat. Code, § 1707 |

Application 18085

Permit 13856

License NA

Statement NA

I (we) hereby petition for change(s) noted above and described as follows:

Point of Diversion or Rediversion – Provide source name and identify points using both Public Land Survey System descriptions to ¼-¼ level and California Coordinate System (NAD 83).

Present: Please refer to Attachment A of the attached Environmental Information for Petition.

Proposed: Please refer to Attachment A of the attached Environmental Information for Petition.

Place of Use – Identify area using Public Land Survey System descriptions to ¼-¼ level; for irrigation, list number of acres irrigated.

Present: Please refer to Attachment A of the attached Environmental Information for Petition.

Proposed: Please refer to Attachment A of the attached Environmental Information for Petition.

Purpose of Use

Present: Please refer to Attachment A of the attached Environmental Information for Petition.

Proposed: Please refer to Attachment A of the attached Environmental Information for Petition.

Instream Flow Dedication – Provide source name and identify points using both Public Land Survey System descriptions to ¼-¼ level and California Coordinate System (NAD 83).

Upstream Location: NA

Downstream Location: NA

List the quantities dedicated to instream flow in either: ☐ cubic feet per second or ☐ gallons per day:

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec

Will the dedicated flow be diverted for consumptive use at a downstream location? ☐ Yes ☐ No

If yes, provide the source name, location coordinates, and the quantities of flow that will be diverted from the stream.

Proposed New User(s)

Provide the names, addresses, and phone numbers for all proposed new user(s) of the water right.

Westlands Water District
3130 N. Fresno Street
PO Box 6056
Fresno, CA 93703-6056

Amount of Water to be Transferred

21,053.00 acre-feet will be transferred. If the basis of right is direct diversion, the average rate of diversion for the maximum 30-day period of use is _____ cubic feet per second or million gallons per day.

General Information – Provide the following information, if applicable to your proposed change(s).

Have you attached an analysis which documents that the amount of water to be transferred or exchanged would have been consumptively used or stored in the absence of the proposed temporary change or long-term transfer? ☒ Yes ☐ No

Have you attached an analysis of any changes to streamflow, water quality, timing of diversion or use, return flows, or effects on legal users from the proposed temporary change or long-term transfer? ☒ Yes ☐ No

Have you attached an analysis that shows the proposed temporary change or long-term transfer will not unreasonably affect fish, wildlife, or other instream beneficial uses? ☒ Yes ☐ No

I (we) have access to the proposed point of diversion or control the proposed place of use by virtue of:

☒ ownership ☐ lease ☐ verbal agreement ☐ written agreement

If by lease or agreement, state name and address of person(s) from whom access has been obtained.

PCWA holds ownership of the Point(s) of Diversion pursuant to Water Right Permit 13856 described in the Environmental Information for Petition; by virtue of written agreement with Westlands Water District for the Proposed Place of Use sought by this Petition.

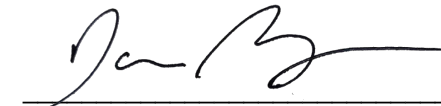
Give name and address of any person(s) taking water from the stream between the present point of diversion or rediversion and the proposed point of diversion or rediversion, as well as any other person(s) known to you who may be affected by the proposed change.

U.S Department of the Interior Bureau of Reclamation; San Juan Water District; Carmichael Water District; County of Sacramento; City of Sacramento

Please refer to Attachment A of the attached Environmental Information for Petition for additional details.

All Right Holders Must Sign Below: I (we) declare under penalty of perjury that this involves only the amount of water which would have been consumptively used or stored in the absence of the proposed temporary change, and that the above is true and correct to the best of my (our) knowledge and belief.

Dated 06/05/2026 at Placer County Water Agency, Auburn, CA .

 Darin Reintjes

Right Holder or Authorized Agent Signature

Right Holder or Authorized Agent Signature

NOTE: All petitions must be accompanied by:

- (1) the form Environmental Information for Petitions, available at:
http://www.waterboards.ca.gov/waterrights/publications_forms/docs/pet_info.pdf
- (2) Division of Water Rights fee, per the Water Rights Fee Schedule, available at:
http://www.waterboards.ca.gov/waterrights/water_issues/programs/fees/
- (3) Department of Fish and Wildlife fee of \$850 (Pub. Resources Code, § 10005)

ENVIRONMENTAL INFORMATION FOR PETITIONS

This form is required for all petitions.

Before the State Water Resources Control Board (State Water Board) can approve a petition, the State Water Board must consider the information contained in an environmental document prepared in compliance with the California Environmental Quality Act (CEQA). This form is not a CEQA document. If a CEQA document has not yet been prepared, a determination must be made of who is responsible for its preparation. As the petitioner, you are responsible for all costs associated with the environmental evaluation and preparation of the required CEQA documents. Please answer the following questions to the best of your ability and submit any studies that have been conducted regarding the environmental evaluation of your project. If you need more space to completely answer the questions, please number and attach additional sheets.

DESCRIPTION OF PROPOSED CHANGES OR WORK REMAINING TO BE COMPLETED

For a petition for change, provide a description of the proposed changes to your project including, but not limited to, type of construction activity, structures existing or to be built, area to be graded or excavated, increase in water diversion and use (up to the amount authorized by the permit), changes in land use, and project operational changes, including changes in how the water will be used. For a petition for extension of time, provide a description of what work has been completed and what remains to be done. Include in your description any of the above elements that will occur during the requested extension period.

Placer County Water Agency (PCWA) proposes to transfer up-to 21,053 acre-feet (AF) of Middle Fork American River Project (MFP) water (Transfer Water) currently stored in Hell Hole Reservoir on the Rubicon River and French Meadows Reservoir on the Middle Fork American River (MFAR) to the Westlands Water District (WWD), for designated beneficial uses within the WWD service area. To accomplish this transfer, the following temporary (one year or less) changes in Place of Use (POU) and Point(s) of Rediversion (PORD) are being sought by Petition pursuant to PCWA Water Right Application 18085 (Permit No. 13856) and consistent with California Water Code §1725-§1732, which includes:

- 1) The temporary addition of United States Department of the Interior Bureau of Reclamation (Reclamation) Central Valley Project (CVP) Bill Jones Pumping Plant (Jones) intake facility and/or the California Department of Water Resources (DWR) State Water Project (SWP) Harvey O. Banks Pumping Plant (Banks) (Attachment B) as Point(s) of Rediversion for WWD to receive PCWA Transfer Water under P13856;
- 2) The temporary addition of San Luis Reservoir (SLR), a Reclamation CVP facility (Attachment B), as a point for the temporary storage and rediversion of Transfer Water by WWD under P13856; and
- 3) The temporary addition of the WWD service area (Attachment C) to P13856 authorizing consumptive and beneficial uses of Transfer Water within the WWD service area.

Explicit details of how the proposed transfer will be executed are contained within Attachments A-G.

Insert the attachment number here, if applicable: A

Coordination with Regional Water Quality Control Board

For change petitions only, you must request consultation with the Regional Water Quality Control Board regarding the potential effects of your proposed change on water quality and other instream beneficial uses. (Cal. Code Regs., tit. 23, § 794.) In order to determine the appropriate office for consultation, see: http://www.waterboards.ca.gov/waterboards_map.shtml. Provide the date you submitted your request for consultation here, then provide the following information.

Date of Request

06/05/2026

Will your project, during construction or operation, (1) generate waste or wastewater containing such things as sewage, industrial chemicals, metals, or agricultural chemicals, or (2) cause erosion, turbidity or sedimentation?

☐ Yes

☐ No

Will a waste discharge permit be required for the project?

☐ Yes

☐ No

If necessary, provide additional information below:

Consistent with Water Code § 1726, a copy of this Petition will be sent prior to Public Notice to:
Lynn Coster - Program Manager - Water Certification Division
Central Valley Regional Water Quality Control Board
11020 Sun Center Drive #200; Rancho Cordova, CA 95670-6114

Insert the attachment number here, if applicable: A-G

Local Permits

For temporary transfers only, you must contact the board of supervisors for the county(ies) both for where you currently store or use water and where you propose to transfer the water. (Wat. Code § 1726.) Provide the date you submitted your request for consultation here.

Date of Contact

06/10/2026

For change petitions only, you should contact your local planning or public works department and provide the information below.

Person Contacted:

Date of Contact:

Department:

Phone Number:

County Zoning Designation:

Are any county permits required for your project? If yes, indicate type below.

☐ Yes

☐ No

Grading Permit

Use Permit

Watercourse

Obstruction Permit

Change of Zoning

General Plan Change

Other (explain below)

If applicable, have you obtained any of the permits listed above? If yes, provide copies.

☐ Yes

☐ No

If necessary, provide additional information below:

Consistent with Water Code § 1726, a copy of this Petition will be sent prior to Public Notice to each respective Board of Supervisors in Placer County, Fresno County, and Kings County.

Insert the attachment number here, if applicable: A-G

Federal and State Permits

Check any additional agencies that may require permits or other approvals for your project:

- ☐ Regional Water Quality Control Board ☐ Department of Fish and Game
- ☐ Dept of Water Resources, Division of Safety of Dams ☐ California Coastal Commission
- ☐ State Reclamation Board ☐ U.S. Army Corps of Engineers ☐ U.S. Forest Service
- ☐ Bureau of Land Management ☐ Federal Energy Regulatory Commission
- ☐ Natural Resources Conservation Service

Have you obtained any of the permits listed above? If yes, provide copies. ☐ Yes ☒ No

For each agency from which a permit is required, provide the following information:

Agency	Permit Type	Person(s) Contacted	Contact Date	Phone Number
--------	-------------	---------------------	--------------	--------------

If necessary, provide additional information below:

No State or Federal Permits are required for this proposed project.

Consistent with Water Code § 1726, a copy of this Petition will be sent prior to Public Notice to Morgan Kilgour, CDFW North Central Regional (R2) Manager at 1701 Nimbus Road, Rancho Cordova, CA 95670 Phone: (916) 358-2900.

Insert the attachment number here, if applicable: A-G

Construction or Grading Activity

Does the project involve any construction or grading-related activity that has significantly altered or would significantly alter the bed, bank or riparian habitat of any stream or lake? ☐ Yes ☐ No

If necessary, provide additional information below:

NA

Insert the attachment number here, if applicable:

Archeology

Has an archeological report been prepared for this project? If yes, provide a copy. ☐ Yes ☐ No

Will another public agency be preparing an archeological report? ☐ Yes ☐ No

Do you know of any archeological or historic sites in the area? If yes, explain below. ☐ Yes ☒ No

If necessary, provide additional information below:

NA

Insert the attachment number here, if applicable:

Photographs

For all petitions other than time extensions, attach complete sets of color photographs, clearly dated and labeled, showing the vegetation that exists at the following three locations:

- ☐ Along the stream channel immediately downstream from each point of diversion
- ☐ Along the stream channel immediately upstream from each point of diversion
- ☐ At the place where water subject to this water right will be used

Maps

For all petitions other than time extensions, attach maps labeled in accordance with the regulations showing all applicable features, both present and proposed, including but not limited to: point of diversion, point of rediversion, distribution of storage reservoirs, point of discharge of treated wastewater, place of use, and location of instream flow dedication reach. (Cal. Code Regs., tit. 23, §§ 715 et seq., 794.)

Pursuant to California Code of Regulations, title 23, section 794, petitions for change submitted without maps may not be accepted.

All Water Right Holders Must Sign This Form:

I (we) hereby certify that the statements I (we) have furnished above and in the attachments are complete to the best of my (our) ability and that the facts, statements, and information presented are true and correct to the best of my (our) knowledge. Dated 06/05/2026 at Placer County Water Agency, Auburn, CA .



Darin Reintjes

Water Right Holder or Authorized Agent Signature

Water Right Holder or Authorized Agent Signature

NOTE:

- Petitions for Change may not be accepted unless you include proof that a copy of the petition was served on the Department of Fish and Game. (Cal. Code Regs., tit. 23, § 794.)
- Petitions for Temporary Transfer may not be accepted unless you include proof that a copy of the petition was served on the Department of Fish and Game and the board of supervisors for the county(ies) where you currently store or use water and the county(ies) where you propose to transfer the water. (Wat. Code § 1726.)

Attachment A

Environmental Information for Petitions

Attachment A

Introduction

Placer County Water Agency (PCWA) proposes to transfer up-to 21,053 acre-feet (AF) of Middle Fork American River Project (MFP) water (Transfer Water) currently stored in Hell Hole Reservoir on the Rubicon River and French Meadows Reservoir on the Middle Fork American River (MFAR) to the Westlands Water District (WWD), for designated beneficial uses within the WWD service area. To accomplish this transfer, the following temporary (one year or less) changes in Place of Use (POU) and Point(s) of Rediversion (PORD) are being sought by Petition pursuant to PCWA Water Right Application 18085 (Permit No. 13856) and consistent with California Water Code §1725-§1732, which includes:

- 1) The temporary addition of United States Department of the Interior Bureau of Reclamation (Reclamation) Central Valley Project (CVP) Bill Jones Pumping Plant (Jones) intake facility and/or the California Department of Water Resources (DWR) State Water Project (SWP) Harvey O. Banks Pumping Plant (Banks) (**Attachment B**) as Point(s) of Rediversion for WWD to receive PCWA Transfer Water under Permit No. 13856;
- 2) The temporary addition of San Luis Reservoir (SLR), a Reclamation CVP facility (**Attachment B**), as a point for the temporary storage and rediversion of Transfer Water by WWD under Permit No. 13856; and
- 3) The temporary addition of the WWD service area (**Attachment C**) to Permit No. 13856 authorizing consumptive and beneficial uses of Transfer Water within the WWD service area.

Transferring Agencies Overview

Placer County Water Agency

PCWA is a public agency created and existing pursuant to the provisions of the Placer County Water Agency Act (Water Code Appx. Ch. 81.). PCWA owns and operates the MFP and holds appropriative water rights for the MFP pursuant to Permits 13856 and 13858, issued on Applications 18085 and 18087, by the State Water Rights Board, predecessor to the State Water Resources Control Board (SWRCB). SWRCB Permits 13856 and 13858, both issued in 1963 and amended in 1975, allow for the combined diversion and storage of up-to 315,000 Acre Feet per Annum (AFA) of MFP water held primarily in two on-stream storage reservoirs (French Meadows and Hell Hole Reservoir).

PCWA's MFP is a multi-purpose project designed to manage waters of the MFAR, the Rubicon River and tributaries thereto for beneficial Domestic, Municipal & Industrial, Recreational, and Irrigation uses as well as hydro-electrical power generation. Principal project features include two storage reservoirs, five associated diversion dams (Duncan, North Fork Long Canyon, South Fork Long Canyon, Middle Fork Interbay, and Ralston Afterbay), and five power plants (French Meadows, Hell Hole, Middle Fork, Ralston, and Oxbow).

For the purposes of this proposed 21,053 AF transfer, PCWA will be solely exercising Permit 13856, which allows for the storage and consumptive use of 249,000 AF of MFP water (25,000 AF at Duncan Creek diversion; 95,000 AF in French Meadows; and 129,000 in Hell Hole Reservoir).

Westlands Water District

WWD (or “the District”) was formed in 1952 and encompasses more than 600,000 acres of farmland in western Fresno and Kings Counties. The District serves approximately 600 family-owned farms that average 900 acres in size.

Water is delivered to WWD through the Central Valley Project, a federal water project that stores water in large reservoirs in Northern California for use by cities and farms throughout California. After it is released from CVP reservoirs, the water is typically pumped from the Sacramento-San Joaquin Delta via Reclamation’s Bill Jones Pumping Plant and delivered 70 miles through the Delta-Mendota Canal to San Luis Reservoir. During the spring and summer, the water is released from San Luis Reservoir and delivered to WWD farmers through the San Luis Canal and the Coalinga Canal. Once it leaves the CVP canals, water is delivered to farmers through 1,034 miles of underground pipe and more than 3,300 water meters. WWD farmers produce more than 60 high quality commercial food and fiber crops sold for the fresh, dry, canned and frozen food markets, both domestic and export. More than 50,000 people live and work in the communities dependent on the District's agricultural economy. The communities in and near the District's boundaries include Mendota, Huron, Tranquillity, Firebaugh, Three Rocks, Cantua Creek, Helm, San Joaquin, Kerman, Lemoore and Coalinga.

WWD is interested in augmenting its reduced CVP contract water supply (25% allocation) through this transfer to provide their agricultural customers a critical supplemental water supply for irrigation of their crops during the 2026 growing season. Transfer water that PCWA provides to WWD will be used entirely within the WWD service area for irrigation of agricultural crops (Attachment C).

Description of Proposed Transfer

PCWA proposes to release up to 21,053 AF of stored surplus water from the MFP for the period spanning approximately August 1, 2026 through September 30, 2026 (61 days) for transfer to WWD (“Transfer Water”); pending approvals. The Transfer Water will be released from Hell Hole Reservoir through Middle Fork Powerhouse (Point of Release), rediverted to Ralston Afterbay through Ralston Powerhouse, and ultimately released to the Middle Fork American River (MFAR) from Ralston Afterbay through Oxbow Powerhouse, a 6.1 Mega Watt (MW) hydroelectric generation facility that discharges approximately 1,040 cubic feet per second (cfs) at peak generating capacity. In the event that the Transfer Water is unable to be moved through the Oxbow Powerhouse, the water will be released through the Ralston Afterbay Dam. Ralston Afterbay is PCWA’s most downstream regulating reservoir on the MFAR. Water released from Ralston Afterbay flows for approximately 24 miles to the confluence with the North Fork American River (NFAR) and then another 8 miles into Folsom Reservoir. The travel

time for a release of 1,000 cfs for this 32-mile stretch of the MFAR (between Ralston Afterbay and Folsom Reservoir) is approximately 14 hours.

Folsom Reservoir is a Point of Diversion (POD) and PORD under PCWA's consumptive water rights. If necessary, the use of Folsom Reservoir to temporarily store and subsequently release Transfer Water will be covered under a Warren Act Agreement between WWD and Reclamation.

Reclamation would release the Transfer water from Folsom Reservoir to WWD on a schedule that is mutually agreeable and/or beneficial to Reclamation, WWD, and the environment such that it will not disrupt normal CVP or State Water Project (SWP) operations and will adhere to all current flow standards for the LAR (from Lake Natoma to the confluence with the Sacramento River) as well as the current regulatory requirements for Delta operations. As described in **Attachment G**, Reclamation would release the Transfer Water from Folsom Reservoir on top of (in addition to) projected CVP operations resulting in increased LAR flows and temperature benefits throughout the period of transfer.

2026 Operations

As part of the Petition approval process, and consistent with §81-5(a) of the PCWA ACT, the PCWA Board of Directors must determine that the demands of PCWA's customers within Placer County will be met prior to declaring that surplus water is available for an out-of-county transfer. To make this determination, the volume of Transfer Water delivered must be measured against PCWA's baseline operations plan for 2026, which considers the following factors:

1. The most up-to-date hydrologic inflow forecasts (June 1, 2026),
2. PCWA's pumping demands from the American River Pump Station (ARPS) based on other available water supplies,
3. Contractual obligations to meet San Juan Water District (SJWD) and City of Roseville demands,
4. MFP FERC required recreational rafting releases,
5. MFP FERC required minimum instream flow requirements,
6. MFP FERC required minimum carryover storage requirements,
7. Evaporative losses,
8. Discretionary power releases, and
9. Annual carryover storage targets.

Although precipitation in Water Year 2026 has been near average, record warm temperatures observed early in the winter season resulted in a near record low snowpack. As a result, the filling of MFP reservoirs occurred much earlier than usual – yielding nearly full reservoirs at the end of April, when they typically hold peak storage in late June. The MFP combined peak storage of 329,000 AF occurred on April 27, 2026 which is 96% capacity and approximately 140% of historical (66'-25') storage for May 1.

PCWA's FERC license for the operation of the MFP dictates the amount of water required to be released for environmental and recreational releases based on the California Department of Water Resources (DWR) May 1 Bulletin 120 (B120) runoff forecast. The May 1, 2026, B120 Unimpaired Flow to Folsom

Lake was projected at 2,420,000 AF. This forecasted runoff volume designates the MFP to an Above Normal (AN) Water Year Type for 2026.

PCWA's pumping demands from ARPS are anticipated to be higher than normal due to anticipated reductions in PG&E supply caused by ongoing repairs and improvements at Lake Spaulding and Fordyce Lake. PG&E's Drum-Spaulding Project supply is the primary source (and in some areas the sole source) for PCWA's Service Area in Placer County, with up to 125,400 AF of annual supplies allocated by various conditions. PCWA anticipates receiving approximately 70% of this supply in 2026. The City of Roseville (Roseville) and the San Juan Water District (SJWD) have access to MFP water to supplement their demands, with each having an estimated demand of 10 TAF of MFP contract water in 2026.

The Transfer Water would also add to the amount of water that Reclamation has available to be released from Folsom Lake. The introduction of MFP water would increase volume of the metalimnion, or middle thermal section of the stratified water pool in Folsom Lake. Transfer water released from the base of PCWA's MFP reservoirs enters Folsom at approximately 65–68°F and travels within the cool-water metalimnion layer. Results from temperature modeling confirm that a more pronounced flow path of cooler water is created toward the dam intake shutters. From the operational perspective, blending of water from the cooler metalimnion with other variable temperature water in the lake strata functionally extends the life of the cold-water pool in Folsom Reservoir (**Attachment G**).

The Transfer Water would be released in addition to the baseline operations described above and would have otherwise remained in storage if not for the proposed transfer. As a result, the carryover storage of the MFP reservoirs will be reduced by the amount of Transfer Water released. Based on all the above, PCWA's operational plan for the 2026/2027 MFP carryover storage target would be 140,000 AF, as shown in Attachment E and described in detail below.

MFP Carryover Storage/Refill Reservation

The typical end-of-the-year (December-February) combined carryover storage target (low point) for the MFP reservoirs (French Meadows and Hell Hole) for the end of 2026 is 160,000 AF. Historically the MFP carryover storage has ranged between 70,400 AF (1992) and 208,434 AF (2011). When accounting for water years that did not involve water transfers (typically wetter 75% of water years), the median MFP carryover storage is 157,000 AF (n=49). Water year 2025 was a good example of this with a carryover storage of 157,542 AF.

The proposed transfer requested under this Petition would likely require refill terms and restrictions to avoid injury to any downstream user of water from the refilling of the vacated space created from the transfer of water. Depending on the hydrologic conditions in subsequent years, PCWA may carry up to an additional 21,053 AF deficit in its MFP carryover target forward in time until conditions allow refill of the deficit (e.g., Folsom Reservoir releases are being made for flood or storage management purposes while the Delta is in Excess Condition). For accounting purposes, the 2026 MFP combined end-of-year carryover target will be 138,947 AF, reflecting the transfer volume of 21,053 AF deducted from the baseline carryover target of 160,000 AF.

In order to accomplish the transfer, PCWA proposes to release 21,053 AF of surplus water from MFP storage reservoirs during the months of August and September of 2026. The proposed with-transfer carryover target of 138,947 AF (**Attachment E**) remains well above the minimum carryover level required by FERC of 75,155 AF total combined storage (24,950 AF in French Meadows & 50,205 AF in Hell Hole) and is more than sufficient to meet PCWA's downstream demands (e.g., consumptive water supply, minimum instream flow requirements, etc.) should water year 2027 be critically dry.

Period of Transfer/Exchange

As shown in the 2026 MFP Operation Plan (Attachment E), PCWA is planning on the release of Transfer Water beginning on approximately August 1, 2026 and continuing through September 30, 2026 (via Middle Fork Powerhouse). Transfer releases will be introduced to the MFAR at an average daily rate of approximately 174 cfs, for a period of approximately 61 days, totaling 21,053 AF.

It is expected that there will be capacity to pump the Transfer Water released from Folsom Lake at the C.W. Bill Jones Pumping Plant beginning in September. Water introduced into Folsom Lake in early August would be released prior to 30 days of being introduced into the lake. Transfer Water will be released to the Lower American River at an average daily rate of approximately 165 cfs, for a period of approximately 61 days, totaling 20,000 AF.

The dates targeted for transfer are contingent on regulatory approvals, PCWA MFP operational constraints, authorizations for points of rediversion, and the ability of Reclamation to release water from Folsom Reservoir to meet contractual obligations and support fisheries resources and water quality objectives in the LAR as well as the Delta.

Agency Coordination and Consultation

To accomplish this transfer, if deemed necessary, WWD will execute a Warren Act Contract with Reclamation to temporarily store and convey the Transfer Water through CVP facilities. As part of this Warren Act contract (federal action), and as the Federal Lead Agency, Reclamation holds discretion for initiating consultation with NMFS and/or the USFWS under Section 7 of the Federal Endangered Species Act (FESA) for federally listed threatened and endangered species.

Reclamation would ensure that Transfer releases adhere to applicable instream flow and temperature mandates in the LAR and Delta. As shown in Attachment G, and as concluded in similar PCWA transfers (2020/2021/2022) approved by SWRCB, implementation of this Transfer would not harm and would provide reasonable temperature benefits to California Endangered Species Act and FESA listed species, as well as improving aquatic habitat conditions in the LAR with additional flow.

Reclamation recently adopted a Mitigated Finding of No Significant Impact and Decision Record signed on March 16, 2026 to implement the Proposed Action in the 2026-2027 North to South Water Transfers EA (CGB-ED-2024-025). This decision extends the approval of Alternative No. 2 [Full Range of Transfers] (Proposed Action) analyzed in their Final Long-Term Water Transfers Environmental Impact Statement /

Environmental Impact Report (EIS/EIR) covering 2021-2025, which includes PCWA Temporary Transfers of up to 47,000 AF per year, transfer water delivered via Folsom Reservoir could be released for delivery to WWD during the period of July through November. These documents are also consistent with the most current 2019 Biological Opinion for the Long Term Operation of the CVP. Furthermore, on May 14, 2026, SLDMWA adopted a Notice of Determination (NOD) for the Addendum to the 2019 Final Long-Term Water Transfers (LTWT) Environmental Impact Report (Final EIR) (SCH# 2011011010). Their determination indicated that the Final EIR retains its relevance, and the Proposed Project would not have any new or substantially more severe significant direct, indirect, or cumulative impact on the existing environment.

Further, PCWA will be sending a copy of this Petition to the California Department of Fish and Wildlife (CDFW) as well as the Central Valley Regional Water Quality Control Board (CVRWQCB) who act as responsible agencies consistent with Water Code §1726(c).

Point of Diversion or Rediversion

Current:

- A.** PCWA's current points of diversion (POD) are located at California Grid Coordinates, Zone II, NAD 27, Mount Diablo B&M:

Water Body	POD Location	N	E	Quart.	Sec.	T-N	R-E
Duncan Creek	Duncan Creek	538,130	2,431,040	NW SW	24	15	13
M.F. American River	French Meadows	530,100	2,434,250	NW NE	36	15	13
Rubicon River	Hell Hole	510,750	2,452,000	SW SE	16	14	14
S.F. Long Canyon	Long Canyon	507,675	2,434,250	SW NE	24	14	13
N.F. Long Canyon	Long Canyon	506,970	2,431,250	NW SW	24	14	13
M.F. American River	Ralston Interbay	498,137	2,397,300	NW NE	35	14	12
M.F. American River	Ralston Afterbay	490,160	2,357,100	NW NW	3	13	11
N.F. American River	Auburn	444,400	2,267,400	NE SW	23	12	8

B. PCWA's current points of rediversion (PORD) are located at California Grid Coordinates, Zone II, NAD 27, Mount Diablo B&M:

Water Body	PORD	N	E	Quart.	Sec.	T-N	R-E
M.F. American River	French Meadows	530,100	2,434,250	NW NE	36	15	13
Rubicon River	Hell Hole	510,750	2,452,000	SW SE	16	14	14
M.F. American River	Ralston Interbay	498,137	2,397,300	NW NE	35	14	12
M.F. American River	Ralston Afterbay	490,160	2,357,100	NW NW	3	13	11
N.F. American River	Auburn	444,400	2,267,400	NE SW	23	12	8
American River	Folsom Dam	380,461	2,240,626	SW NE	24	10	7

Proposed Point(s) of Rediversion:

C. No changes are requested in this Petition for PCWA's current points of diversion or points of rediversion.

Water released from Folsom Reservoir will be re-operated via Lake Natoma into the LAR; water released from Lake Natoma flows for an additional 22 miles to the confluence with the Sacramento River. The Sacramento River flows approximately 55 miles where it meets the San Joaquin River at the head of the Sacramento-San Joaquin Delta. From this location, Transfer Water would move east via counter flow back up the San Joaquin River and then south, meandering for an additional 45 miles to points of rediversion at either the Harvey O. Banks Pumping Plant (Banks) and/or Bill Jones Pumping Plant (Jones) (**Attachment B**). Utilization of the Delta Cross Channel, when available, cuts approximately 18 miles off the total distance to the CVP/SWP South Delta Pumps and will likely be the preferred conveyance route once the salinity barrier is installed

Water rediverted at the Jones intake facility would be conveyed south for approximately 70 miles via the Delta Mendota Canal to San Luis Reservoir; water diverted at Banks would be conveyed via the California Aqueduct to San Luis Reservoir. Transfer Water would be temporarily stored in San Luis Reservoir, a PORD sought under this petition, and then delivered via the San Luis Canal, which runs through the heart of the WWD service area, thence the Coalinga Canal (**Attachment C**).

WWD will coordinate with Reclamation CVO staff to determine the timing and flow rate of Transfer Water releases from the Point of Delivery at Folsom Reservoir for rediversion at the Jones and/or Banks intake facility. In the event that Banks is used as a PORD, WWD and PCWA will consult with DWR to execute a conveyance agreement.

Accordingly, PCWA proposes to add the following points of rediversion sought under this Petition:

Harvey O. Banks Pumping Plant

This SWP Point of Rediversion is located 37°48'1.41"N/ 121°37'17.50"W, California Coordinate System,

Zone 3, NAD 83, being within the SW ¼ of Section 35, T1S, R3E, MDB&M. This proposed point of rediversion is identified on maps filed with the Division of Water Rights (Division) under Application 5630, and shown in **Attachment B**.

Bill Jones Pumping Plant

This CVP Point of Rediversion is located 37°47'47.22"N/ 121°35'8.06"W, California Coordinate System, Zone 3, NAD 83, being within the SW ¼ of Section 35, T1S, R3E, MDB&M. This proposed point of rediversion is identified on maps filed with the Division under Application 9368, and shown in **Attachment B**.

San Luis Reservoir

This CVP Point of Rediversion is located 37° 4'27.36"N/121° 0'54.55"W California Coordinate System, Zone 3, NAD 83, being within the SE ¼ of Section 7, T10S, R9E, MDB&M. This proposed point of temporary storage and rediversion is identified on maps filed with the Division under Reclamation Application 15764 (Permit 12860) for the use of San Luis Reservoir, and shown in **Attachment B**.

PCWA Place of Use

Current: Western Placer County and northern Sacramento County, as shown on a map set dated July 31, 1996 on file with the Division and as shown in **Attachment D**.

Proposed: No change in PCWA's current POU is proposed; PCWA proposes to add the service area of WWD as an additional POU in order to facilitate the temporary water transfer to WWD. This proposed temporary (one year) addition to the PCWA POU includes the WWD service area as shown in **Attachment C**.

Purpose of Use

Current: Domestic, Municipal & Industrial, Recreational, Irrigation.

Proposed: No change is being requested in PCWA's current purpose of use within its designated POU; WWD would use the Transfer Water predominantly for Agricultural Irrigation uses in its service area.

Season of Use, Direct Diversion Use (cfs), and Storage (AF)

Current: See project description and water rights permit.

Proposed: No change requested.

Access to Proposed Point(s) of Rediversion

All PORD's and conveyance facilities are owned by the Federal Government and/or State of California

and will be covered in the Warren Act contract with Reclamation or Conveyance Agreement with DWR.

The proposed transfer/exchange water is presently used or stored within the county/counties of:

Placer & Sacramento

The proposed transfer/exchange water will be beneficially used within the following county/counties:

Fresno & Kings

Checklist Questions:

- 1a. Would the transfer/exchange water have been consumptively used or stored in the absence of the proposed temporary change (See WC 1725)?**

Yes. The 21,053 AF of proposed Transfer Water is currently stored in PCWA's MFP reservoirs and would remain in storage absent this transfer, as described above.

- 1b. Provide an analysis which provides documentation that the amount of water to be transferred/exchanged would have been consumptively used or stored in the absence of the proposed temporary change.**

To provide WWD with the Transfer Water sought under this Petition, PCWA proposes to transfer a surplus 21,053 AF of MFP storage which is currently (June 1, 2026) at 326,000 AF (140% of average YTD). As stated above, the release of this surplus water would be accomplished in synchronization with PCWA's hydroelectric power generation between August 1, 2026 and September 30, 2026. Attachment E shows the 2026 MFP operational plan both with and without the transfer. Please refer to the PCWA 2026 Operations discussion above for justification that the Transfer Water would have been consumptively used or stored in the absence of the proposed temporary change. Consistent with §81-5 of the PCWA ACT, the Agency must ensure that the needs of their Placer County customers are met prior to determining that surplus water is available for out-of-county transfer and/or sale.

- 2a. If the point of diversion/rediversion is being changed, are there any person(s) taking water from the stream between the present point of diversion/rediversion and the proposed point?**

Yes – However, the water to be transferred would not have been released if not for the transfer and therefore would not have been available to any person(s) regardless.

- 2b. Are there any persons taking water from the stream between the present point of diversion or return flow and the proposed point of diversion or return flow?**

There are a number of water users taking water from the American River, Sacramento River, Sacramento-San Joaquin Delta, and CVP facilities south of the Delta pumps between PCWA's current points of return flow and the points at which any downstream water user would return

water to the system. PCWA would not transfer water such that it would adversely impact water users within the PCWA service area and PCWA will continue to deliver MFP stored water (Roseville, SJWD, and PCWA Zone 6 via ARPS) as described above to its existing Placer County customers with or without the proposed temporary water transfer.

3a. Provide an analysis of any changes in streamflow, water quality, timing of diversion or use, return flows, or effects on legal users resulting from the proposed transfer/exchange.

Middle Fork and North Fork American Rivers

This transfer will not significantly alter flows, water quality, or reduce the ability for legal users to lawfully take water on the Middle Fork and/or North Fork American rivers when compared to baseline conditions of PCWA's MFP operations. During the transfer period, PCWA will be generating power as is always done during periods of peak summer energy demand. Peak power generation at the point of transfer release (Middle Fork Powerhouse) is approximately 80 megawatts (MW) with a discharge of approximately 950 cfs. The release of Transfer Water would generally occur at times when PCWA is not using the full generation capacity at Middle Fork Powerhouse and would occur within the 'shoulder hours' or off-peak times when generation is typically not scheduled. As such, PCWA's release of Transfer Water will, therefore, fall into the same range of flows (approximately 150 cfs to 1100 cfs) that occur normally in the Middle Fork and North Fork American rivers, during recreational whitewater rafting flow releases or during periods of peak generation common for the spring and summer months.

Physical habitat and water chemistry conditions in the tributary streams and rivers associated with the MFP are of high quality, with low concentrations of mineral constituents and other substances generally conforming to regulatory water quality objectives and standards. Historical data shows that generally all of the constituents analyzed in project-affected waters (within and downstream of project impoundments) complied with current regulatory standards; Water Quality Technical Study Report - AQ 11 prepared in support of the Federal Energy Regulatory Commission (FERC) Environmental Impact Statement (EIS) for PCWA's MFP FERC Relicensing Project No. 2079 is provided electronically as **Attachment F** for a detailed description of general water quality conditions within the MFP watershed.

In addition, as owner and operator of a Public Water System, PCWA conducts routine California Code of Regulations (CCR) Title 22 water quality sampling at the ARPS (approximately four miles upstream of the Point of Delivery) pursuant to Section 116275 of the California Safe Drinking Water Act which is contained in Part 12, Chapter 4 of the California Health and Safety Code. PCWA's California Department of Public Health and Safety (DPHS) Monitoring requirements set forth in California Department of Public Health and Safety Permit No. 01-02-07(P) 003 issued on December 10, 2007 are set to ensure that MFP surface water diverted from the North Fork American River at the ARPS meets current DPHS drinking water standards as well as Central Valley Regional Water Quality Control Plan (Basin Plan) Water Quality Standards and Objectives.

The previous four years (2017-2025) of data from the ARPS DPHS water quality sampling is also attached electronically in Attachment F as an example of the high-quality water received from the American River Basin.

Based on the clean, cold, generally high-quality water released from the MFP, the increase in timing, duration, and magnitude of flows during the transfer period will benefit downstream water temperatures and instream flow conditions as detailed in **Attachment G**.

Receiving Water Bodies: Lower American and Sacramento Rivers

After release at Oxbow Powerhouse, Transfer Water will flow first through the Oxbow Powerhouse or the Ralston Afterbay Dam not the MFAR. The water would then flow into Folsom Reservoir where it will be temporarily held in storage by Reclamation and scheduled for release to the Jones and/or Banks intake facility (**Attachment B**). **Attachment G** shows that Transfer Water will, in general, decrease the temperature of water from the North Fork American River entering Folsom Reservoir - as well as decrease temperatures in the Lower American River when released in August and September. Reclamation will ultimately be responsible for coordination and scheduling of the volume and timing of releases from Folsom Reservoir to the Point of Rediversion so that optimal thermal conditions are realized in the receiving water bodies consistent with existing state and federal regulations, endangered species acts, and all biological opinions in effect at the time of the transfer. These releases from Folsom will enter the LAR which in turn flows into the Sacramento River.

Although Transfer Water may be released by PCWA and rediverted by WWD for a period of up to one year or less from the date of SWRCB approval (Water Code §1728), it is currently anticipated that the water will be released from the MFP by PCWA in August (10,527 AF) and September (10,526 AF) of 2026 (Attachment E). During these summer months, stream flows in the American River, Sacramento River, and Sacramento-San Joaquin Delta are typically dominated by CVP and SWP releases to meet Delta Water Quality objectives, fulfill contractual deliveries, and facilitate temporary water transfers. This is largely due to the fact that the normal, historical unimpaired hydrology of the American and Sacramento rivers, as well as those of the Delta and its tributaries, would typically support a declining hydrograph during these summer months. As shown in Attachment G, modeling indicates that the Transfer will benefit water temperature conditions in the lower American River during a critical period over the summer with water released on top of Reclamations projected operations for Folsom Reservoir.

Thus, while the exact schedule and daily volume of transfer releases that will be implemented by CVO for Folsom Reservoir cannot be stated with precision at this time, it is their intent to make transfer releases from Folsom during August and September as described **Attachment G**. As such, the transfer will not cause substantial changes in streamflow, water quality, timing of

diversion or use, return flows, nor would it have a detrimental effect on legal users of water within the MFP area or PCWA's current deliveries within their permitted POU.

The only effects of this transfer on other legal users of water downstream of the Point of Delivery would be a slight increase in flows from Transfer releases at Folsom Reservoir to the proposed Point of Rediversion at the Jones/Banks intake facility, depending on how Reclamation operates Folsom Reservoir. The diversion of Transfer Water at the Jones and/or Banks intake facility would comply with current standards and all state and federal regulations and permits that apply to the proposed Point (s) of Rediversion. As such, the transfer will cause no adverse economic, physical, or environmental effects within the geographic scope of this transfer.

These determinations are consistent with the conclusions made by Reclamation in their Amended Record of Decision (ROD) signed on May 7, 2021 to implement Alternative No. 2 [Full Range of Transfers] (Proposed Action) analyzed in the 2019 Final Long-Term Water Transfers Environmental Impact Statement/Environmental Impact Report (EIS/EIR), which includes PCWA Temporary Transfers of up to 47,000 AF per year for the period covering 2019 through 2024. On May 14, 2026, SLDMWA adopted a Notice of Determination (NOD) for the Addendum to the 2019 Final Long-Term Water Transfers (LTWT) Environmental Impact Report (Final EIR) (SCH# 2011011010). Their determination indicated that the Final EIR retains its relevance, and the Proposed Project would not have any new or substantially more severe significant direct, indirect, or cumulative impact on the existing environment.

3b. State reasons you believe the proposed temporary change will not injure any legal user of the water, see Water Code Section 1727(b)(1).

No legal user of water will be injured due to PCWA's transfer since the transfer of water will only slightly increase, not decrease, streamflow below PCWA's MFP reservoirs. Any such increase will be minor and will not cause any water flows to increase above normal seasonal levels, nor would the increased flows violate regulatory flow requirements as Reclamation will be adhering to their CVP Biological Opinion and the MFMS for the LAR. The 21,053 AF of proposed Transfer Water is currently held in storage in accordance with PCWA's water rights and would not be available to any other legal user of water absent this transfer. The Transfer will not affect PCWA's ability to meet future demands or contractual obligations – even if water year 2027 is critically dry. Additionally, PCWA will enter into a reservoir refill agreement with Reclamation, ensuring that future refill of any storage deficit in PCWA's MFP reservoirs created by the transfer will not reduce the amount of water the SWP/CVP or other water users could otherwise divert during the hydrologic refill cycle following the transfer.

4. Consult with staff of the applicable Regional Water Quality Control Board concerning the proposed temporary change. State the name and phone number of person(s) contacted. Summarize their opinion concerning compliance with CCR 794(b) and any Regional Board requirements.

PCWA will send a copy of this Petition prior to the posting of the Public Notice and opening of the 15 day comment period to the CVRWQCB. PCWA has executed numerous transfers similar to this proposed transfer in the past without any concerns in water quality noted by the CVRWQCB. The MFP water proposed for transfer is very high-quality runoff derived predominantly from snowmelt and rains falling in largely undeveloped higher elevation portions of Placer County in the Sierra Nevada's. As detailed above and as referenced in **Attachment G**, the slight increase in flows in downstream reaches resulting from this transfer will improve water quality by decreasing or moderating water temperatures in the LAR.

- 5a. Consult with the California Department of Fish and Wildlife (CDFW) pursuant to 14 CCR 794(b) concerning the proposed temporary change. State the name and phone number of the person(s) contacted and their opinion concerning the potential effect(s) of the proposed temporary change on fish, wildlife, or other instream beneficial uses, and state any measures recommended for mitigation.**

Consistent with Water Code § 1726, a copy of this Petition will be sent prior to Public Notice to the CDFW North Central Regional Manager at 1701 Nimbus Road, Rancho Cordova, CA 95670 Phone: (916) 358-2900. PCWA expects CDFW to concur that the transfer will not unreasonably affect fish or wildlife resources because very similar transfers have occurred in the past with no adverse impacts identified by CDFW. In the past, CDFW advocated for such PCWA transfers as part of the transfer of water to the CAL-FED Environmental Water Account (EWA) in 2001 and 2004. CDFW has reviewed many similar transfers from PCWA since the early 1990's and has never indicated that instream beneficial uses would be adversely affected by the introduction of PCWA Transfer Water to downstream reaches.

- 5b. Does the proposed use serve to preserve or enhance wetlands habitat, fish and wildlife resources, or recreation in or on the water (See WC § 1707)?**

While the increased releases may preserve or enhance wetlands habitat, fish and wildlife resources, or recreation in or on the water, this Petition is not intended for an instream flow dedication pursuant to WC § 1707

While the primary purpose of this Petition will be for designated beneficial uses within the WWD service area, the release of Transfer Water from PCWA's MFP reservoirs will provide up to 21,053 AF of supplementary flows in the Middle Fork and North Fork American rivers to the proposed Point of Rediversion providing multiple benefits along the way as described herein.

Releasing 21,053 AF of supplemental transfer water that would have otherwise stayed in storage provides additional benefits including, achieving flow augmentation objectives in the Lower American River, supplying more hydropower generation to the CAISO Grid during peak summer demand periods, and potentially enhancing commercial and recreational rafting opportunities in the MFAR.

Making additional water available to PCWA's and Reclamation's powerhouses during the peak summer power load period of a drier year is important for grid regulation in California. Hydroelectric power generation is the primary source of flexible generation used by the California ISO to regulate the fluctuations of the electric grid in California. The MFP is regularly called upon by California ISO to provide critical grid support services when abrupt changes in load occur.

PCWA's summer power generation releases support the regional whitewater economy and a whitewater rafting industry averaging approximately 20,000 user-days on the MFAR. The rafting season began on Memorial Day weekend (May 23-25) and extends through September 25. The proposed Transfer could potentially increase recreational opportunities in the MFAR during the late summer period (September 7th - 30th).

5c. Provide an analysis of potential effect(s) on fish, wildlife, or other instream beneficial uses which may arise from the proposed change.

As explained above, the proposed transfer will improve water quality and provide numerous benefits for many instream beneficial uses including fish and wildlife resources. There is no evidence that the proposed transfer will negatively affect fish and wildlife or other beneficial instream uses in any unreasonable, significant, or measurable way.

When the Transfer Water is diverted at the Jones and/or Banks intake facility (**Attachment B**), all applicable existing state and federal regulations will be followed for the operation of the facilities. Additionally, there is close monitoring and coordination between Reclamation, USFWS, NMFS, and the CDFW regarding the effects of operations on the sensitive aquatic species inhabiting the LAR based on the ambient conditions and water levels of Folsom Reservoir at the time of the Transfer. Because all state and federal resource agencies are currently working closely on LAR flow conditions, if any adverse condition arises, they will be quick to react to avoid significant impacts to species of special concern (i.e., listed and protected under state or federal laws).

Since 1990 PCWA has submitted 16 change petitions for temporary transfers, all of which have been granted by the SWRCB without cause for concern, and have never been associated with or responsible for identifiable adverse water quality or flow conditions resulting in take of any listed species nor have these transfers ever adversely affected downstream beneficial uses.

5d. State reasons you believe the proposed temporary change will not unreasonably affect fish, wildlife, or other instream beneficial uses, see Water Code Section 1727(b)(2).

See response to Question 5c above.

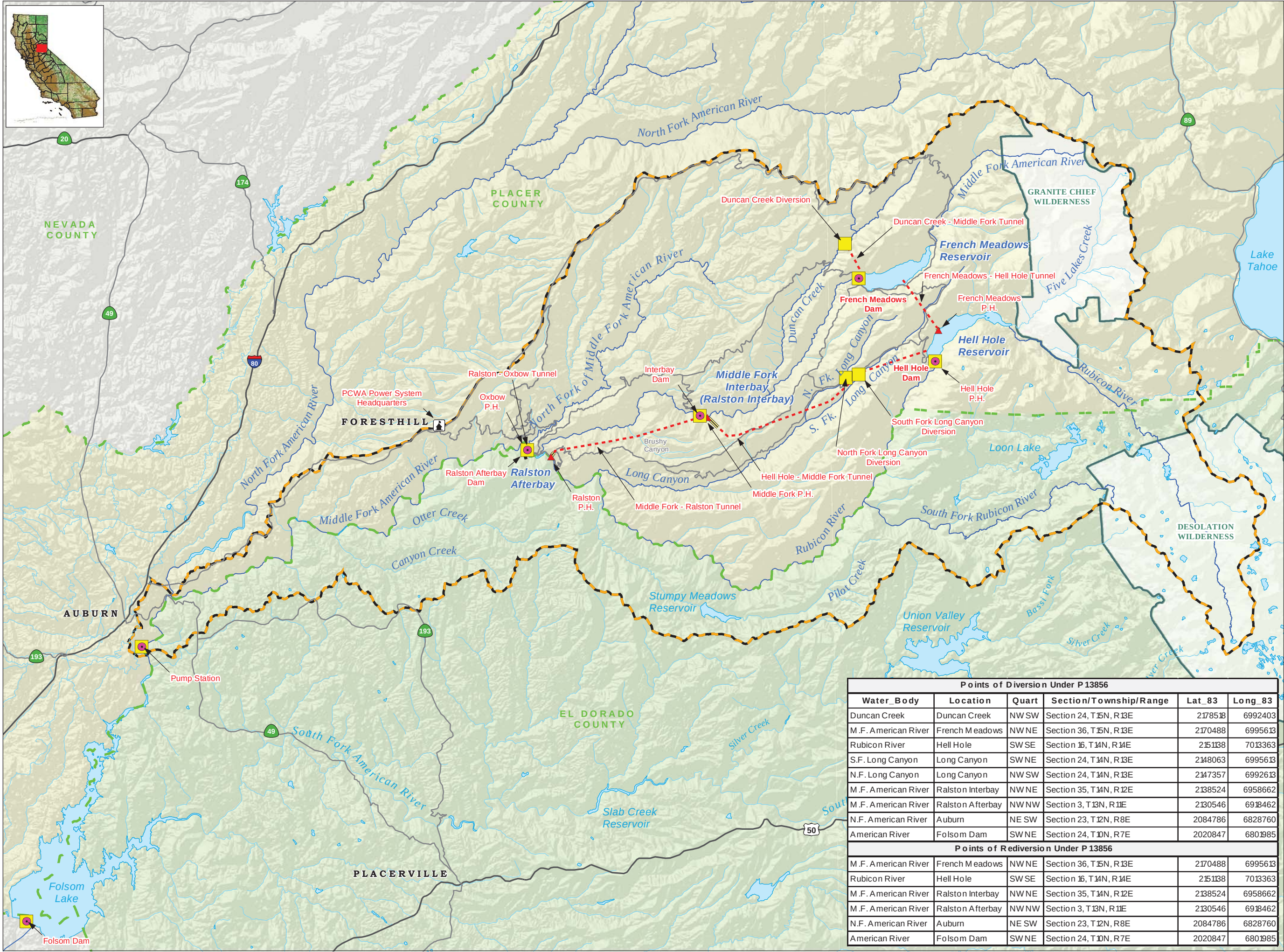
6a. Does any agency involved in the proposed transfer/exchange rely upon section 382 of the Water Code to allow the delivery of water outside of the agency's service area?

No. PCWA has independent legal authority for this transfer under §81-5 of the PCWA ACT. (See Water Code Appx. Ch. 81.)

6b. If yes, provide an analysis of the effect of the proposed transfer/exchange on the overall economy of the area from which the water is being transferred. N/A

Attachment B

PCWA & WWD Points of Diversion and Rediversion



Project Facilities*

- ▲ Powerhouse
- Tunnel
- == Penstock

* All MFP facilities labeled in red.

Transportation

- Major Road
- Minor Road

Hydrography

- Watercourse
- Water Body

Designated Boundary

- County Boundary
- Wilderness Area
- Middle Fork American River Watershed**

**Modified from Calwater Ver. 2.2 to represent drainage above high-water mark of Folsom Lake

Points of Diversion (POD) and Rediversion (PORD)

- POD
- PORD

Points of Diversion Under P 13856					
Water_Body	Location	Quart	Section/Township/Range	Lat_83	Long_83
Duncan Creek	Duncan Creek	NW SW	Section 24, T 15N, R 13E	2178513	6992403
M.F. American River	French Meadows	NW NE	Section 36, T 15N, R 13E	2170488	6995613
Rubicon River	Hell Hole	SW SE	Section 16, T 14N, R 14E	2151138	7013363
S.F. Long Canyon	Long Canyon	SW NE	Section 24, T 14N, R 13E	2148063	6995613
N.F. Long Canyon	Long Canyon	NW SW	Section 24, T 14N, R 13E	2147357	6992613
M.F. American River	Ralston Interbay	NW NE	Section 35, T 14N, R 12E	2138524	6958662
M.F. American River	Ralston Afterbay	NW NW	Section 3, T 13N, R 11E	2130546	6913462
N.F. American River	Auburn	NE SW	Section 23, T 12N, R 8E	2084786	6828760
American River	Folsom Dam	SW NE	Section 24, T 10N, R 7E	2020847	6801985
Points of Rediversion Under P 13856					
M.F. American River	French Meadows	NW NE	Section 36, T 15N, R 13E	2170488	6995613
Rubicon River	Hell Hole	SW SE	Section 16, T 14N, R 14E	2151138	7013363
M.F. American River	Ralston Interbay	NW NE	Section 35, T 14N, R 12E	2138524	6958662
M.F. American River	Ralston Afterbay	NW NW	Section 3, T 13N, R 11E	2130546	6913462
N.F. American River	Auburn	NE SW	Section 23, T 12N, R 8E	2084786	6828760
American River	Folsom Dam	SW NE	Section 24, T 10N, R 7E	2020847	6801985



Placer County Water Agency
PCWA Petition for Change Involving Water Transfers
June 2026

Attachment B1

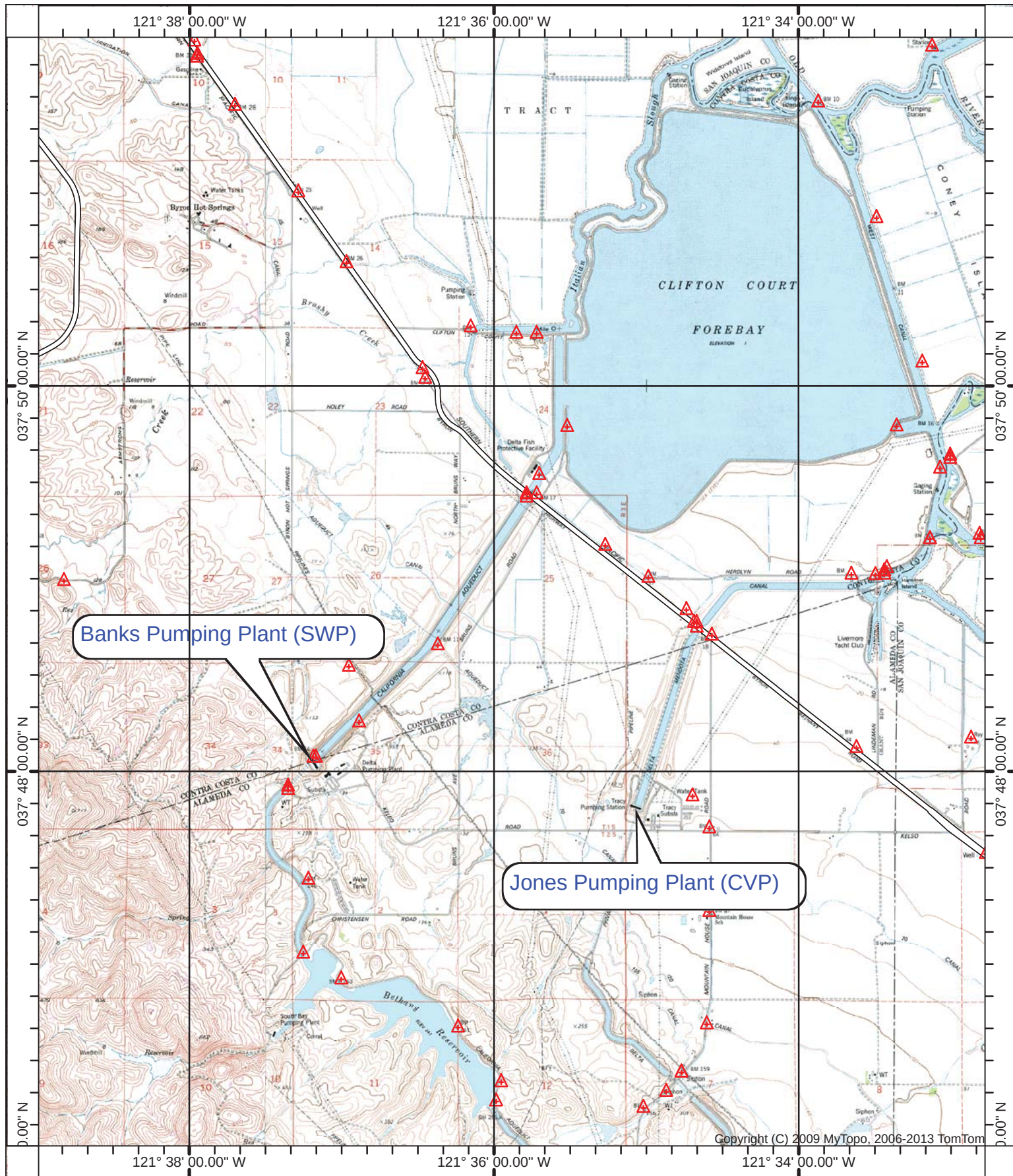
Points of Diversion and Rediversion
under P13856



0 0.5 1 2 3 4 5 Miles

Projection: CA State Plane, Zone 2
Datum: NAD 83

Date: 5/12/2013



Copyright (C) 2009 MyTopo, 2006-2013 TomTom

SCALE 1:48000

0 1 MILE

0 1000 2000 YARDS

0 1 2 KILOMETERS

Map Name: CLIFTON COURT FOREBAY

Print Date: 06/05/2026

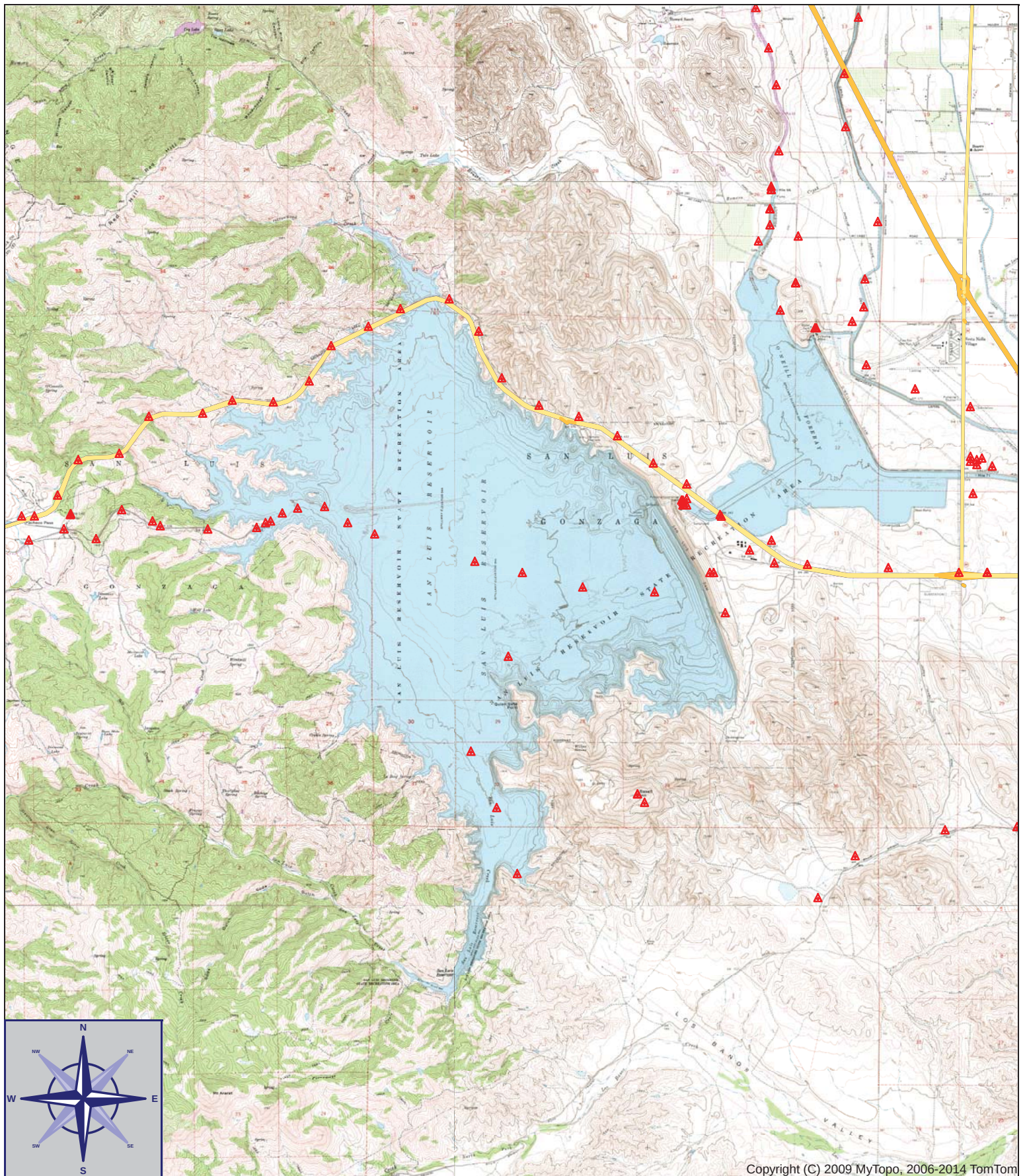
Scale: 1 inch = 4,000 ft.

Map Center: 037° 48' 56.04" N 121° 35' 53.03" W

Horizontal Datum: NAD27



MAP 1- Point of Rediversion



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ATTACHMENT B3- SAN LUIS RESERVOIR

POINT OF REDIVERSION (PORD)

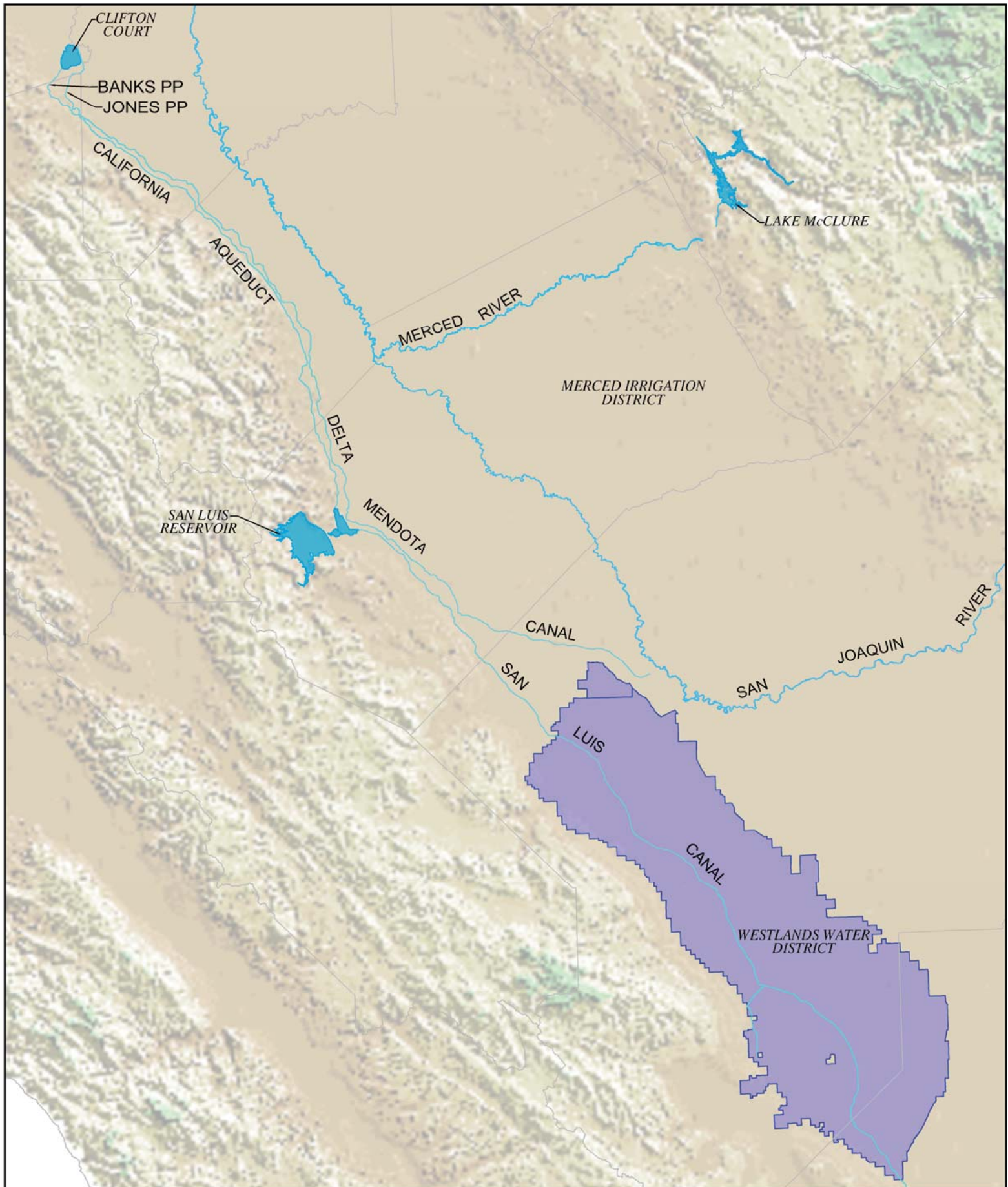
PCWA/WWD 20TAF TRANSFER-2026

SCALE 1:96000

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0 10000 20000 30000 FEET

0 10000 METERS



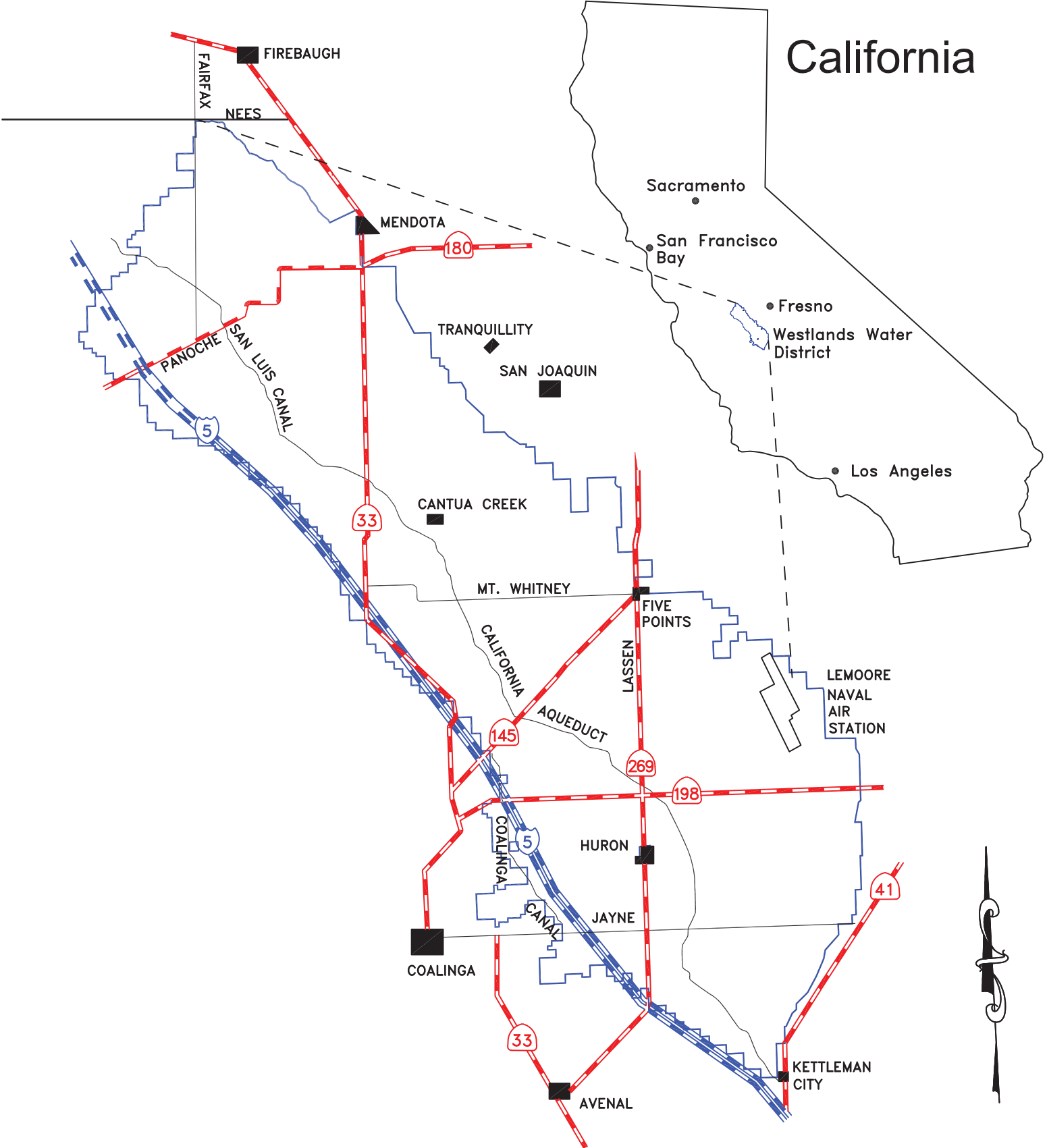
WESTLANDS WATER DISTRICT
3130 N. FRESNO ST. FRESNO, CALIFORNIA 93703
559.224.1523 Fax 559.241.6277

**WESTLANDS WATER DISTRICT
FACILITIES MAP**

Attachment C

Westlands Water District POU

California



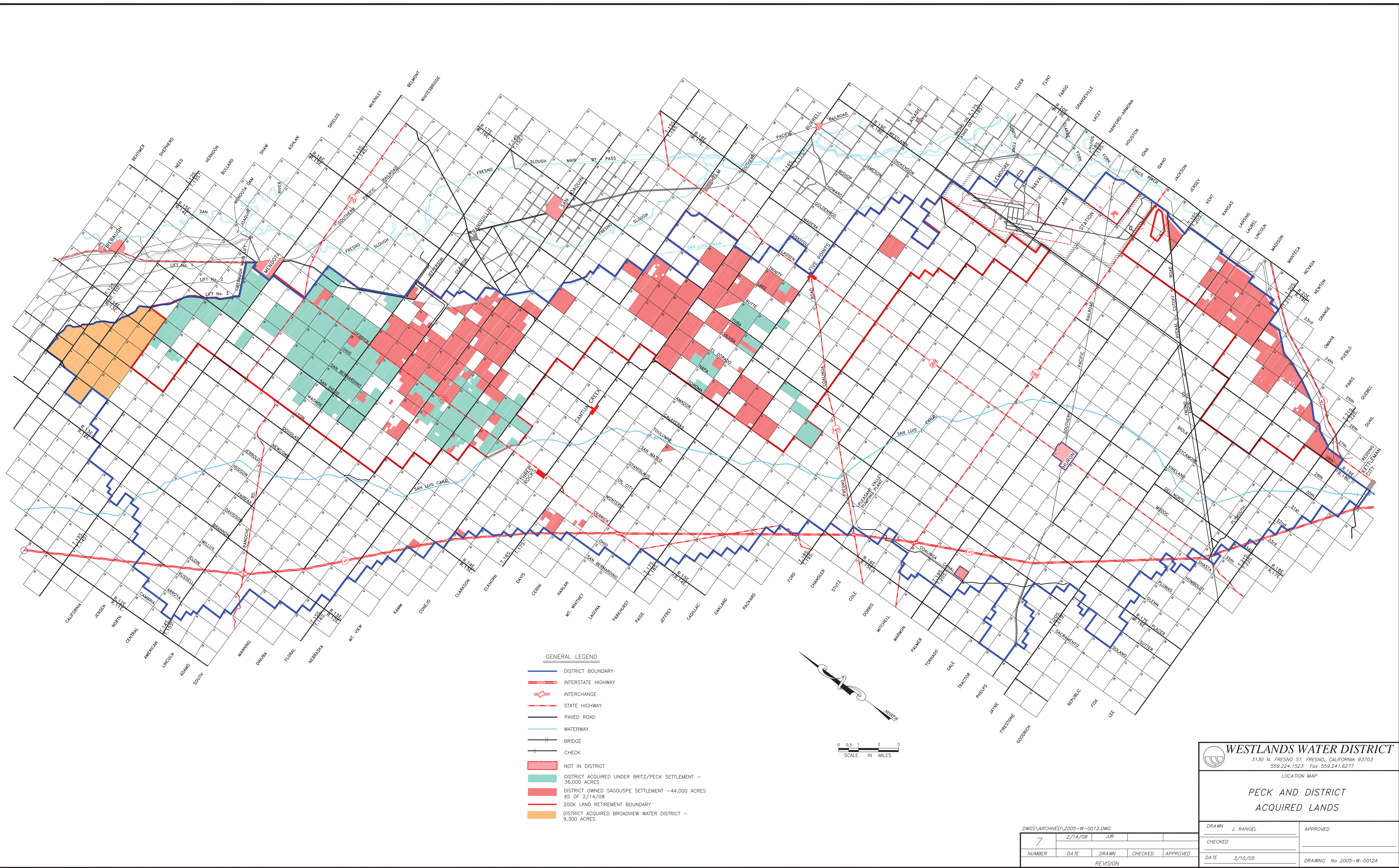
WESTLANDS WATER DISTRICT
3130 N. FRESNO ST. FRESNO, CALIFORNIA 93703
559.224.1523 Fax 559.241.6277

**WESTLANDS WATER DISTRICT
AREA MAP**

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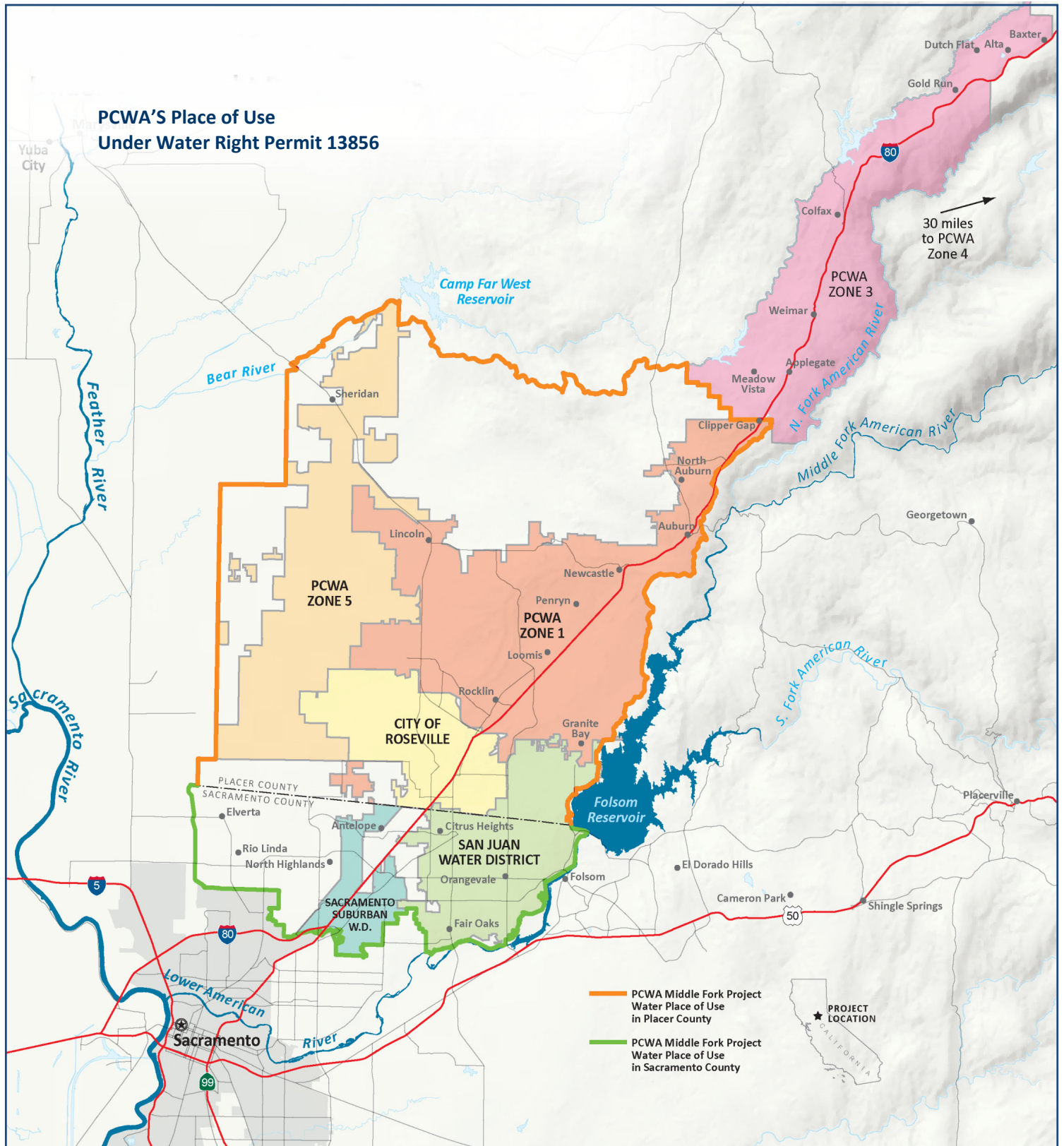
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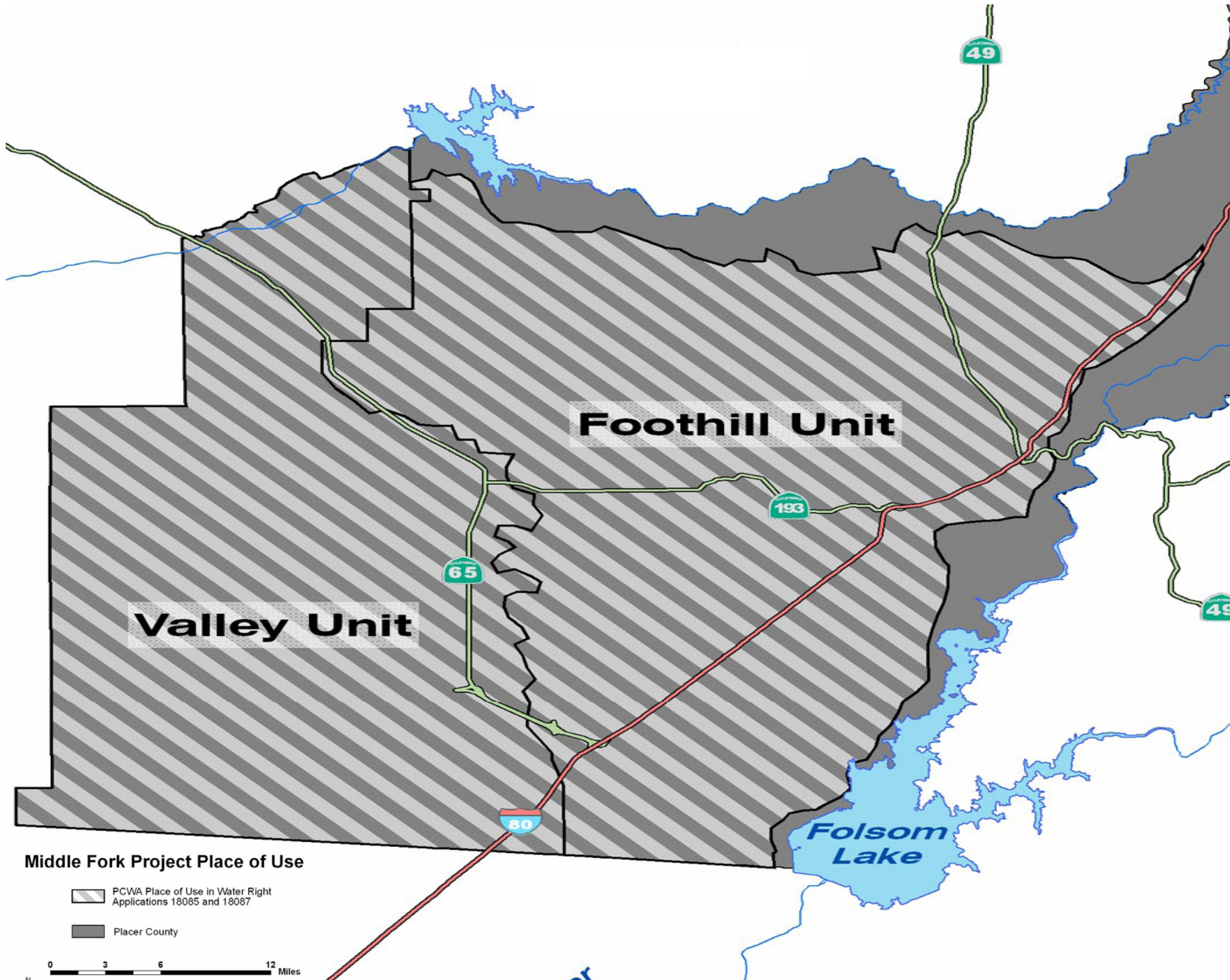
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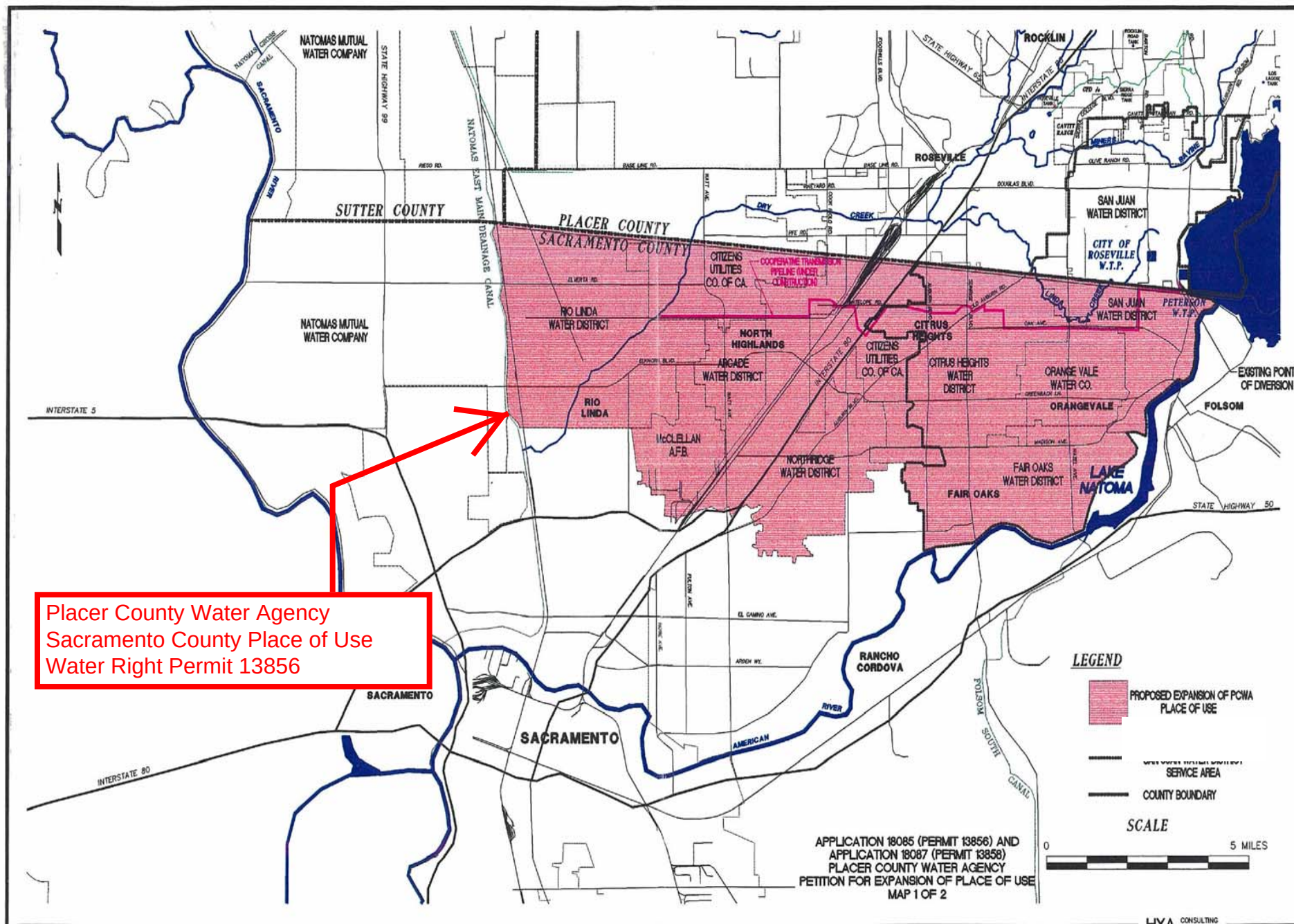


Attachment D

PCWA POU

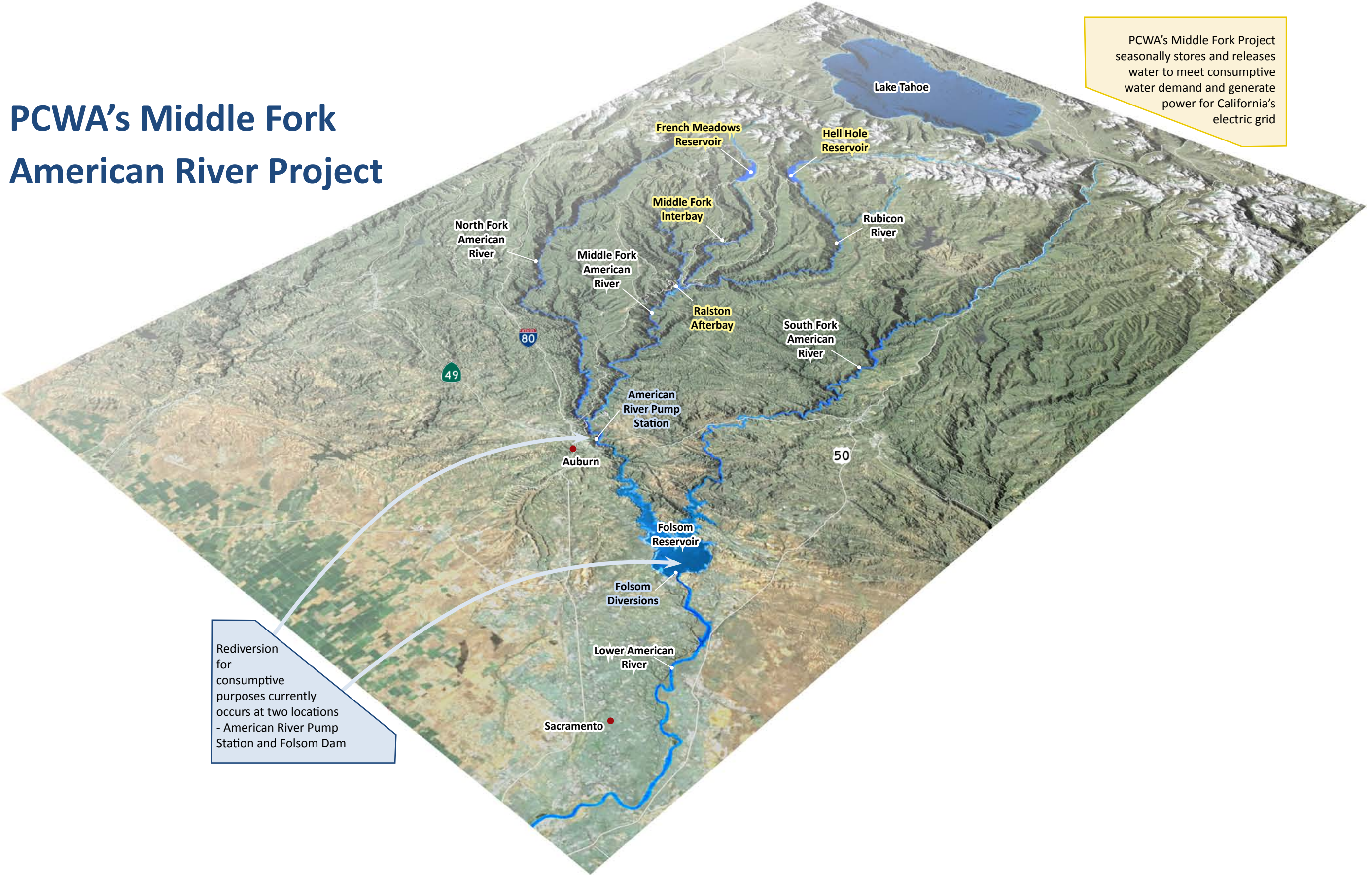






PCWA's Middle Fork American River Project

PCWA's Middle Fork Project seasonally stores and releases water to meet consumptive water demand and generate power for California's electric grid



Rediversion for consumptive purposes currently occurs at two locations - American River Pump Station and Folsom Dam

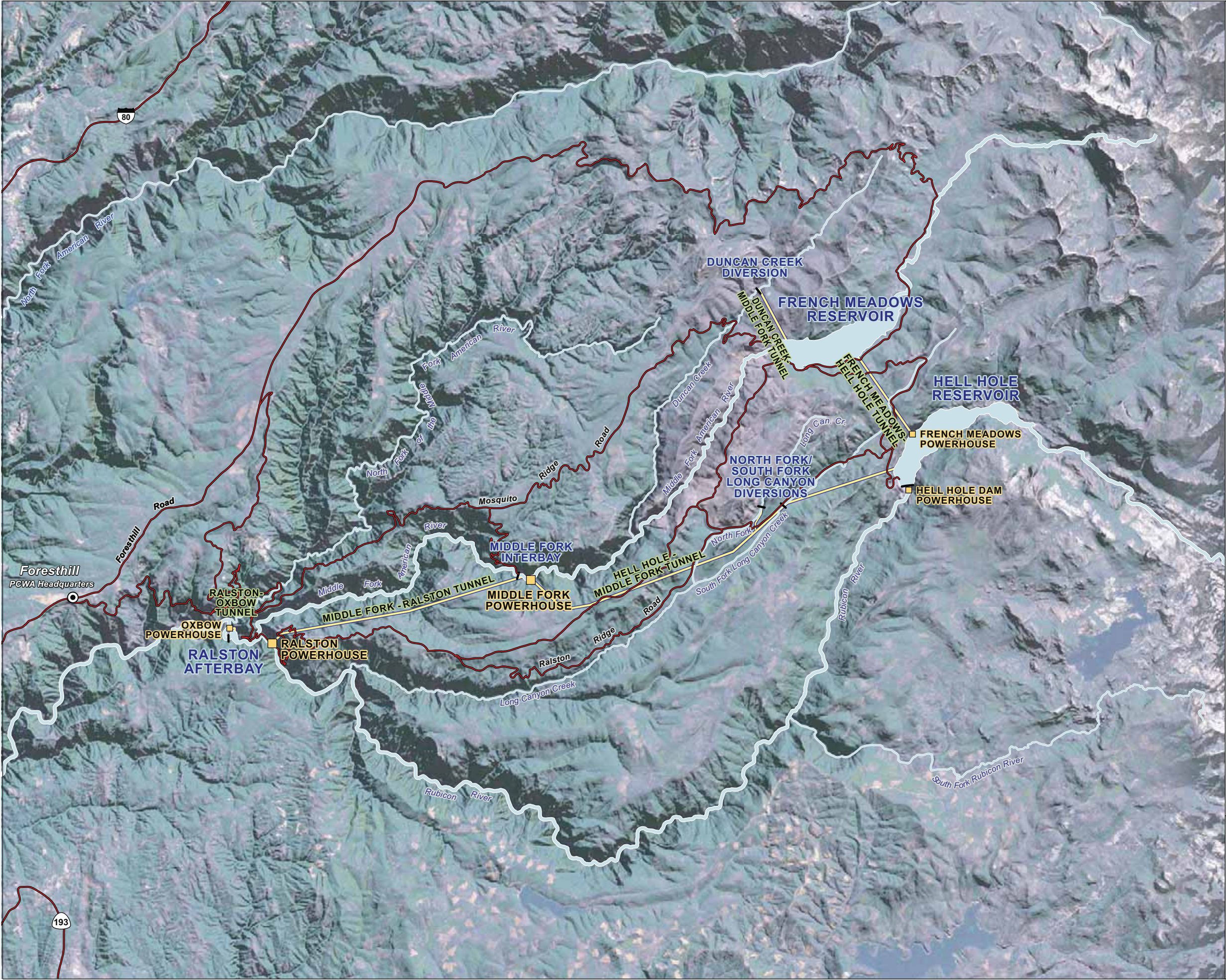
Middle Fork Project Facts and Figures

PROJECT SUMMARY	
Project Completed	1967
Total Energy Production Capacity:	223.7 MW
Average Annual Energy Production:	1,039,078 MWh
Total Gross Water Storage:	345,560 acre-feet (af)
Earth and Rockfill Dams:	11,900,000 cubic yards
Concrete Dams and Diversions:	94,000 cubic yards
Tunnels and Penstocks:	23.2 miles

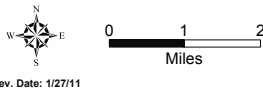
RESERVOIRS AND DIVERSIONS	Elevation	Storage Capacity
Duncan Creek Diversion	5,265'	20 af
French Meadows Reservoir	5,244.5'	134,993 af
Hell Hole Reservoir	4,630'	207,590 af
North Fork Long Canyon Diversion	4,716'	0.39 af
South Fork Long Canyon Diversion	4,640'	0.83 af
Middle Fork Interbay	2,529'	175 af
Ralston Afterbay	1,179'	2,782 af

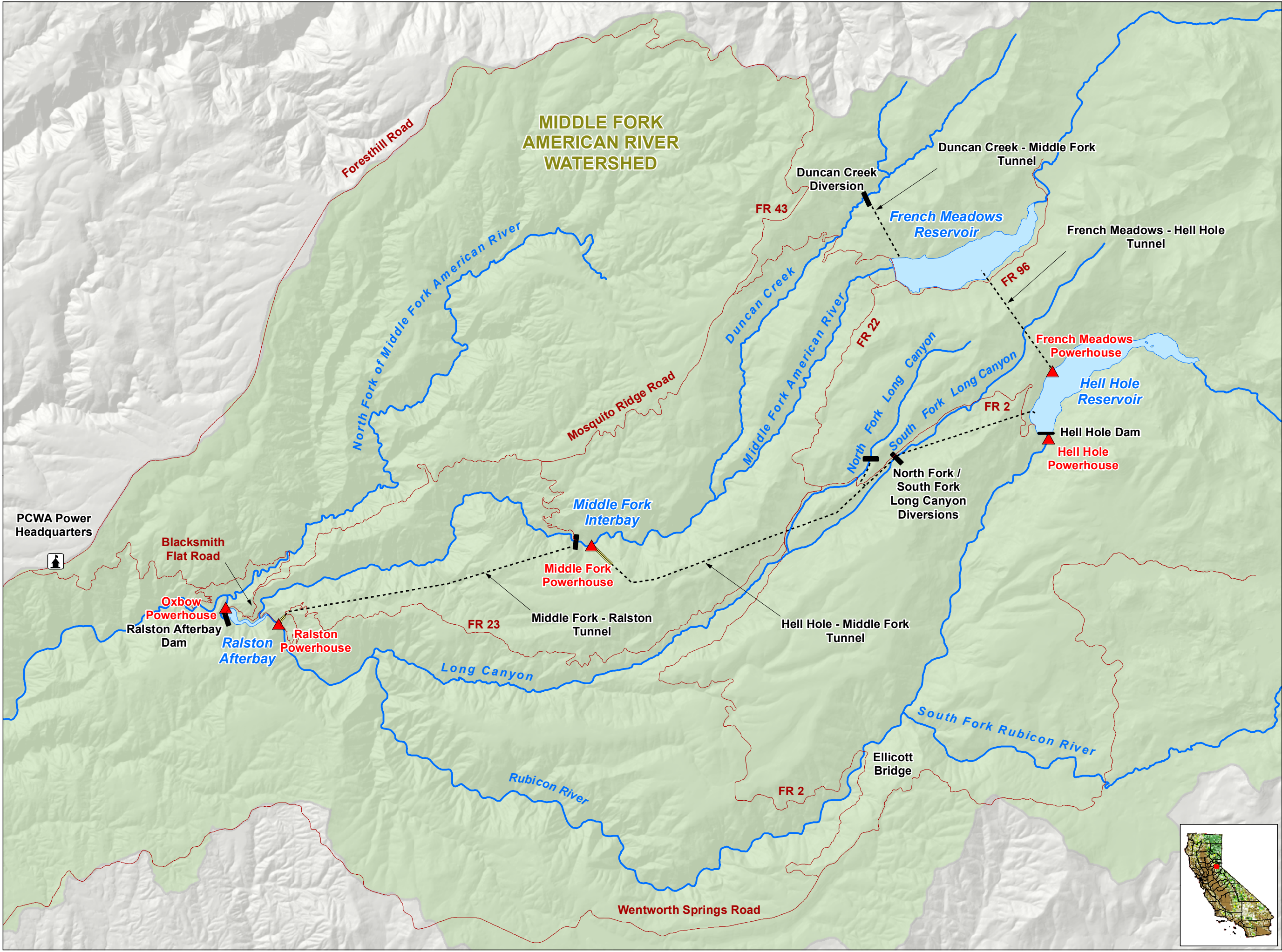
POWERHOUSES		Production Capacity
French Meadows Powerhouse	4,630'	15.3 MW
Hell Hole Powerhouse	4,240'	0.73 MW
Middle Fork Powerhouse	2,529'	122.4 MW
Ralston Powerhouse	1,175'	79.2 MW
Oxbow Powerhouse	1,089'	6.1 MW

TUNNELS		Discharge Capacity
Duncan Creek-Middle Fork Tunnel	-	400 cfs
French Meadows-Hell Hole Tunnel	-	400 cfs
Hell Hole-Middle Fork Tunnel	-	920 cfs
Middle Fork-Ralston Tunnel	-	836 cfs
Ralston-Oxbow Tunnel	-	1,088 cfs



Placer County Water Agency
Middle Fork American River Project
Middle Fork Project and Vicinity





Project Facilities

- ▲ Powerhouse
- Dam
- - - - Tunnel
- ==== Penstock

Transportation

- Road

Hydrography

- Watercourse
- Water Body
- Middle Fork American River Watershed*

*Modified from Calwater Ver. 2.2 to represent drainage above high-water mark of Folsom Lake



Placer County Water Agency
Middle Fork American River Project

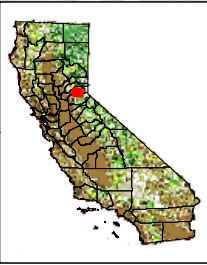
**Middle Fork American River
Project and Vicinity**



Date: 8/17/10



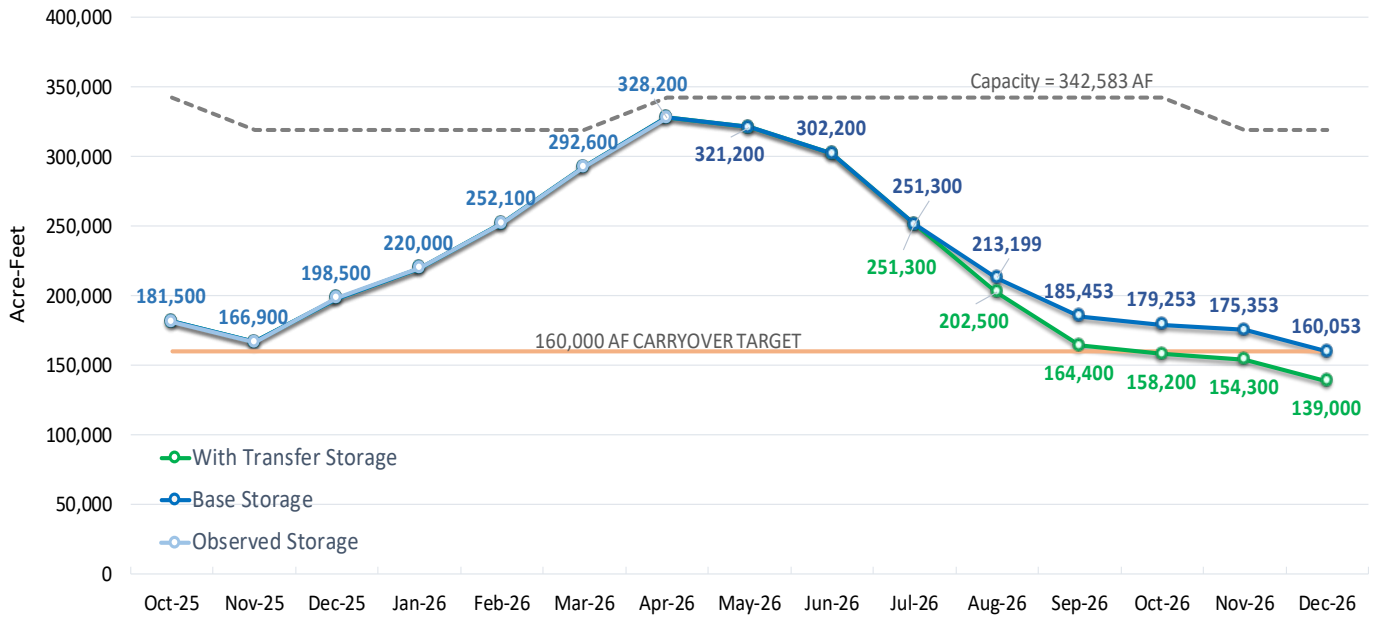
Projection: CA State Plane, Zone 2
Datum: NAD 83



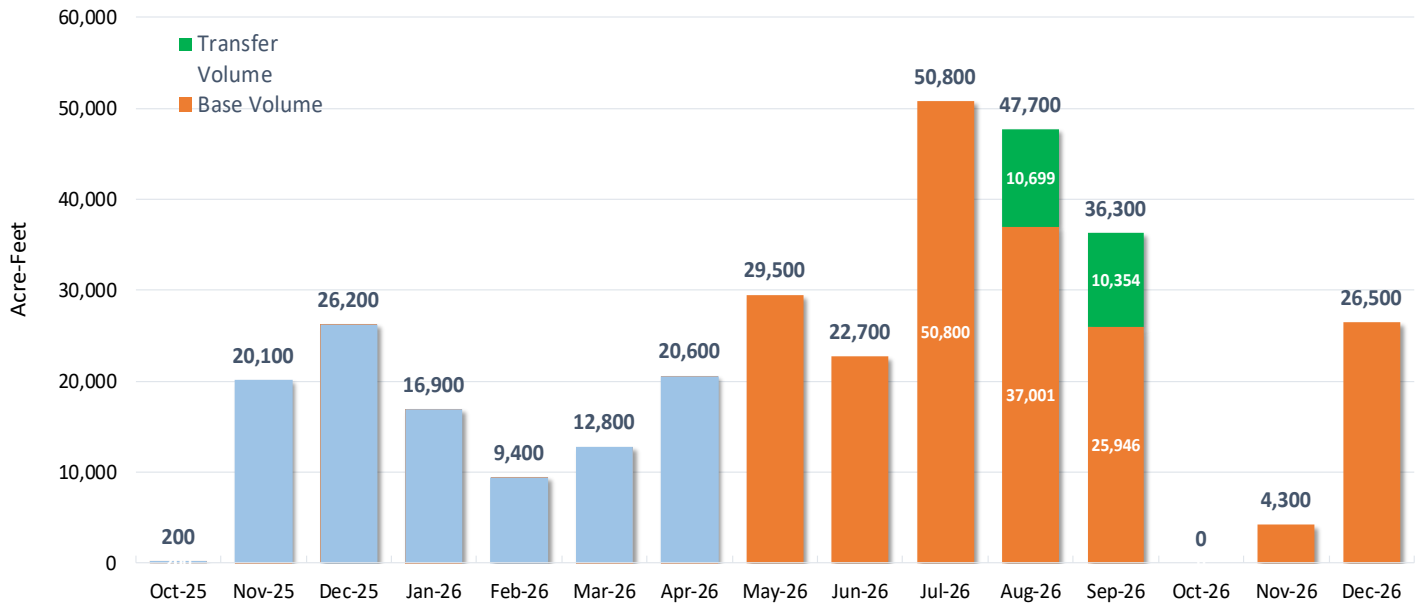
Attachment E

PCWA MFP 2026 Operations Plan

2026 Middle Fork Project Transfer Operations - Storage (AF)



2026 Middle Fork Project Transfer Operations - Middle Fork Powerhouse Releases (AF)



Attachment F(a)

Water Quality Technical Reports

**Placer County Water Agency
Middle Fork American River Project
(FERC No. 2079)**

FINAL

**AQ 11 - WATER QUALITY
TECHNICAL STUDY REPORT - 2007**



Placer County Water Agency
P.O. Box 6570
Auburn, CA 95604

June 2008

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1.0 INTRODUCTION

This report describes water quality studies conducted by the Placer County Water Agency (PCWA) in accordance with the AQ 11 - Water Quality Technical Study Plan (AQ 11 - TSP) for the Middle Fork American River Project (MFP or Project). The stakeholder-approved TSP was included in Supporting Document (SD) H of the Pre-Application Document (PAD) filed with the Federal Energy Regulatory Commission (FERC or Commission) on December 13, 2007 (PCWA 2007). A draft report was distributed to the Aquatics Technical Working Group (TWG) on February 1, 2008 for a 60 day comment period. The comment period ended on April 4, 2008. Oral comments were received at the March 10, 2008 Aquatics TWG meeting and have been addressed in this report. No written comments were received.

Water quality studies were conducted in the vicinity of the MFP during the spring and fall 2007 to characterize the physical, chemical, and bacterial water quality conditions upstream and downstream of Project facilities. The study consisted of summarizing current water quality objectives from the literature, implementing a water quality field sampling field program, and comparing water quality data from field with pertinent regulatory objectives and criteria. In addition, a screening level study of methyl mercury concentrations in sport fish tissue muscle was completed.

The water quality field sampling program included: (1) *in-situ* measurements; (2) collection of water quality samples for laboratory chemical analysis, hereafter referred to as the general water quality sampling; (3) voluntary water quality sampling that enhanced the approach described in the AQ 11 - TSP; (4) coliform sampling; and (5) measurement of water temperature and dissolved oxygen (profiles) in Project reservoirs. Fish for the methyl mercury muscle tissue analysis were also collected from the Project reservoirs and one location in the Middle Fork American River peaking reach (downstream of Oxbow Powerhouse, the lowermost Project facility) near Otter Creek.

The following sections provide a detailed description of the study objectives, study implementation, extent of the study area, study approach, study results, and literature cited.

2.0 STUDY OBJECTIVES

The objective of the water quality studies described in the AQ 11 - TSP is to characterize physical, chemical, and bacterial water quality conditions in the bypass reaches and the peaking reach, comparison reaches, and Project reservoirs and diversion pools and compare to the Central Valley Regional Water Quality Control Board (CVRWQCB 1998) Basin Plan objectives and water quality objectives.

3.0 STUDY IMPLEMENTATION

Figure 11-1 shows the AQ 11 - TSP objective and the study elements and activities that relate to completion of the study. It also shows how information developed through the water quality studies will be documented and provided to the stakeholders. The

following sections summarize the study elements completed, any deviations from the TSP and the rationale, outstanding study elements, and proposed modifications to the TSP.

3.1 STUDY ELEMENTS COMPLETED

The following study elements have been completed:

- Collected *in-situ* and general water quality measurements on the bypass reaches, peaking reaches, reservoirs, and diversion pools in spring (39 locations) and fall (36 locations).
- Collected fecal coliform samples at 17 sites.
- Collected fish samples at Project reservoirs (Hell Hole, French Meadows, Ralston Afterbay, Middle Fork Interbay) and at one river site (Middle Fork American River downstream of Ralston Afterbay) for mercury fish tissue analyses.
- Provided water quality samples to State-certified laboratories approved by the State Water Resources Control Board for chemical analyses.
- Compared water quality results to the CVRWQCB Basin Plan objectives and water quality objectives (CVRWQCB, Fourth Edition revised February 2007).
- Compared fish tissue results to the California's Office of Environmental Health Hazard Assessment (OEHHA) guidelines.

3.2 DEVIATIONS FROM TECHNICAL STUDY PLAN

The water quality studies proceeded as described in the AQ 11 - TSP except for the following deviations:

General Water Quality Sampling

- Water quality samples were not collected during high and low flow events at all of the sampling locations along the peaking reach of the Middle Fork American River during the spring and fall sampling events, as indicated in the TSP. Instead, water quality samples were collected in the peaking reach once during the spring sampling event and again during the fall sampling event. During each event, water quality samples were collected at each of the locations identified in the TSP, under a range of flow conditions.
- One metal (manganese) was not analyzed during the spring sampling event due to a transcription error. Manganese was sampled during the fall sampling event.

Coliform Sampling

- According to the fecal coliform sampling protocols, fecal coliform samples were to be collected five times within a 30 day period between July 4 and Labor Day. Two of the fecal coliform sampling locations were sampled the week after Labor

Day (the fifth sample in 30 days) because of a sampling location change late in the summer. Two of the sampling locations were changed to better meet the water quality sampling objectives. The location changes were agreed to by the Aquatics TWG.

Voluntary Enhancements

- *In-situ* measurements were taken at three additional locations (leakage channels and main channel) downstream of Hell Hole Reservoir and five additional locations (leakage channels and main channel) downstream of French Meadows Reservoir.
- Additional water samples were collected and analyzed for dissolved metals and total mercury due to the presence of a rust-color staining on the substrate and precipitate at these selected locations described above.
- The TSP states that the water quality analytical results would be compared to the Water Quality Control Plan (Basin Plan) for the California Regional Water Quality Control Board Central Valley Region, Fourth Edition, published in September 1998. The analytical results were compared to the most recent version of the Basin Plan, which was updated with amendments in February 2007.

Fish Tissue Sampling

- Five of the 10 recommended fish caught at French Meadows Reservoir (two brown trout and three rainbow trout) were analyzed for individual methyl mercury concentrations in the fish muscle tissue. The remaining five fish (brown trout) that were caught should have been analyzed individually. However, these five fish were analyzed as a composite.

Voluntary Enhancements

- In addition to the ten fish caught at Hell Hole Reservoir (brown trout, rainbow trout, and lake trout that were analyzed for individual methyl mercury concentration), five additional fish (brown trout) were caught and analyzed as a composite sample.

3.3 OUTSTANDING STUDY ELEMENTS

The following describes the only outstanding element of the water quality study:

- Consult with Aquatic TWG to discuss contingency water quality related studies.

3.4 PROPOSED MODIFICATION TO TECHNICAL STUDY PLAN

These are no proposed modifications to the AQ 11 - TSP.

4.0 EXTENT OF STUDY AREA

The study area included bypass and comparison reaches, the peaking reach, Project reservoirs, and diversion pools. The sampled locations are listed in Table AQ 11-1 and are shown on Maps AQ 11-1 and 11-2.

5.0 STUDY APPROACH

This section describes the study approach used to conduct the water quality studies in the study area. This section first describes the sources that were reviewed to identify the existing water quality objectives relevant to the physical, chemical, and bacterial constituents that were analyzed during this study. The section next describes the field sampling methods and associated laboratory analyses methods and reporting employed during the collection of *in-situ* measurements, general water quality sampling, coliform sampling, and fish tissue sampling. This section concludes with a discussion of quality assurance / quality control procedures.

5.1 EXISTING WATER QUALITY OBJECTIVES

Existing water quality objectives for the physical, chemical, and bacterial constituents analyzed in this study were identified by reviewing The Sacramento River Basin and San Joaquin River Basin Water Quality Control Plan (CVRWQCB, Fourth Edition revised February 2007), California Toxics Rule (CTR) “Water Quality Standards: Establishment of Numeric Criteria for Priority Toxic Pollutants for the State of California” (Federal Register, 65 FR 31682, EPA 2000) and the National Toxics Rule (NTR) “Water Quality Standards: Establishment of Numeric Criteria for Priority Toxic Pollutants” (Federal Register, 57 FR 60848, EPA 1992). The Basin Plan includes water quality objectives established by the State Water Resources Control Board (SWRCB) for waters in the Upper American River Watershed. The CTR and NTR, which consider background levels based on criteria that protect both human health and aquatic life, were also reviewed. The SWRCB selects the most controlling (most stringent) of these values to determine compliance with the Clean Water Act.

The California’s Office of Environmental Health Hazard Assessment (OEHHA) guidelines (Cal EPA 2005 and Klasing and Brodberg 2006) were also reviewed for fish tissue analysis.

5.2 WATER QUALITY FIELD SAMPLING PROGRAM

The water quality field sampling program was conducted during spring and fall 2007 and included collection of: (1) *in-situ* measurements; (2) general water quality samples; (3) voluntary enhanced water quality samples; (4) coliform samples; and (5) fish tissue samples. The locations of sampling stations for each of these sampling activities are summarized in Tables AQ 11-1 and 11-3 and are shown on Maps AQ 11-1 through 11-4.

Three spring sampling locations within the Project area were not sampled in the fall. These locations included Duncan Creek above Middle Fork American River confluence

(DC-3 RM0.2) and the Middle Fork American River above and below Duncan Creek confluence (MFAR-3 RM39.9 and MFAR-4 RM39.5). After the spring sampling event and following consultation with the Aquatic TWG, access to these locations was determined to be unsafe for continued sampling.

5.2.1 *In-situ* Measurements

In-situ measurements in the stream and river study reaches were made at each of the sampling locations listed in Table AQ 11-1 during the spring runoff period (May 14 through 31, 2007) and during the low flow (base flow) period in the fall (September 24 through October 3, 2007). The *in-situ* measurements included dissolved oxygen (DO), pH, specific conductance, and water temperature. These four parameters were measured at each sampling location on the stream and river reaches and Middle Fork Interbay using portable multi-probe water quality meters (YSI® or Hydrolab Quanta). Hach Environmental (Loveland, CO) and Equipco (Concord, CA) calibrated the water quality meters prior to the spring and fall sampling events, respectively. In addition, the DO sensor was calibrated in the field to adjust for changes in elevations and barometric pressure at each sampling location prior to data collection. The *in-situ* measurements were taken just below the water surface at representative locations within the stream.

In-situ water quality measurements were also collected during the general water quality sampling program at Project reservoirs (French Meadows Reservoir, Hell Hole Reservoir, and Ralston Afterbay) as outlined in the AQ 11 - TSP (Table AQ 11-1) using portable, multi-probe water quality meters (YSI® or Hydrolab Quanta). A secchi depth was also measured at these locations to determine the clarity of the water column. Middle Fork Interbay was only sampled at the surface as outlined in the AQ 11 - TSP.

5.2.2 General Water Quality Sampling

General water quality samples were collected once during the spring runoff period (May 14 through 31, 2007) and once during the low flow (base flow) period in the fall (September 24 through October 4, 2007) at sampling locations listed in Table AQ 11-1. The location of all the sampling sites were identified using a Global Positioning System (GPS) unit and the coordinates recorded in a field log book. Water quality samples in bypass reaches, peaking reach, and comparison reaches were collected in representative portions of the stream channel, using methods consistent with the Environmental Protection Agency (EPA) 1669 sampling protocol *Sampling Ambient Water for Trace Metals at EPA Water Quality Criteria*. Water quality samples collected from the streams and rivers were analyzed for the parameters listed in Table AQ 11-2, which include a suite of general parameters, dissolved metals, total mercury, and total and fecal coliform.

General water quality samples were also collected once during the spring and fall at Project reservoirs (Table AQ 11-1). In Hell Hole Reservoir, French Meadows Reservoir, and Ralston Afterbay, the samples were collected at the surface and immediately below the thermocline, if the reservoir was thermally stratified. If the Project reservoir was not thermally stratified, then water quality samples were collected at mid-depth of the

reservoir. A boat with gasoline engine was used to access the various reservoir sampling locations. Prior to sample collection, the engine was turned off for five to ten minutes to minimize the potential for sample contamination.

Surface water quality samples from Project reservoirs were collected using similar methods as those used for the stream water quality collection. Sub-surface water quality samples for laboratory analysis were collected using a Teflon® Kemmerer style sampler to ensure integrity of the sample collected from depth. Water quality samples collected from the reservoirs were analyzed for the parameters listed in Table AQ 11-2. Laboratory analysis for hydrocarbons were conducted on water quality samples collected from French Meadows and Hell Hole reservoirs and Ralston Afterbay, where motorized boating may occur.

All water quality samples were decanted into laboratory-supplied sample containers. Sample bottles requiring chemical preservation (HCl, HNO₃, or H₂SO₄) were preserved by Test America Laboratory (Morgan Hill, California). Samples collected for dissolved metals were filtered in the field with pre-cleaned 0.45 µm filtration units supplied by Brooks Rand Laboratory (Seattle, Washington). The sample containers were labeled with the sampling site ID and the date and time that the sample was collected. The sample container was stored on ice and delivered to a State-certified water quality laboratory for analyses in accordance with maximum holding periods. A chain-of-custody record was also maintained with the samples at all times.

5.2.3 Voluntary Enhanced Water Quality Sampling

Voluntary enhanced water quality samples not specified in the AQ 11 - TSP were collected during the spring and fall general water quality sampling program. The additional sampling was initiated by PCWA when field personnel observed and reported the presence of rust color staining of the substrate and a precipitate at select locations below Hell Hole Dam and French Meadows Dam. Based on experience in other relicensing water quality studies, the staining was thought to be result of iron oxidation and warranted further investigation. The locations of the voluntary enhanced water quality samples are described in Table AQ 11-3 and identified on Maps AQ 11-3 and AQ 11-4. The additional samples were collected immediately downstream of Hell Hole Dam (May 22, 2007) and French Meadows Dam (August 6, 2007) in the leakage channels and river locations upstream and downstream of the confluence of the leakage channel. Water quality samples collected from the leakage and river channel were analyzed for hardness, dissolved metals (arsenic, cadmium, copper, iron, lead, manganese, nickel and total chromium), and total mercury.

5.2.4 Coliform Sampling

Total and fecal coliform sampling was conducted to determine if the study waters met Basin Plan objectives for contact recreational activities. Samples were collected at all locations listed in Table AQ 11-1 in the spring (May 14 through 31, 2007) and fall (September 24 through October 3, 2007) concurrent with the general water quality sampling program. These samples were analyzed for total and fecal coliform in accordance with the AQ 11 - TSP.

Sampling for fecal coliform also occurred at near-shore locations adjacent to recreation facilities at Project reservoirs and along bypass reaches where substantial contact recreation (swimming, fishing, rafting, etc.) occurs. These sampling locations were identified in the AQ 11 - TSP and are provided in Table AQ 11-1 and depicted on Map AQ 11-2.

The samples for fecal coliform analysis at 15 of the 17 locations with substantial contact recreation were collected five times within a thirty-day period between August 6, 2007 and Labor Day. The sampling was conducted over Labor Day weekend, rather than July 4th to attempt to capture the highest holiday recreation use. July 4 occurred in the middle of the week in 2007 and therefore recreation use was assumed to be higher during the Labor Day weekend. Two of the coliform sampling locations (FC-9 and FC-11) were not sampled during the first week (August 6, 2007) due to a location change after the first sampling event. Sampling at these two locations extended one additional week after Labor Day until September 10, 2007 in order to complete the 5 samples in a 30-day period.

The sample containers were provided by Diamond Water Laboratory (Auburn, California). The containers were labeled with the sampling site ID and the date and time that the sample was collected. The sample container was stored on ice and delivered to the local State-certified water quality laboratory for analyses in accordance with maximum holding periods. A chain-of-custody record was also maintained with the samples at all times.

5.2.5 Water Quality Laboratory Analysis and Reporting

Water quality samples collected during the general water quality sampling program and coliform sampling were submitted for laboratory analysis at a State-certified laboratory approved by the State Water Resources Control Board (SWRCB) for chemical analysis (total of 31 analytes). The analytes tested are listed in Table AQ 11-2 and are described in Appendix A. Twenty analytes (general parameters and hydrocarbons) were submitted to Test America Laboratory, nine analytes (a suite of dissolved metals and total mercury) were submitted to Brooks Rand Laboratory, and two analytes (total and fecal coliform) were submitted to Diamond Water Laboratory. The laboratories provided reports of each chemical parameter analyzed and the associated laboratory method detection limit, reporting limit, and practical quantification limit.

The reporting units from Test America and Brooks Rand laboratories were reported in mg/L (ppm), µg/L (ppb), or ng/L (ppt). To keep the data results consistent with the reporting parameters listed for the Basin Plan, CTR, and NTR, all lab results were converted to the appropriate unit, if necessary. If these sources do not have a criterion for an analyte, then the units provided in the laboratory reports were used. Conversions between the units are shown in Appendix B.

5.3 WATER TEMPERATURE AND DISSOLVED OXYGEN RESERVOIR PROFILES

Reservoir profiles were completed at selected sampling locations in Hell Hole Reservoir, French Meadows Reservoir, and Ralston Afterbay during the spring and fall sampling period as described in the AQ 11 - TSP. The reservoir profile measurements included water temperature and DO at 1-meter (m) depth intervals to determine if thermal stratification was present. If a thermocline was present, the water quality parameters were measured below the thermocline at 2-m intervals or less to the bottom of the reservoir. If a thermocline was not present, measurements were made at 2-m intervals or less below the mid-depth point to the bottom of the reservoir. Results of the sampling were compiled and presented in tabular and graphical format in Appendix C.

The sampling locations within the Project reservoirs are described below.

Hell Hole Reservoir

Water quality depth profiles and sampling were conducted at three locations on May 30, 2007 and October 1-2, 2007 (Map AQ 11-1). HH-1 was located at the front of the reservoir near the dam, HH-2 was in the middle of the reservoir near the French Meadows Powerhouse, and HH-3 was the upstream most location within the reservoir. Between the spring and fall sampling events, the reservoir water surface elevation steadily declined, resulting in a decrease in the maximum depth sampled. Reservoir storage during the spring and fall sampling events was obtained from the California Department of Water Resources website (DWR 2007), and surface elevations were estimated from PCWA storage capacity curves (PCWA 2007). Water surface elevations were estimated at:

May 30, 2007: 4,583 ft msl

October 1, 2007: 4,514 ft msl.

French Meadows Reservoir

Water quality depth profiles and sampling were conducted at three locations on May 30, 2007 and October 3, 2007 (Map AQ 11-1). FM-1 was located at the front of the reservoir near the dam, FM-2 was in the middle of the reservoir, and FM-3 was just downstream from the French Meadows boat ramp in the middle of the reservoir. Between the spring and fall sampling events, the reservoir water surface elevation steadily declined, resulting in a decrease in the maximum depth sampled. Reservoir storage during the spring and fall sampling events was obtained from the California Department of Water Resources website (DWR 2007), and surface elevations were estimated from PCWA storage capacity curves (PCWA 2007). Water surface elevations during the spring and fall sampling events were estimated at:

May 30, 2007: 5,243 ft msl

October 3, 2007: 5,206 ft msl.

Ralston Afterbay

Water quality depth profiles and sampling were conducted at one location just behind the float barriers on May 29, 2007 and September 26, 2007 (Map AQ 11-1). Water surface elevations during the spring and fall sampling events were estimated by PCWA at:

May 29, 2007: 1,177 ft msl

September 26, 2007: 1,175 ft msl.

Monthly reservoir profiles (consisting of temperature, DO, and specific conductance) at the same reservoir locations described above were also completed by PCWA in 2005-2007 as part of early relicensing studies. The results of the 2005 and 2006 reservoir profiles are presented in the PAD, SD (G) (PCWA 2007). The 2007 reservoir profile results will be summarized in early 2008 and provided to the Aquatics TWG under separate cover.

5.4 FISH TISSUE COLLECTION AND ANALYSIS FOR METHYL MERCURY

A screening level study of methyl mercury concentrations in sport fish muscle tissue was conducted at selected locations in the study area. As identified in the AQ 11 - TSP, at least 10 non-hatchery sport fish of edible size were collected from each of the following locations: Hell Hole Reservoir, French Meadows Reservoir, Middle Fork Interbay, Ralston Afterbay, and the Middle Fork American River near the Otter Creek confluence. Larger fish and species with greater potential for bioaccumulation were targeted for collection and analysis. The initial goal of the study was to collect five fish each of two different species from each location based on the following priority ranking. The two species present with the highest priority ranking would be targeted for collection (1 = highest priority) as follows:

- 1) bass
- 2) pikeminnow
- 3) lake trout
- 4) brown trout
- 5) rainbow trout

If five fish of two different species were not caught, then fish from a third species was included in the analysis.

At the four reservoirs, fish were captured in clean nylon gill nets. In the Middle Fork American River near Otter Creek fish were captured by electrofishing and hook-and-line sampling. For each fish collected, the species, fork length, total length, and weight were recorded.

The field handling procedures were consistent with those outlined in California Environmental Protection Agency (Cal EPA 2005) and those used at the Department of Fish and Game Marine Pollution Studies Laboratory at Moss Landing (Method # MPSL-

102a). The fish were placed into zipper-closure bags and immediately placed on ice in a cooler. The fish were then stored in a freezer prior to shipment to the analytical laboratory. All fish were shipped in an ice chest packed with ice and delivered by an overnight courier to Brooks Rand Laboratory (Seattle, Washington). Each cooler was shipped with a chain of custody form showing the sample identification number and collection date and time of each sample.

Muscle tissue from individual fish was analyzed for concentrations of methyl mercury in accordance with the General Protocol for Sport Fish Sampling and Analysis developed by the Cal EPA (2005) and with methods comparable to those used at the Department of Fish and Game Marine Pollution Studies Laboratory at Moss Landing. The results of the fish fillet analyses were reported in ng/g. These were converted to mg/kg fish (ppm) to be consistent with the OEHHA guidelines. The conversion is provided in Appendix B.

In one instance at French Meadows Reservoir, five brown trout were sent to the laboratory for analysis as one composite sample. For Hell Hole Reservoir, in addition to the 10 individual fish analyzed, a composite sample of five brown trout was analyzed.

5.5 QUALITY ASSURANCE/ QUALITY CONTROL PROCEDURES

Standard precautions were established for the collection of water quality samples. At each station, all samples were collected by the same person, wearing ultra-trace sampling gloves. Water quality samples were collected using the designated collection bottle supplied by the appropriate laboratory. Upon collection, each sample was immediately labeled with the date and time and logged on a chain-of-custody form and placed into a cooler filled with ice.

Water quality samples were delivered to the analytical laboratory within the appropriate holding times. Coliform samples were delivered to the laboratory on the same day of collection, while all other samples were delivered between 24 to 48 hours of the sample collection time by courier. A chain-of-custody form accompanied all samples from the time of collection to delivery and submittal to the analytical laboratory.

In-stream water samples were collected just below the water surface in areas of steady flow. Water samples from the reservoirs and impoundments were collected below the water surface following the same quality control (QC) procedures. Additional precautions were followed when sampling from a motorized boat. Samples were collected from the bow of the boat after the motor was turned off for at least five to ten minutes to avoid possible hydrocarbon contamination from the motor boat. Sampling equipment was cleaned with a cleaning solution and distilled water prior to sample collection.

Standard quality assurance (QA) procedures were performed by the laboratories during analyses of water samples. These included matrix and laboratory spikes and spike duplicates, matrix duplicates, and method blanks as appropriate. A summary of the QA measures were included with each certified laboratory report.

A QA/QC screening level review was also conducted on all of these laboratory analytical reports. Results of the QA/QC review are presented in Appendix D.

6.0 STUDY RESULTS

6.1 REVIEW OF EXISTING WATER QUALITY OBJECTIVES

The Basin Plan identifies specific water quality objectives of allowable limits or levels of water quality constituents. These objectives are established for the protection of beneficial uses of the waters associated with the MFP (CVRWQCB 2007). If water quality is maintained at levels that meet these objectives, the beneficial uses of the waters are considered to be protected. The beneficial uses identified in the Basin Plan that pertain to water associated with the MFP include: (1) municipal and domestic supply; (2) agricultural irrigation and stock watering; (3) power generation; (4) contact recreation; (5) non-contact recreation; (6) coldwater habitat and spawning habitat for fisheries; and (7) wildlife habitat. The definition of each of these beneficial uses is provided in Table AQ 11-4.

Water quality objectives include both numeric and narrative objectives (Table AQ 11-2). The Basin Plan provides specific numeric objectives for bacteria, *in-situ* measurements, and for chemical or metal constituents. The objectives for chemical and metal constituents are derived from various sources such as maximum contaminant levels (MCLs) that are provided in Title 22 of the California Code of Regulations or from the CTR or NTR. The most stringent objectives were used for this study.

Often more stringent objectives are provided by the CTR and the NTR to protect aquatic life and human health. The CTR and NTR numeric objective for cadmium (Cd), copper (Cu), lead (Pb) and nickel (Ni) is more stringent than the Basin Plan objective. The CTR and NTR have established more stringent criteria for these metals to protect freshwater aquatic life. The CTR and NTR set acute and chronic criteria that are hardness-dependent and must be calculated on a location-by-location basis. For each of these metals, the water quality criterion decreases with decreasing water hardness. These calculated criteria and laboratory results are shown in Tables AQ 11-9, AQ 11-12, and AQ 11-15. The formulas for calculating hardness-dependent criteria are provided in the CTR and NTR guidance documents (US EPA 2007 and 2007a).

The Basin Plan also specifies a water temperature thermal heating objective that states, "Natural water temperatures shall not be altered unless it can be demonstrated to the satisfaction of the Regional Board that such alteration does not adversely affect beneficial uses. At no time or place shall the temperature be increased more than 5°F (2.8°C) above the natural receiving water."

Several of the parameters analyzed do not have established objectives. Various literature sources were reviewed for each parameter to identify guidelines or ranges of the different parameters that might be expected for the MFP area. The ranges are described in Appendix A.

The results of the water quality sampling field program were compared to the most stringent water quality objectives identified Table AQ 11-2. The locations where the objectives have not been met were identified and are discussed in the following results section.

6.2 WATER QUALITY SAMPLING AND ANALYTICAL RESULTS

The following sections provide a discussion of the results of the water quality field sampling program (including the *in-situ* measurements, general water quality sampling, voluntary enhanced water quality sampling, and coliform sampling) associated with the spring and fall sampling events. Within this section the results from the stream and river reaches are discussed first, followed by the results of the sampling on Project reservoirs. The results of the *in-situ* measurements and coliform sampling for the spring and fall sampling events are summarized below. For the other general water quality parameters in the streams and rivers, only those that do not meet the most stringent Basin Plan, CTR, or NTR water quality objective are summarized.

6.2.1 Water Quality Results from Streams and Rivers

All the parameters measured in Project area streams and rivers during the spring and fall sampling event met with the Basin Plan, CTR, and NTR objectives with the exception of dissolved oxygen at three locations near the confluence of Duncan Creek and Middle Fork American River in the spring, and manganese in the fall at one location on the Middle Fork American River below French Meadows Dam at the gaging station.

***In-situ* Field Measurements**

The results of *in-situ* measurements collected in streams and rivers in the vicinity of the MFP during the sampling periods are shown in Tables AQ 11-5 and 11-6. The results of the measurements indicate that three sampling locations did not meet the Basin Plan objectives for dissolved oxygen in the spring. All measurements met the Basin Plan objectives for pH. There are no Basin Plan objectives for temperature, and specific conductance, but measurements were all within expected ranges.

Dissolved Oxygen

According to the Basin Plan objectives, DO concentrations shall not be reduced below a minimum level of 7.0 mg/L for waters designated as COLD. DO concentration will vary with other parameters such as temperature, elevation, photosynthetic activity, biotic activity, stream discharge, and the concentration of other solutes (Hem 1989, Michaud 1994). Increasing temperature or elevation will result in lower DO (MELP 1998).

Dissolved oxygen measurements typically ranged between 7.1 and 11.7 during the spring and fall sampling events. These measurements are consistent with Basin Plan objective. However, at three locations during the spring sampling event, DO was below the Basin Plan objective of 7.0 mg/L. These locations included Duncan Creek above Middle Fork American River confluence (DC-3 RM0.2) and the Middle Fork American River above and below the Duncan Creek confluence (MFAR-3 RM39.9 and MFAR-4

RM39.5). DO concentrations at these locations were measured at 6.2 and 6.3. Based on DO concentrations measured at locations upstream and downstream from these sampling locations, these data are believed to be incorrect due to instrument malfunction or sampling error. These locations were not sampled in the fall due to the unsafe field conditions accessing the sampling locations.

Water Temperature

Measured surface water temperatures generally warm in the downstream direction during both the spring and fall sampling events (Tables AQ 11-5 and AQ 11-6).

Additional water temperature monitoring in rivers and streams in the vicinity of the MFP have been conducted by PCWA as part of ongoing studies. Water temperature data has been collected annually from 2005 through 2007. This monitoring program will continue through summer 2008. The data collected will be summarized and used to evaluate compliance with temperature objectives defined in the Basin Plan. Preliminary water temperature data are presented in the PAD, SD (G), 2005 Water Temperature Report and the 2006 Water Temperature Report (PCWA 2007).

pH

According to the Basin Plan, pH should not be below 6.5 or above 8.5. Furthermore, changes in normal ambient pH levels shall not exceed 0.5 in fresh waters designated as COLD or WARM beneficial uses. Values above 9.5 or below 4.5 are considered lethal to aquatic organisms (EPA 1996; MELP 1998).

Measured pH values were within the range required in the Basin Plan (between 6.5 and 8.5) at all sampling locations.

Specific Conductance

There are no specific Basin Plan objectives for specific conductance. The conductivity of freshwater at 25° C varies between 50 and 1,500 µS/cm (Hem 1989; MELP 1998).

Specific conductance measurements during the spring sampling event ranged from 51 to 82 µS/cm and ranged from 16 to 107 µS/cm during the fall sampling event (Tables AQ 11-5 and AQ 11-6).

General Water Quality Parameters

The laboratory analytical results for the spring and fall sampling programs are summarized in Tables AQ 11-7 through AQ 11-12. Electronic copies of laboratory reports are available on CD. The analytes collected and submitted for laboratory analysis including 17 general parameters, eight dissolved metals, and total mercury. Refer to Table AQ 11-2 for the list of analytes.

During the spring and fall sampling events, all general parameters measured and total mercury samples met the Basin Plan, CTR, or NTR objectives, or were within the expected ranges for the ones that do not have established objectives. All dissolved metal analyses with the exception of dissolved manganese at one location (Middle Fork American River below French Meadows Dam at gaging station) met Basin Plan, CTR, or NTR objectives. The results of the general water quality parameters are summarized in Tables AQ 11-7 through AQ 11-12.

Manganese

The Basin Plan objectives for manganese is 50 µg/L. One sampling location below French Meadows Reservoir, MFAR-2 RM46.6 (Middle Fork American River below French Meadows Dam at gaging station) did not meet the Basin Plan objective (Figure AQ 11-2). The laboratory measured a concentration of 57.7 µg/L. Manganese was not analyzed during the spring sampling event, so it is unknown if MFAR-2 RM46.6 met the Basin Plan objective in the spring (runoff flow). Manganese concentrations in the fall (base flow) met the Basin Plan objective at the sampling locations farther downstream on the Middle Fork American River (Table AQ 11-10).

Voluntary Enhanced Water Quality Sampling

Voluntary enhanced water quality samples, not specified in the AQ 11 - TSP, were collected immediately downstream of Hell Hole Dam (May 22, 2007) and French Meadows Dam (August 6, 2007) in the leakage channels and river locations upstream and downstream of the confluence of the leakage channel. Three locations were sampled below Hell Hole Dam and five locations were sampled below French Meadows Dam. Analyses included *in-situ* measurements, calculated hardness, eight dissolved metals, and total mercury. Flows within the leakage weirs below French Meadows and Hell Hole dams are provided in Appendix E.

Similar to the discussion above, the *in-situ* measurements collected are summarized at each location and only the water quality objectives that did not meet the Basin Plan, CTR or NTR objectives are discussed. The *in-situ* measurements and sampling results are presented in Tables AQ 11-13 through 11-15.

Hell Hole Dam

In Situ Field Measurements

All in-situ field measurements collected below Hell Hole Dam met Basin Plan objectives or were within the expected ranges for the ones that do not have established objectives.

General Water Quality Parameters

The three voluntary enhanced water quality samples collected below Hell Hole Dam met all listed Basin Plan, CTR and NTR objectives.

French Meadows Dam

In Situ Field Measurements

In-situ measurements results indicated that pH and DO did not meet water quality objectives.

- *pH*

The five sampling locations below French Meadows Dam were all below the Basin Plan objective of 6.5 and ranged between 5.3 and 5.3. The results are listed in Table AQ 11-13.

- *Dissolved Oxygen*

Two sampling locations (FM-D and FM-E, both located within the main channel) below French Meadows Dam met the Basin Plan objective of 7.0 mg/L. Three sampling locations in the leakage channel (FM-A, FM-B, and FM-C) did not meet the Basin Plan objective and were below 7.0 mg/L. The results are listed in Table AQ 11-13 and are shown in Figure AQ 11-2.

General Water Quality Parameters

Iron and manganese concentrations in the five samples collected below French Meadows Dam exceeded Basin Plan or NTR objectives. These locations are shown with the sampled locations further downstream in Figure AQ 11-2. All other analytes met the listed Basin Plan or NTR objectives (Tables AQ 11-14 and AQ 11-15).

- *Iron*

The Basin Plan objective for iron is 0.3 mg/L and the NTR objective is 1 mg/L. The Basin Plan specifies a criterion for iron of 0.3 mg/L, based on secondary maximum contaminant levels for drinking water. This criterion is based on a taste, odor, and visual threshold (CTR 2000). When iron is precipitated out of solution due to oxidation, it causes a reddish brown color in the water. The EPA has recommended a value of 1.0 mg/L for a 4-day average continuous concentration for the protection of freshwater aquatic life.

Three of the five samples collected below French Meadows Dam did not meet the Basin Plan and NTR objectives for iron and ranged from 16.0 mg/L to 20.4 mg/L. All of these locations are in the small leakage channels draining from the base of French Meadows Dam. These locations are shown on Map AQ 11-4. The laboratory results for iron are summarized in Table AQ 11-14 and Figure AQ 11-2.

Iron staining was observed along the ground and drainage channels at these three locations, as well as in the Middle Fork American River channel downstream. However, iron results in the plunge pool at the outlet pipe for French Meadow Reservoir (FM-E) and several hundred feet downstream (FM-D) met the Basin Plan and NTR objectives.

- *Manganese*

The Basin Plan objective for manganese is 50 µg/L and is based on secondary maximum contaminant levels for drinking water. Four of the five locations sampled below French Meadows Dam did not meet the Basin Plan objective. Three of these locations are in the small leakage channels draining from the base of French Meadows Dam (results range from 3,610 µg/L and 4,040 µg/L) and the fourth is in the channel downstream of the dam (62.6 µg/L). These locations are shown on Map AQ 11-4. The laboratory results are summarized in Table AQ 11-14 and Figure AQ 11-2.

Coliform Sampling

Total and fecal coliform samples were collected from streams and rivers in the vicinity of the MFP to determine if study waters met Basin Plan objectives for recreational activities. Coliform concentrations are reported at the number of bacteria colonies per 100 mL of sample water (MPN/100 mL). An objective of 200 colonies/100 mL was used to determine if fecal coliform concentrations met Basin Plan objectives for contact recreational activities. There are no Basin Plan objectives for total coliform.

Total and fecal coliform samples were collected during the spring and fall sampling events (Map AQ 11-2). The laboratory results of the total and fecal coliform concentrations are provided in Tables AQ 11-7 and AQ 11-10 and are summarized below.

The fecal coliform results met Basin Plan objectives during the spring sampling event and ranged from less than 2 to 4/100 mL. Total coliform results during the spring sampling event ranged from less than 2/100 mL to 30/100 mL.

During the fall sampling event, one location (NFLC-2 RM2.9) exceeded the objective for fecal coliform (300/100 mL). The remainder of the fecal coliform results met Basin Plan objectives. Total coliform results ranged from less than 2/100 mL to 900/100 mL.

30-Day, Five Sample Fecal Coliform Sampling

The Basin Plan states that "...the fecal coliform concentration, based on a minimum of not less than five samples for any 30-day period, shall not exceed a geometric mean of 200/100 mL, nor shall more than ten percent of the total samples during any 30-day period exceed 400/100 mL." Seventeen locations throughout the study area were sampled five times over a 30-day period (Table AQ 11-16 and Map AQ 11-2). Sampling began on August 6, 2007 and continued for five subsequent weeks and concluded on Labor Day. At two locations (FC-9 and FC-11), sampling continued until September 10, 2007 due to a sampling location change after the first sampling event on August 6, 2007.

The geometric mean at each of the 17 sampling locations was below the objective of 200/100 mL. However, at one location (FC-15, Ralston Afterbay near the Ralston picnic area) on August 27, 2007, the sample result was 1,600/100 mL. Although, the

geometric mean at this location was 30/100 mL, which is below the Basin Plan objective.

6.2.2 Water Quality Results: Reservoir Profiling and Laboratory Analysis

Water quality depth profiles and the water quality sampling program (including *in-situ* measurements, secchi depth, general water quality sampling, and coliform sampling) associated with the spring and fall sampling events were conducted at various locations in Hell Hole Reservoir, French Meadows Reservoir, and Ralston Afterbay. The following provides a summary of the water quality profiling and sampling results for Ralston Afterbay, Hell Hole Reservoir, and French Meadows Reservoir. The temperature and DO profiling measurements are presented in Appendix C. The results of the profiles and *in-situ* measurements are summarized for each reservoir. For the other general water quality parameters, only those that do not meet the most stringent Basin Plan, CTR, or NTR water quality objectives are summarized.

All parameters measured in Hell Hole Reservoir, French Meadows Reservoir, and Ralston Afterbay during the spring and fall sampling program met with the Basin Plan, CTR, and NTR objectives with the exception of dissolved oxygen in Hell Hole and French Meadows reservoirs.

Hell Hole Reservoir

Water Quality Temperature and Dissolved Oxygen Profile Results

The spring water temperature profiles at the three sampling locations were similar. Spring surface temperatures ranged from 12.7°C at HH-3 to 14.5°C at HH-1. Temperatures steadily declined with depth until 30 to 35m below the water surface, where temperatures remained relatively steady at 6 to 7°C down to the bottom of the reservoir. The fall temperature profiles at the three locations were also similar. Fall surface temperatures were slightly warmer than spring surface water temperatures. Fall water temperatures varied only slightly with depth from the surface to approximately 35 to 40 m. At greater depths, temperatures steadily declined to 11 to 15°C. Reservoir bottom temperatures were approximately 5 to 7°C warmer in the fall than those recorded during the spring sampling event. There was no distinct thermal stratification or thermocline measured in either the spring or fall temperature profiles.

The DO profiles during the spring sampling were similar between the three locations. DO concentrations ranged from 8.1 mg/L to 8.8 mg/L at the surface and ranged from 8.4 mg/L to 8.7 mg/L near the bottom. DO concentrations varied little with depth. The spring DO profiles were also similar between each sampling location. Fall concentrations were slightly lower than those measured during the spring sampling event. Surface concentrations ranged from 6.3 mg/L to 7.1 mg/L and decreased to 5.4 mg/L to 5.8 mg/L near the bottom of the reservoir. DO concentrations had a slight decreasing trend with depth. The DO concentrations for most of the three sampling locations during the fall sampling events were below the Basin Plan objective of 7.0 mg/L for COLD water bodies except at the surface for HH-1. The lowest DO

measurement of 5.4 mg/L was recorded at the bottom of the reservoir at the HH-2 sampling location. Based on other DO concentrations collected in the fall in 2005 and 2006 from Hell Hole Reservoir (PCWA 2007), these fall 2007 data from Hell Hole Reservoir are believed to be incorrect due to instrument malfunction or sampling error.

In-Situ Field Measurements

In-situ measurements were collected at the surface and at approximately mid-depth in the profile. The sampling depths at the three locations for the spring and fall sampling events are shown below.

Site ID	Spring Sampling Depths (m)	Fall Sampling Depths (m)
HH-1	0 and 30	0 and 23
HH-2	0 and 30	0 and 27
HH-3	0 and 30	0 and 20

The results of the measurements are shown in Tables AQ 11-5 and AQ 11-6.

In-situ temperature and DO measurements followed the same trends as discussed above in the profiles for the spring and fall sampling events. Surface water temperatures were warmer than the mid-depth measurements. DO concentration measurements were slightly higher at mid-depth than at the surface for the spring sampling, but were slightly lower at two of the three sampling locations in the fall.

All pH measurements are within the objective listed in the Basin Plan. Surface pH measurements were higher than mid-depth measurements for all three sampling locations during the spring and fall sampling events. Surface pH measurements ranged from 6.9 to 7.1 in the spring and 6.7 to 7.9 in the fall. Mid-depth pH measurements ranged from 6.7 to 6.8 in the spring and 6.8 to 7.1 in the fall. Surface pH measurements were greater in the fall than in the spring at HH-1 and HH-3, but were less at HH-2. All mid-depth pH measurements were greater during the fall sampling event than in the spring sampling event.

Specific conductance measurements were similar between the surface and mid-depth and between the spring and fall sampling events. Spring measurements were approximately 20 μ S/cm and fall measurements were ranged between 30 and 40 μ S/cm.

Secchi depth measurements were conducted at the three sampling locations. The secchi depths for each sampling location during the spring and fall sampling events are shown below.

Site ID	Spring Sampling Secchi Depth (m)	Fall Sampling Secchi Depth (m)
HH-1	9	10
HH-2	11	10
HH-3	8	9.4

General Water Quality Parameters

All the spring and fall parameters analyzed met the Basin Plan, CTR, or NTR objectives. All sampling locations were within or below the suggested ranges discussed in Appendix A for parameters analyzed without established objectives.

Coliform Sampling

All fecal coliform concentrations met the 200/100 mL objective during the spring and fall sampling events.

French Meadows Reservoir

Water Quality Temperature and Dissolved Oxygen Profile Results

The spring water temperature profiles at the three locations were similar (surface temperatures at approximately 16°C). Temperatures steadily declined until approximately 20 m in depth, where temperatures remained relatively steady at 7 to 8°C down to the bottom. The fall temperature profiles at the three locations were similar with surface temperatures (approximately 15°C) and were slightly cooler than spring surface water temperatures. Fall water temperature profiles were different from the spring water temperature profiles. In the fall, water temperatures varied only slightly in depth from the surface to approximately 20 m. Below this depth, temperatures rapidly declined to 8°C at FM-1 and FM-2. Bottom temperatures were warmer at FM-3 (the shallowest location) than at the other two sampling locations. A thermocline was measured in the spring temperature profiles between 10 and 15 m and during the fall between 20 and 25 m.

The DO profiles during the spring sampling were similar at the three locations. Spring DO concentrations ranged from 7.7 mg/L to 7.9 mg/L at the surface and generally increased to the thermocline, then slowly decreased to the bottom of the reservoir. DO concentrations near the bottom of the reservoir ranged from 6.1 mg/L to 8.4 mg/L. The fall DO profiles were also similar at each sampling location. Fall DO surface concentrations were slightly higher than during the spring sampling event. Surface concentrations ranged from 8.2 mg/L to 8.5 mg/L and stayed relatively constant down to the thermocline. DO concentrations then increased at the thermocline (only at FM-1 and FM-2), followed by decreasing concentrations to the bottom of the reservoir (4.3 mg/L to 7.4 mg/L). The DO concentrations for most of the three sampling locations during the spring and fall sampling events met the Basin Plan objective of 7.0 mg/L for COLD water bodies. DO measurements below 7 mg/L were measured at FM-1 during the spring, and at FM-2 during the spring and fall near the bottom of the reservoir sampling areas.

In-Situ Field Measurements

In-situ measurements were collected at the surface and at approximately mid-depth or at the thermocline. The sampling depths at the three locations for the spring and fall

sampling events are shown below. The results of the measurements are shown in Tables 11-5 and 11-6.

Site ID	Spring Sampling Depths (m)	Fall Sampling Depths (m)
FM-1	0 and 30	0 and 22.5
FM-2	0 and 20	0 and 22.5
FM-3	0 and 15	0 and 22.5

In-situ temperature and DO measurements followed the same trends as discussed above in the profiles for the spring and fall sampling events. Surface water temperatures were warmer than the mid-depth measurements. DO concentration measurements were slightly higher at mid-depth than at the surface for the spring sampling. In comparison, in the fall, DO concentrations were greater at the surface than at mid-depth.

All pH measurements were within the acceptable ranges of 6.5 to 8.5, as listed in the Basin Plan. Surface pH measurements were higher than mid-depth measurements for all three sampling locations during the spring and fall sampling events. Spring surface and mid-depth pH measurements were overall slightly higher during the fall sampling event. Surface pH measurements ranged from 6.6 to 6.9 in the spring and from 7.2 to 7.9 in the fall. Mid-depth pH measurements ranged from 6.5 to 6.6 in the spring and from 6.5 to 6.7 in the fall.

Specific conductance measurements were similar between the surface and mid-depth and between the spring and fall sampling events. Spring measurements were approximately 30 $\mu\text{S}/\text{cm}$ and fall measurements were approximately 20 $\mu\text{S}/\text{cm}$.

Secchi depth measurements were conducted at the three sampling locations during the spring event. Measurements were taken at only one location during the fall event due to high winds on the reservoir later in the day. The winds and water currents would have prevented accurate secchi depth measurements, as the disk would not drop vertically, skewing the results. At the one sampling location, water clarity was better during the fall than during the spring. The secchi depths for each sampling locations during the spring and fall sampling events are shown below.

Site ID	Spring Sampling Secchi Depth (m)	Fall Sampling Secchi Depth (m)
FM-1	6.5	9.5
FM-2	7.5	Too Windy*
FM-3	7	Too Windy*

*Conditions on the reservoir were too windy for collecting accurate measurements.

General Water Quality Parameters

All the spring and fall parameters analyzed met the Basin Plan, CTR, or NTR objectives. All sampling locations were within or below the expected ranges discussed in Appendix A for parameters analyzed without established objectives.

Coliform Sampling

All fecal coliform concentrations met the 200/100 mL objective during the spring and fall sampling events.

Ralston Afterbay

Water Quality Temperature and Dissolved Oxygen Profile Results

Spring surface temperature in Ralston Afterbay was measured at 19 °C and decreased to 10.5 °C near the bottom of the afterbay. In comparison, temperatures in the fall were fairly constant with depth, ranging from 13.5 °C at the surface to 12 °C near the bottom. Some thermal stratification was present during the spring profiling event, but not during the fall profiling event.

The DO at the surface was 10.3 mg/L and 11.0 mg/L for the spring and fall sampling events, respectively. The concentration of DO generally increased with increasing depth (and with decreasing water temperature) to 10 m below the water surface. During the spring when the depth exceeded 10 m, DO concentrations decreased. DO concentrations ranged between 10.0 mg/L and 11.6 mg/L during both sampling events throughout the entire profile.

In-Situ Field Measurements

In-situ measurements were collected at the surface and at approximately mid-depth in the profile. The sub-surface measurements were collected at 6 m and at 5 m during the spring and fall sampling events, respectively. The results of the measurements are shown in Tables AQ 11-5 and AQ 11-6.

In-situ temperature and DO measurements followed the same trend as discussed above in the profiles for the spring and fall sampling events. Surface water temperatures were warmer than the mid-depth measurements and conversely, DO measurements were higher at mid-depth than at the surface.

In-situ pH measurements were between 6.0 and 7.0, acceptable limits within the Basin Plan. Spring pH measurements were 6.6 at the surface and 6.5 at mid-depth. Fall pH measurements were 7.0 at the surface and 6.8 at mid-depth.

Specific conductance measurements were similar between the surface and mid-depth and between the spring and fall sampling events. Spring measurements ranged between 30 and 50 µS/cm. Fall measurements ranged between 30 and 40 µS/cm.

Secchi depth measurements were also collected at the sampling location. Water clarity remained the same between the two sampling periods, with secchi depth readings of 7 m for both the spring and fall sampling events.

General Water Quality Parameters

All the spring and fall parameters analyzed met the Basin Plan, CTR, or NTR objectives. In addition, the results of the analyses for the parameters without established objectives were within the expected ranges discussed in Appendix A.

Coliform Sampling

All fecal coliform concentrations met the 200/100 mL objective during the spring and fall sampling events.

6.3 FISH TISSUE ANALYSIS

The following section provides a discussion of the fish tissue analysis from the Project reservoirs, Ralston Afterbay, Middle Fork Interbay, and the Middle Fork American River near Otter Creek. Laboratory analyses of methyl mercury were conducted on muscle tissue samples from individual and composite fish samples. The screening value for methyl mercury in fish established by the OEHHA to determine if additional studies are warranted is 0.08 ppm (which is equal to 0.08 mg/kg fish).

Methyl mercury concentrations in at least one fish from each location exceeded the OEHHA screening value of 0.08 mg/kg fish. Twenty-three of the 45 individual fish analyzed exceeded the screening value. The highest concentrations (up to 1.140 mg/kg) were measured in fish from Hell Hole Reservoir, where the largest fish were caught. A summary of the fish that were caught, including the species, fork and total lengths, and weight, is provided in Table AQ 11-17. The direct relationship between methyl mercury concentrations and the weight of the fish for each of the sampling locations is shown in Figure AQ 11-3. The results of the fish tissue sampling at each location are summarized below.

In Hell Hole Reservoir, eight of the ten individual fish analyzed (brown trout, lake trout, and rainbow trout), as well as the composite sample of brown trout, exceeded the OEHHA guidelines. Methyl mercury concentrations in the fish tissue from Hell Hole Reservoir ranged from 0.004 mg/kg fish to 1.14 mg/kg fish. All the brown trout analyzed exceeded the screening level.

In French Meadows Reservoir, three of the five individual fish, including both brown trout exceeded 0.08 ppm. The composite sample of five brown trout also exceeded the screening value. The highest methyl mercury concentration measured in the fish from French Meadows Reservoir was 0.357 mg/kg fish.

Only one of the ten brown and rainbow trout caught in Middle Fork Interbay exceeded the screening value. The concentration of the rainbow trout measured was 0.135 mg/kg fish.

Eight of the ten fish caught, including all the Sacramento pikeminnows and the four largest brown trout, in Ralston Afterbay exceeded the screening value. The highest concentration measured in the fish caught in Ralston Afterbay was 0.348 mg/kg fish.

Methyl mercury concentrations in three of the ten fish caught in the Middle Fork American River near Otter Creek exceeded 0.08 mg/kg fish. Only rainbow trout were caught at this location. The exceedances occurred in the three of the four largest fish caught at this location. The greatest concentration measured in fish from the Middle Fork American River was 0.130 mg/kg fish.

6.4 QUALITY ASSURANCE/ QUALITY CONTROL PROCEDURES

A detailed summary of the QA/QC review of these reports can be found in Appendix D, Tables D-1 through D-4. A summary of potential issues identified in the QA/QC reports from each laboratory and sampling event is also provided in Appendix D.

The QA/QC review from the Test America (TA) and Brooks Rand (BR) laboratories indicated that most sample results (spring and fall sampling event, voluntary enhanced sampling below Project reservoirs, and fish tissue sampling) were acceptable, with only four sample results considered estimates. The results that were considered estimates include the spring sample at FM-3 (S) for TOC, and for three of the additional samples below French Meadows Dam (FM-A, FM-B, and FM-C) for manganese.

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TABLES

Table AQ 11-1. Water Quality Monitoring and Sampling Station Locations for 2007 Sampling Program.

Sample ID	Location Name	GPS Coordinates		Spring Sampling Program May 14-31	Weekly Sampling						Fall Sampling Program Sept. 24-Oct. 3
		UTM10_ NAD 83 X	UTM10_ NAD 83 Y		Aug 6	Aug. 13	Aug. 20	Aug. 27	Sept. 3	Sept. 10	
Duncan Creek											
DC-1 RM8.9	Duncan Creek above diversion	718058	4334904	X							X
DC-2 RM8.8	Duncan Creek below diversion	717492	4334534	X							X
DC-3 RM0.2	Duncan Creek above Middle Fork American River confluence	712310	4324261	X							
Middle Fork American River											
MFAR-1 RM52.8	Middle Fork American River above French Meadows Reservoir	724030	4334663	X							X
FM-1 (S)	French Meadows Reservoir surface (lower)	718930	4332295	X							X
FM-1	French Meadows Reservoir sub-surface (lower)	718930	4332295	X							X
FM-2 (S)	French Meadows Reservoir surface (middle)	720708	4332155	X							X
FM-2	French Meadows Reservoir sub-surface (middle)	720708	4332155	X							X
FM-3 (S)	French Meadows Reservoir surface (upper)	722241	4332680	X							X
FM-3	French Meadows Reservoir sub-surface (upper)	722241	4332680	X							X
MFAR-2 RM 46.6	Middle Fork American River below French Meadows Dam at gaging station	717789	4331977	X							X
MFAR-3 RM39.9	Middle Fork American River above Duncan Creek confluence	712707	4324155	X							
MFAR-4 RM39.5	Middle Fork American River below Duncan Creek confluence	712202	4323824	X							
MFAR-5 RM36.3	Middle Fork American River above Interbay Reservoir	708507	4322669	X							X
IR-1 RM35.7	In Middle Fork Interbay	717789	4331977	X							X
MFAR-6 RM35.5	Middle Fork American River below Middle Fork Interbay	707362	4322470	X							X
MFAR-7 RM26.1	Middle Fork American River above Ralston Afterbay	696379	4320205	X							X
Ralston Afterbay Downstream											
RA-1(S)	Ralston Afterbay surface	695348	4319604	X							X
RA-1	Ralston Afterbay sub-surface	695348	4319604	X							X
MFAR-8 RM24.7	Middle Fork American River below dam	694987	4319551	X							X
MFAR-9 RM24.3	Middle Fork American River below Oxbow Powerhouse tailrace	695104	4319974	X							X

Table AQ 11-1. Water Quality Monitoring and Sampling Station Locations for 2007 Sampling Program (continued).

Sample ID	Location Name	GPS Coordinates		Spring Sampling Program May 14-31	Weekly Sampling						Fall Sampling Program Sept. 24-Oct. 3
		UTM10_ NAD 83 X	UTM10_ NAD 83 Y		Aug 6	Aug. 13	Aug. 20	Aug. 27	Sept. 3	Sept. 10	
MFAR-10 RM9.1	Middle Fork American River below the Drivers Flat Road Rafting Take-Out	679156	4314631	X							X
MFAR-11 RM0.1	Middle Fork American River above North Fork American River	670249	4309058	X							X
NFAR-1 RM20.6	North Fork American River below Middle Fork American River	669795	4308943	X							X
Rubicon River											
RR-1 RM35.9	Rubicon River above Reservoir	729518	4328802	X							X
HH-1 (S)	Hell Hole Reservoir surface (lower)	724117	4326670	X							X
HH-1	Hell Hole Reservoir sub-surface (lower)	724117	4326670	X							X
HH-2 (S)	Hell Hole Reservoir surface (middle)	724599	4328282	X							X
HH-2	Hell Hole Reservoir sub-surface (middle)	724599	4328282	X							X
HH-3 (S)	Hell Hole Reservoir surface (upper)	726090	4329264	X							X
HH-3	Hell Hole Reservoir sub-surface (upper)	726090	4329264	X							X
RR-2 RM30.2	Rubicon River below dam at gaging station	724209	4326071	X							X
RR-3 RM 22.8	Rubicon River above South Fork Rubicon River confluence	719372	4316701	X							X
SFRR-1 RM0.2	South Fork Rubicon River above Rubicon River confluence	719482	4316246	X							X
RR-4 RM22.5	Rubicon River below South Fork Rubicon River confluence	719153	4316364	X							X
RR-5 RM3.8	Rubicon River above Long Canyon Creek confluence	700507	4318147	X							X
RR-6 RM3.5	Rubicon River below Long Canyon Creek confluence	700162	4318171	X							X
RR-7 RM0.7	Rubicon River above Ralston Afterbay	697119	4319216	X							X
Long Canyon Creek											
NFLC-1 RM3.2	North Fork Long Canyon Creek above diversion	717980	4325629	X							X
NFLC-2 RM2.9	North Fork Long Canyon Creek below diversion	717848	4325174	X							X
NFLC-3 RM0.3	North Fork Long Canyon Creek above Long Canyon Creek confluence	715004	4322534	X							X
SFLC-1 RM3.4	South Fork Long Canyon Creek above diversion	719042	4325646	X							X
SFLC-2 RM3.1	South Fork Long Canyon Creek below diversion	718669	4325275	X							X
SFLC-3 RM0.2	South Fork Long Canyon Creek above Long Canyon Creek confluence	715314	4322198	X							X

Table AQ 11-1. Water Quality Monitoring and Sampling Station Locations for 2007 Sampling Program (continued).

Sample ID	Location Name	GPS Coordinates		Spring Sampling Program May 14-31	Weekly Sampling						Fall Sampling Program Sept. 24-Oct. 3
		UTM10_ NAD 83 X	UTM10_ NAD 83 Y		Aug 6	Aug. 13	Aug. 20	Aug. 27	Sept. 3	Sept. 10	
LCC-1 RM11.3	Long Canyon Creek below North Fork and South Fork Long Canyon creeks confluence	714962	4321986	X							X
LCC-2 RM0.3	Long Canyon Creek above Rubicon River confluence	700544	4318487	X							X
Fecal Coliform											
FC-1	Middle Fork American River below Ahart Campground	724066	4336067		X	X	X	X	X		
FC-2	Middle Fork American River below Gates Group Campground	723679	4335535		X	X	X	X	X		
FC-3	Middle Fork American River below Coyote and Lewis Campground	723578	4334312		X	X	X	X	X		
FC-4	French Meadows Reservoir near McGuire Picnic Area	722892	4333328		X	X	X	X	X		
FC-5	French Meadows Reservoir near McGuire Boat Ramp	722565	4333376		X	X	X	X	X		
FC-6	French Meadows Reservoir near French Meadows Campground	722654	4332703		X	X	X	X	X		
FC-7	French Meadows Reservoir near French Meadows Boat Ramp	722249	4332433		X	X	X	X	X		
FC-8	French Meadows Reservoir near Poppy Campground	721628	4333151		X	X	X	X	X		
FC-9	Hell Hole Reservoir near Upper Hell Hole Reservoir Campground	728501	4329059			X	X	X	X	X	
FC-10	Hell Hole Reservoir near Hell Hole Boat Ramp	723737	4326842		X	X	X	X	X		
FC-11	South Fork Long Canyon Creek above Big Meadows Campground	722744	4328540			X	X	X	X	X	
FC-12	South Fork Long Canyon Creek below Big Meadows Campground	722119	4328056		X	X	X	X	X		
FC-13	South Fork Long Canyon Creek above Middle Meadows Campground	719274	4325849		X	X	X	X	X		
FC-14	South Fork Long Canyon Creek below Middle Meadows Campground	718907	4325560		X	X	X	X	X		
FC-15	Ralston Afterbay near Ralston Picnic Area	696326	4319720		X	X	X	X	X		
FC-16	Middle Fork American River below Oxbow Powerhouse (Horseshoe Bar Area)	695159	4320291		X	X	X	X	X		
FC-17	Middle Fork American River below the Drivers Flat Road Camping and Rafting Take-out	679156	4314631		X	X	X	X	X		

Table AQ 11-2. Summary of Water Quality Analytical Tests, Including Laboratory Methods and Detection Limits, and Chemical Water Quality Objectives.

Analyte	Units ¹	Analysis Method ²	Method Detection Limit (MDL) ³	Practical Quantitation Limit (PQL) ⁴	State and Federal Criteria			Sample Container	Hold Time	Preservative/Comment
					Basin Plan ⁵	CA Toxics Rule (CTR) ⁶	National Toxics Rule (NTR) ⁷			
In-Situ Measurements										
Oxygen, dissolved (DO)	mg/L	Water Quality Meter	Not Applicable	Not Applicable	7.0 ⁸	NS	NS ⁹	Not Applicable	Not Applicable	None
Secchi Depth	meter	Secchi Disc	Not Applicable	Not Applicable	NS	NS	NS	Not Applicable	Not Applicable	None
pH	unitless	Water Quality Meter	Not Applicable	Not Applicable	6.5 – 8.5 ¹⁰	NS	6.5 – 9.0 ¹¹	Not Applicable	Not Applicable	None
Water Temperature	Celsius	Water Quality Meter	Not Applicable	Not Applicable	NS	NS	NS	Not Applicable	Not Applicable	None
Specific Conductance	uS/cm at 25 °C	Water Quality Meter	Not Applicable	Not Applicable	NS	NS	NS	Not Applicable	Not Applicable	None
General Parameters										
Calcium	mg/L	EPA-200.7	Not Applicable	0.50	NS	NS	NS	1L plastic	180 days	Refrigerate
Chloride	mg/L	EPA-300.0	Not Applicable	1.0	250 ¹²	NS	230/860 ¹³	1L plastic	28 days	Refrigerate
Hardness (as CaCO ₃)	mg/L	SM2340B	Not Applicable	1.0	NS	NS	NS	1L plastic	180 days	HNO ₃ , refrigerate
Magnesium	ug/L	EPA-200.7	Not Applicable	100	NS	NS	NS	1L plastic	180 days	HNO ₃ , refrigerate
Nitrate/Nitrite (NO ₃)	mg/L	EPA-300.0	Not Applicable	0.20	1	NS	NS	1L plastic	28 days	Refrigerate
Ammonia as N	mg/L	EPA-350.3	Not Applicable	0.1	1.5 ¹⁴	NS	(15)	1L plastic	28 days	H ₂ SO ₄ ,Refrigerate
Total Kjeldahl Nitrogen (TKN)	mg/L	EPA-351.2	Not Applicable	0.100	NS	NS	NS	1L plastic	28 days	H ₂ SO ₄ ,Refrigerate
Total Phosphorus	mg/L	EPA-365.3	Not Applicable	0.1	NS	NS	NS	1L plastic	28 days	H ₂ SO ₄ ,Refrigerate
Ortho-phosphate	mg/L	SM4500P-E	Not Applicable	0.010	NS	NS	NS	1L plastic	48 hours	Refrigerate
Potassium	mg/L	EPA-200.7	Not Applicable	2.0	NS	NS	NS	1L plastic	180 days	HNO ₃ , refrigerate
Sodium	mg/L	EPA-200.7	Not Applicable	0.50	NS	NS	NS	1L plastic	180 days	HNO ₃ , refrigerate
Sulfate (SO ₄)	mg/L	EPA-300.0	Not Applicable	0.50	250 ¹²	NS	NS	1L plastic	28 days	Refrigerate
Total Dissolved Solids	mg/L	SM2540C	Not Applicable	10	500 ¹²	NS	NS	1L plastic	7 days	Refrigerate
Total Suspended Solids	mg/L	SM2540D	Not Applicable	10	NS	NS	NS	1L plastic	7 days	Refrigerate
Turbidity	NTU	EPA-180.1	Not Applicable	0.10	(16)	NS	NS	1L plastic	48 hours	Refrigerate
Organic Carbon, Total (TOC)	mg/L	SM5310B	Not Applicable	1.00	NS	NS	NS	250 mL amber glass	28 days	HCL, refrigerate
Total Alkalinity (as CaCO ₃)	mg/L	SM2320B	Not Applicable	5.0	NS	NS	>20 ¹⁷	1L plastic	14 days	Refrigerate
Metals-Dissolved										
Arsenic	ug/L	EPA-1368	0.06	0.20	10	150/340 ¹³	150/340 ¹³	250 mL plastic	180 days	Field filtered, refrigerate
Cadmium	ug/L	EPA-1368	0.004	0.01	5	Hardness Dependent ^{13, 18}	Hardness Dependent ^{13, 18}	250 mL plastic	180 days	Field filtered, refrigerate
Copper	mg/L	EPA-1368	0.00004	0.0002	1 ¹²	1.3 ²⁰ , Hardness Dependent ^{13, 18}	1.3 ²⁰ , Hardness Dependent ^{13, 18}	250 mL plastic	180 days	Field filtered, refrigerate
Iron	mg/L	EPA-1368	0.0014	0.005	0.3 ¹²	NS	1 ¹⁹	250 mL plastic	180 days	Field filtered, refrigerate
Lead	ug/L	EPA-1368	0.01	0.05	15	Hardness Dependent ^{13, 18}	Hardness Dependent ^{13, 18}	250 mL plastic	180 days	Field filtered, refrigerate
Manganese	ug/L	EPA-1368	0.01	0.05	50 ¹²	NS	NS	250 mL plastic	180 days	Field filtered, refrigerate
Nickel	ug/L	EPA-1368	0.04	0.20	100	610 ²⁰ , 4,600 ²¹ , Hardness Dependent ^{13, 18}	610 ²⁰ , 4,600 ²¹ , Hardness Dependent ^{13, 18}	250 mL plastic	180 days	Field filtered, refrigerate
Chromium-Total	ug/L	EPA-1368	0.03	0.15	50	NS	NS	250 mL plastic	180 days	Field filtered, refrigerate
Metals-Total										
Mercury	ug/L	EPA-1361e	0.00015	0.0004	NS	0.05	0.77/1.4 ¹³	250 mL plastic	180 days	Refrigerate
Methyl mercury	mg/Kg fish	EPA-1630 mod./MSPL-102a	0.001-0.01	0.003-0.029	NS	NS	0.3 ²²	Teflon sheet and ziplock bag	Not Applicable	Freeze

Quality Analytical Tests, Including Laboratory Methods and Detection Limits, and Chemical Water Quality Objectives (continued).

Method	Method Detection Limit (MDL) ³	Practical Quantitation Limit (PQL) ⁴	State and Federal Criteria			Sample Container	Hold Time	Preservative/Comment
			Basin Plan ⁵	CA Toxics Rule (CTR) ⁶	National Toxics Rule (NTR) ⁷			
1	Not Applicable	0.50	5 ¹²	NS	NS	40mL VOA	14 days	HCL, refrigerate
2	Not Applicable	50	NS	NS	(23)	40mL VOA	14 days	HCL, refrigerate
3	Not Applicable	4.8	(24)	NS	(25)	1L amber glass	48 hours	HCL, refrigerate
4	Not Applicable	2	NS	NS	NS	NS	24 hours	Refrigerate
5	Not Applicable	2-1600	200	NS	NS	100 mL plastic	24 hours	Refrigerate

not available, laboratory supplied units were used. (Note: µg/L=ppb and mg/L=ppm)

The most recent methods available were used for the water quality analysis.

can be reported with a 99% confidence that the analyte concentration is greater than zero." (40 CFR Part 136)

reliably measured within specified limits of precision and accuracy during routine laboratory operating conditions." (50 FR 46906)

ver Basins rely on California primary and secondary Maximum Concentration Level objectives as criteria for water quality to be used as a municipal and domestic supply for human consumption.

on USEPA standards developed under the Clean Water Act for human consumption of water and aquatic organisms with an adult risk for carcinogens estimated to be one in one million as contained in the
ber 1, 1996.

SEPA standards developed under the Clean Water Act for human consumption of water and aquatic organisms with an adult risk for carcinogens estimated to be one in one million as contained in the IRIS

d to all states not complying with the Clean Water Act section 303(c)(2)(B).

mean is recommended to achieve the required intergravel dissolved oxygen concentrations.

than 8.5. Changes in normal ambient pH should not exceed 0.5.

values between the first and second numbers shown.

on Levels for California drinking water quality objectives that do not necessarily indicate a toxic amount of contaminate. Rather these standards dictate water quality objectives designed to preserve taste,

tration (4-day average)/maximum concentration (1-hour average).

quality factors shall not exceed the following limits: where natural turbidity is between 0 and 5 NTU's, increases shall not exceed 1 NTU. Where natural turbidity is between 5 and 50 NTU's, increases

een 50 and 100 NTU's, increases shall not exceed 10 NTU's. Finally, where natural turbidity is greater than 100 NTU's, increases shall not exceed 10%.

cept where natural concentrations are less (USEPA's 1976 'Red Book'). The 'Red Book' also recommends that natural alkalinity not be reduced by more than 25%.

a function of hardness and decreases as hardness decreases. The actual criteria are calculated based on the hardness (as CaCO₃) of the sample water.

ncentration (4-day average).

g Water Sources (consumption of water an aquatic organisms).

quatic organism consumption only).

c) for methyl mercury and was published by the USEPA in a document titled Water Quality Criterion for the Protection of Human Health: Methyl mercury-Final (EPA-823-R-01-001, January 2001).

artially updated in 1997.

: taste and odor threshold and USEPA SNARL = 100 ug/L. TPH-gasoline: taste and odor threshold and proposed USEPA SNARL = 5 mg/L.

materials in concentrations that cause nuisance, result in a visible film or coating on the surface of the water or on objects in the water, or otherwise adversely affect beneficial uses.

rease, particularly from the tastes and odors that emanate from petroleum products (USEPA's 1986 'Gold Book').

00 mL of water.

0 mL of water.

Table AQ 11-3. List of Voluntary Enhanced Water Quality Sampling Locations.

Hell Hole Reservoir

Sample ID	Sample Location Description	GPS Coordinates	
		UTM10_ NAD 83X	UTM10_ NAD 83Y
RR-2A	Rubicon River below Hell Hole Reservoir outlet pipe	724275	4326213
RR-EC	Leakage channel below Hell Hole Reservoir	724237	4326112
RR-BEC	Rubicon River below Hell Hole Reservoir and leakage channel	724232	4326108

French Meadows Reservoir

Sample ID	Sample Location Description	GPS Coordinates	
		UTM10_ NAD 83X	UTM10_ NAD 83Y
FM-A	Leakage channel A below French Meadows Reservoir	718622	4332105
FM-B	Leakage channel B below French Meadows Reservoir	718569	4332212
FM-C	Leakage channel C below French Meadows Reservoir	718569	4332226
FM-E*	Middle Fork American River below French Meadows Reservoir outlet pipe	718551	4332220
	Middle Fork American River below French Meadows Reservoir and spillway channel	718304	4332195

*Sampling IDs are listed in upstream to downstream order

Table AQ 11-4. The Sacramento River Basin and San Joaquin River Basin Water Quality Control - Definition of Beneficial Uses.

Beneficial Use	Definition
Municipal and Domestic Supply (MUN)	Uses of water for community, military, or individual water supply systems including, but not limited to, drinking water supply.
Agricultural Supply (AGR)	Uses of water for farming, horticulture, or ranching including, but not limited to, irrigation (including leaching of salts), stock watering, or support of vegetation for range grazing.
Hydropower Generation (POW)	Uses of water for hydropower generation.
Water Contact Recreation (REC-1)	Uses of water for recreational activities involving body contact with water, where ingestion of water is reasonably possible. These uses include, but are not limited to, swimming, wading, water-skiing, skin and scuba diving, surfing, whitewater activities, fishing, or use of natural hot springs.
Non-contact Water Recreation (REC-2)	Uses of water for recreational activities involving proximity to water, but where there is generally no body contact with water, nor any likelihood of ingestion of water. These uses include, but are not limited to, picnicking, sunbathing, hiking, beachcombing, camping, boating, tidepool and marine life study, hunting, sightseeing, or aesthetic enjoyment in conjunction with the above activities.
Cold Freshwater Habitat (COLD)	Uses of water that support cold water ecosystems including, but not limited to, preservation or enhancement of aquatic habitats, vegetation, fish, or wildlife, including invertebrates.
Spawning, Reproduction and/or Early Development (SPWN)	Uses of water that support high quality aquatic habitats suitable for reproduction and early development of fish.
Wildlife Habitat (WILD)	Uses of water that support terrestrial or wetland ecosystems including, but not limited to, preservation and enhancement of terrestrial habitats or wetlands, vegetation, wildlife (e.g., mammals, birds, reptiles, amphibians, invertebrates), or wildlife water and food sources.

Source: Table II of *The Sacramento River Basin and San Joaquin River Basin Water Quality Control Plan (Basin Plan)* for the California Regional Water Quality Control Board –Control Valley Region Fourth Edition revised February 2007.

Table AQ 11-5. Summary of *In-Situ* Stream Measurements Collected During the Spring 2007 Sampling Event.

Sample ID	Location Name	Date	Temperature (°C)	Dissolved Oxygen (mg/L)	Specific Conductance (µS/cm at 25 °C)	pH	Sample Water Depth ¹ (m)	Secchi Depth ² (m)
Duncan Creek								
DC-1 RM8.9	Duncan Creek above diversion	5/22/2007	7.24	8.9	57	7.6	0	
DC-2 RM8.8	Duncan Creek below diversion	5/22/2007	7.97	8.8	57	7.9	0	
DC-3 RM0.2	Duncan Creek above Middle Fork American River confluence	5/17/2007	11.16	6.3	67	8.2	0	
Middle Fork American River								
MFAR-1 RM51.6	Middle Fork American River above French Meadows Reservoir	5/22/2007	8.23	9.0	53	7.7	0	
FM-1 (S)	French Meadows Reservoir surface (lower)	5/30/2007	16.32	7.9	25	6.9	0	6.5
FM-1	French Meadows Reservoir sub-surface (lower)	5/30/2007	7.17	8.2	23	6.5	30	
FM-2 (S)	French Meadows Reservoir surface (middle)	5/31/2007	16.12	7.7	25	6.6	0	7.5
FM-2	French Meadows Reservoir sub-surface (middle)	5/31/2007	8.25	8.4	24	6.5	20	
FM-3 (S)	French Meadows Reservoir surface (upper)	5/31/2007	16.45	7.9	25	6.6	0	7
FM-3	French Meadows Reservoir sub-surface (upper)	5/31/2007	9.89	8.8	23	6.6	15	
MFAR-2 RM 46.6	Middle Fork American River below French Meadows Dam at gaging station	5/22/2007	10.60	9.0	54	7.4	0	
MFAR-3 RM39.9	Middle Fork American River above Duncan Creek confluence	5/17/2007	13.17	6.3	66	7.7	0	

Table AQ 11-5. Summary of *In-Situ* Stream Measurements Collected During the Spring 2007 Sampling Event (continued).

Sample ID	Location Name	Date	Temperature (°C)	Dissolved Oxygen (mg/L)	Specific Conductance (µS/cm at 25 °C)	pH	Sample Water Depth ¹ (m)	Secchi Depth ² (m)
MFAR-4 RM39.5	Middle Fork American River below Duncan Creek confluence	5/17/2007	12.44	6.2	67	7.8	0	
MFAR-5 RM36.3	Middle Fork American River above Middle Fork Interbay	5/16/2007	13.25	8.9	68	8.4	0	
IR-1 RM35.7	In Middle Fork Interbay	5/16/2007	13.77	8.8	66	7.2	0	
MFAR-6 RM35.5	Middle Fork American River below Middle Fork Interbay	5/16/2007	10.02	9.3	60	7.7	0	
MFAR-7 RM26.1	Middle Fork American River above Ralston Afterbay	5/22/2007	15.44	8.5	82	7.4	0	
Ralston Afterbay Downstream								
RA-1(S)	Ralston Afterbay surface	5/29/2007	19.15	10.3	53	6.6	0	7
RA-1	Ralston Afterbay sub-surface	5/29/2007	12.03	11.4	36	6.5	6	
MFAR-8 RM24.7	Middle Fork American River below dam	5/21/2007	18.76	8.0	63	7.0	0	
MFAR-9 RM24.3	Middle Fork American River below Oxbow Powerhouse tailrace	5/21/2007	15.32	8.9	66	7.3	0	
MFAR-10 RM9.1	Middle Fork American River below the Drivers Flat Road Rafting Take-Out	5/14/2007	16.53	9.7	64	6.8	0	
MFAR-11 RM0.1	Middle Fork American River above North Fork American River	5/16/2007	19.73	8.7	67	7.3	0	
NFAR-1 RM20.6	North Fork American River below Middle Fork American River	5/16/2007	18.51	8.7	72	7.4	0	

Table AQ 11-5. Summary of *In-Situ* Stream Measurements Collected During the Spring 2007 Sampling Event (continued).

Sample ID	Location Name	Date	Temperature (°C)	Dissolved Oxygen (mg/L)	Specific Conductance (µS/cm at 25 °C)	pH	Sample Water Depth ¹ (m)	Secchi Depth ² (m)
Rubicon River								
RR-1 RM35.9	Rubicon River above Reservoir	5/24/2007	9.60	10.3	52	7.8	0	
HH-1 (S)	Hell Hole Reservoir surface (lower)	5/30/2007	14.52	8.5	28	7.0	0	9
HH-1	Hell Hole Reservoir sub-surface (lower)	5/30/2007	6.65	8.7	27	6.7	30	
HH-2 (S)	Hell Hole Reservoir surface (middle)	5/30/2007	14.72	8.1	28	6.9	0	11
HH-2	Hell Hole Reservoir sub-surface (middle)	5/30/2007	7.99	8.8	27	6.7	30	
HH-3 (S)	Hell Hole Reservoir surface (upper)	5/30/2007	12.72	8.8	29	7.1	0	8
HH-3	Hell Hole Reservoir sub-surface (upper)	5/30/2007	7.79	9.0	26	6.8	30	
RR-2 RM30.2	Rubicon River below dam at gaging station	5/22/2007	7.13	9.8	54	7.1	0	
RR-3 RM 22.8	Rubicon River above South Fork Rubicon River confluence	5/23/2007	12.19	8.8	75	7.4	0	
SFRR-1 RM0.2	South Fork Rubicon River above Rubicon River confluence	5/23/2007	11.83	8.8	51	7.5	0	
RR-4 RM22.5	Rubicon River below South Fork Rubicon River confluence	5/23/2007	12.78	8.9	69	7.5	0	
RR-5 RM3.8	Rubicon River above Long Canyon Creek confluence	5/21/2007	16.30	8.4	75	6.9	0	

Table AQ 11-5. Summary of *In-Situ* Stream Measurements Collected During the Spring 2007 Sampling Event (continued).

Sample ID	Location Name	Date	Temperature (°C)	Dissolved Oxygen (mg/L)	Specific Conductance (µS/cm at 25 °C)	pH	Sample Water Depth ¹ (m)	Secchi Depth ² (m)
RR-6 RM3.5	Rubicon River below Long Canyon Creek confluence	5/21/2007	16.26	8.4	72	7.3	0	
RR-7 RM0.7	Rubicon River above Ralston Afterbay	5/21/2007	19.61	8.6	71	7.3	0	
Long Canyon Creek								
NFLC-1 RM3.2	North Fork Long Canyon Creek above diversion	5/15/2007	12.86	8.8	55	7.5	0	
NFLC-2 RM2.9	North Fork Long Canyon Creek below diversion	5/15/2007	13.80	8.7	54	7.7	0	
NFLC-3 RM0.3	North Fork Long Canyon Creek above Long Canyon Creek confluence	5/15/2007	10.81	9.2	63	7.3	0	
SFLC-1 RM3.4	South Fork Long Canyon Creek above diversion	5/15/2007	11.31	8.8	59	6.5	0	
SFLC-2 RM3.1	South Fork Long Canyon Creek below diversion	5/15/2007	11.68	9.1	58	6.6	0	
SFLC-3 RM0.2	South Fork Long Canyon Creek above Long Canyon Creek confluence	5/15/2007	9.51	9.3	60	7.2	0	
LCC-1 RM11.3	Long Canyon Creek below North Fork and South Fork Long Canyon creeks confluence	5/15/2007	9.61	9.3	60	7.3	0	
LCC-2 RM0.3	Long Canyon Creek above Rubicon River confluence	5/21/2007	15.14	8.8	69	7.5	0	

1: Water sample was collected just below the water surface unless otherwise noted.

2: Secchi depth measurements were only collected in the reservoirs.

3: Instrument malfunction, no in-situ measurements available.

Table AQ 11-6. Summary of *In-Situ* Stream Measurements Collected During the Fall 2007 Sampling Event.

Sample ID	Location Name	Date	Temperature (°C)	Dissolved Oxygen (mg/L)	Specific Conductance (µS/cm at 25 °C)	pH	Sample Water Depth ¹ (m)	Secchi Depth ²
Duncan Creek								
DC-1 RM8.9	Duncan Creek above diversion	9/25/2007	12.25	7.2	67	7.8	0	
DC-2 RM8.8	Duncan Creek below diversion	9/25/2007	11.61	7.0	65	7.1	0	
DC-3 RM0.2	Duncan Creek above Middle Fork American River confluence	NS	NS	NS	NS	NS	NS	
Middle Fork American River								
MFAR-1 RM51.6	Middle Fork American River above French Meadows Reservoir	10/3/2007	8.79	13.6	33	7.5	0	
FM-1 (S)	French Meadows Reservoir surface (lower)	10/3/2007	15.07	8.3	34	7.8	0	9.5
FM-1	French Meadows Reservoir sub-surface (lower)	10/3/2007	10.07	7.3	33	6.7	22.5	
FM-2 (S)	French Meadows Reservoir surface (middle)	10/3/2007	15.23	8.3	33	7.9	0	Too windy
FM-2	French Meadows Reservoir sub-surface (middle)	10/3/2007	10.23	7.7	30	6.6	22.5	
FM-3 (S)	French Meadows Reservoir surface (upper)	10/3/2007	15.36	8.6	33	7.2	0	Too windy
FM-3	French Meadows Reservoir sub-surface (upper)	10/3/2007	11.36	7.7	33	6.5	22.5	
MFAR-2 RM 46.6	Middle Fork American River below French Meadows Dam at gaging station	10/3/2007	8.93	11.7	16	7.5	0	
MFAR-3 RM39.9	Middle Fork American River above Duncan Creek confluence	NS	NS	NS	NS	NS	NS	

Table AQ 11-6. Summary of *In-Situ* Stream Measurements Collected During the Fall 2007 Sampling Event (continued).

Sample ID	Location Name	Date	Temperature (°C)	Dissolved Oxygen (mg/L)	Specific Conductance (µS/cm at 25 °C)	pH	Sample Water Depth ¹ (m)	Secchi Depth ²
MFAR-4 RM39.5	Middle Fork American River below Duncan Creek confluence	NS	NS	NS	NS	NS	NA	
MFAR-5 RM36.3	Middle Fork American River above Middle Fork Interbay	9/24/2007	11.75	7.8	62	8.0	0	
IR-1 RM35.7	In Middle Fork Interbay	9/24/2007	12.14	7.8	66	8.0	0	
MFAR-6 RM35.5	Middle Fork American River below Middle Fork Interbay	9/24/2007	12.41	7.7	39	7.8	0	
MFAR-7 RM26.1	Middle Fork American River above Ralston Afterbay	9/26/2007	13.52	10.5	54	7.4	0	
Ralston Afterbay Downstream								
RA-1(S)	Ralston Afterbay surface	9/26/2007	13.24	10.9	41	7.0	0	7
RA-1	Ralston Afterbay sub-surface	9/26/2007	12.38	11.3	36	6.8	5	
MFAR-8 RM24.7	Middle Fork American River below dam	9/26/2007	17.58	9.9	42	6.9	0	
MFAR-9 RM24.3	Middle Fork American River below Oxbow Powerhouse tailrace	9/26/2007	13.08	11.3	39	7.1	0	
MFAR-10 RM9.1	Middle Fork American River below the Drivers Flat Road Rafting Take-Out	9/24/2007	13.90	10.2	46	7.7	0	
MFAR-11 RM0.1	Middle Fork American River above North Fork American River	9/25/2007	13.62	10.5	49	7.7	0	
NFAR-1 RM20.6	North Fork American River below Middle Fork American River	9/25/2007	14.45	10.0	63	7.7	0	

Table AQ 11-6. Summary of *In-Situ* Stream Measurements Collected During the Fall 2007 Sampling Event (continued).

Sample ID	Location Name	Date	Temperature (°C)	Dissolved Oxygen (mg/L)	Specific Conductance (µS/cm at 25 °C)	pH	Sample Water Depth ¹ (m)	Secchi Depth ²
Rubicon River								
RR-1 RM35.9	Rubicon River above Reservoir	10/2/2007	11.74	7.8	107	7.1	0	
HH-1 (S)	Hell Hole Reservoir surface (lower)	10/1/2007	16.66	7.2	36	7.9	0	10
HH-1	Hell Hole Reservoir sub-surface (lower)	10/1/2007	15.81	6.3	31	6.8	23	
HH-2 (S)	Hell Hole Reservoir surface (middle)	10/1/2007	16.10	6.4	33	6.7	0	10
HH-2	Hell Hole Reservoir sub-surface (middle)	10/1/2007	15.82	6.3	32	7.0	27	
HH-3 (S)	Hell Hole Reservoir surface (upper)	10/2/2007	15.80	6.3	44	7.8	0	9.4
HH-3	Hell Hole Reservoir sub-surface (upper)	10/2/2007	15.76	6.3	40	7.2	20	
RR-2 RM30.2	Rubicon River below dam at gaging station	10/3/2007	8.97	9.9	18	6.9	0	
RR-3 RM 22.8	Rubicon River above South Fork Rubicon River confluence	9/25/2007	11.34	7.6	54	7.1	0	
SFRR-1 RM0.2	South Fork Rubicon River above Rubicon River confluence	9/25/2007	11.56	7.7	25	8.4	0	
RR-4 RM22.5	Rubicon River below South Fork Rubicon River confluence	9/25/2007	11.64	7.3	30	7.0	0	
RR-5 RM3.8	Rubicon River above Long Canyon Creek confluence	9/27/2007	15.40	8.4	56	7.7	0	
RR-6 RM3.5	Rubicon River below Long Canyon Creek confluence	9/27/2007	15.27	8.3	59	7.3	0	
RR-7 RM0.7	Rubicon River above Ralston Afterbay	9/26/2007	17.86	9.7	62	7.2	0	

Table AQ 11-6. Summary of *In-Situ* Stream Measurements Collected During the Fall 2007 Sampling Event (continued).

Sample ID	Location Name	Date	Temperature (°C)	Dissolved Oxygen (mg/L)	Specific Conductance (µS/cm at 25 °C)	pH	Sample Water Depth ¹ (m)	Secchi Depth ²
Long Canyon Creek								
NFLC-1 RM3.2	North Fork Long Canyon Creek above diversion	10/2/2007	8.46	9.7	41	7.4	0	
NFLC-2 RM2.9	North Fork Long Canyon Creek below diversion	10/2/2007	10.52	9.0	42	7.4	0	
NFLC-3 RM0.3	North Fork Long Canyon Creek above Long Canyon Creek confluence	10/2/2007	8.46	9.8	29	7.3	0	
SFLC-1 RM3.4	South Fork Long Canyon Creek above diversion	10/2/2007	8.81	8.8	34	7.1	0	
SFLC-2 RM3.1	South Fork Long Canyon Creek below diversion	10/2/2007	8.85	9.6	34	7.4	0	
SFLC-3 RM0.2	South Fork Long Canyon Creek above Long Canyon Creek confluence	10/2/2007	7.52	9.7	29	7.0	0	
LCC-1 RM11.3	Long Canyon Creek below North Fork and South Fork Long Canyon creeks confluence	10/2/2007	8.17	7.6	29	7.5	0	
LCC-2 RM0.3	Long Canyon Creek above Rubicon River confluence	9/27/2007	14.30	8.6	92	7.4	0	

1: Water sample was collected just below the water surface unless otherwise noted.

2: Secchi depth measurements were only collected in the reservoirs.

NS: No sample was collected at this location during the fall sampling event due to dangerous access conditions.

Table AQ 11-7. Summary of Analytical Results for Water Quality Samples Collected during the Spring 2007 Sampling Event.

				Station	DC-1 RM8.9	DC-2 RM8.8	DC-3 RM0.2	MFAR-1 RM51.6	FM-1(S)	FM-1	FM-2(S)	FM-2	FM-3(S)	FM-3	MFAR-2 RM 46.6	MFAR-3 RM39.9	MFAR-4 RM39.5	MFAR-5 RM36.3	IR-1 RM35.7	MFAR-6 RM35.5	MFAR-7 RM26.1	RA-1(S)	RA-1	MFAR-8 RM24.7	MFAR-9 RM24.3	MFAR-10 RM9.1	MFAR-11 RM0.1	NFAR-1 RM20.6
				Date	5/22/2007	5/22/2007	5/1707	5/22/2007	5/31/2007	5/31/2007	5/31/2007	5/31/2007	5/31/2007	5/31/2007	5/22/2007	5/17/2007	5/17/2007	5/16/2007	5/16/2007	5/16/2007	5/22/2007	5/29/2007	5/29/2007	5/21/2007	5/21/2007	5/14/2007	5/16/2007	5/16/2007
				Time	9:45	10:40	11:00	11:40	9:30	8:40	10:00	10:40	13:15	12:15	12:30	12:30	12:00	9:25	10:10	8:50	8:00	12:30	10:40	14:00	13:30	15:50	15:10	14:30
General Parameters	Units	PQL	WQ Criteria																									
Calcium	mg/L	0.5	NS		2.7	2.8	4.8	2.3	2.1	2.3	2.2	2.2	2.2	2.2	2.6	4.5	4.7	5.3	4.9	3.5	7.4	5.7	4.3	4.8	4.8	4.7	5.1	6
Chloride	mg/L	1.0	250 ¹		ND	ND	1.1	ND	ND	ND	ND	ND	ND	ND	ND	1.3	1.2	1.2	1.1	1.1	1.2	1.7	1.2	1.5	1.8	1.5	1.6	1.5
Hardness (as CaCO ₃)	mg/L	1.0	NS		9.5	9.8	16	8.2	7.5	8.1	7.8	7.9	7.8	7.8	9	15	15	17	16	12	23	18	14	16	16	17	18	21
Magnesium	µg/L	100	NS		680	690	910	600	540	570	560	580	570	570	620	800	890	970	920	730	1200	1000	810	980	910	1200	1300	1500
Nitrate/Nitrite (NO ₃)	mg/L	0.20	1 ¹		ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Ammonia as N	mg/L	0.100	1.5		ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Total Kjeldahl Nitrogen (TKN)	mg/L	0.100	NS		4.2	8.4	0.56	3.1	1.4	2	1.1	2.5	78	5	7	0.56	0.56	3.9	1.1	0.56	2.8	1.4	1.7	0.56	0.56	0.84	0.56	0.56
Total Phosphorus	mg/L	0.100	NS		ND	0.49	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	0.13	ND	ND	ND	ND	ND	ND
Ortho-phosphate	mg/L	0.010	NS		ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Potassium	mg/L	0.20	NS		ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Sodium	mg/L	0.50	NS		1.3	1.3	1.5	1.2	1.2	1.2	1.2	1.2	1.2	1.2	1.3	1.9	1.8	1.8	1.8	1.5	2	2.3	1.9	1.9	2	1.8	1.7	1.8
Sulfate (SO ₄)	mg/L	0.50	250 ¹		0.56	0.58	0.98	ND	ND	ND	ND	ND	ND	ND	ND	0.73	0.88	0.74	0.75	0.72	2.9	1.4	0.76	1.5	1.3	1.7	1.8	2
Total Dissolved Solids	mg/L	10	500 ¹		32	24	30	30	40	44	40	44	38	40	28	50	38	46	34	24	44	48	26	36	50	38	60	38
Total Suspended Solids	mg/L	10	NS		ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Turbidity	NTU	0.10	(5)		ND	0.16	3.8	ND	1.1	1.1	1.1	1.2	0.78	0.6	0.44	1.2	0.13	0.86	2.2	0.44	0.12	0.41	1.2	0.38	0.15	0.27	0.44	0.53
Organic Carbon, Total (TOC)	mg/L	1.00	NS		ND	ND	ND	1.3	1	1.1	1.6	1.2	1.6	1.4	1.1	ND	ND	ND	ND	ND	1.4	1.3	1.9	ND	ND	ND	ND	ND
Total Alkalinity	mg/L	5.0	>20 ³		16	14	16	14	22	22	24	20	20	22	14	18	20	22	18	16	20	22	16	20	20	16	22	26
Metals-Dissolved																												
Arsenic	µg/L	0.20	10 ¹		0.060 ^U	0.060 ^U	0.060 ^U	0.090 ^B	0.130 ^B	0.120 ^B	0.130 ^B	0.110 ^B	0.110 ^B	0.120 ^B	0.130 ^B	0.120 ^B	0.090 ^B	0.100 ^B	0.090 ^B	0.170 ^B	0.230	0.220	0.200 ^B	0.170 ^B	0.170 ^B	0.220	0.240	0.450
Cadmium	µg/L	0.010	(6)		0.005 ^B	0.005 ^B	0.004 ^U	0.006 ^B	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	
Copper	mg/L	0.00020	(6)		0.00015 ^B	0.00016 ^B	0.000130 ^B	0.000160 ^B	0.000190 ^B	0.000220	0.000190 ^B	0.000180 ^B	0.000180 ^B	0.000180 ^B	0.000190 ^B	0.000140 ^B	0.000160 ^B	0.000180 ^B	0.000590	0.000240	0.000330	0.000340	0.000390	0.000310	0.000340	0.000410	0.00030	0.000430
Iron	mg/L	0.005	0.3 ¹		0.0014 ^U	0.019300	0.0028 ^B	0.005 ^B	0.0014 ^U	0.0022 ^B	0.0014 ^U	0.0014 ^U	0.00410 ^B	0.0014 ^U	0.135000	0.013100	0.008400	0.006600	0.005300	0.007400	0.00260 ^B	0.005400	0.008300	0.071600	0.022100	0.008200	0.007400	0.014600
Lead	µg/L	0.050	(6)		0.010 ^U	0.010 ^U	0.010 ^U	0.030 ^B	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	
Manganese	µg/L	0.05	50 ¹		*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*
Nickel	µg/L	0.20	(6)		0.180	0.170	0.160 ^B	0.080 ^B	0.040 ^U	0.040 ^U	0.040 ^U	0.040 ^U	0.040 ^U	0.040 ^U	0.060 ^B	0.070 ^B	0.110 ^B	0.100 ^B	0.120 ^B	0.090 ^B	0.210	0.090 ^B	0.090 ^B	0.150 ^B	0.130 ^B	0.230	0.250	0.380
Chromium-Total	µg/L	0.15	50 ¹		0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	
Metals-Total																												
Mercury	µg/L	0.0004	0.05 ²		0.000360 ^B	0.000270 ^B	0.0004 ^B	0.000430	0.000290 ^B	0.000860	0.000350 ^B	0.000420	0.000340 ^B	0.000610	0.000330 ^B	0.000350 ^B	0.000400 ^B	0.000530	0.000380 ^B	0.000560	0.000330 ^B	0.000340 ^B	0.000680	0.000370 ^B	0.000360 ^B	0.000850	0.000610	0.001480
Hydrocarbons																												
Methyl-tertiary-butyl Ether (MtBE)	µg/L	0.50	5 ¹																			ND	ND					
Total Petroleum Hydrocarbons (as gasoline and as diesel)	µg/L	50	NS																			ND	ND					
Oil and Grease	mg/L	4.8	NS																			ND	ND					
Bacteria																												
Total Coliform (3x5, 6 hr hold)	MPN/100 mL	2	NS		<2	<2	<2	4	<2	70	<2	<2	<2	23	<2	4	<2	<2	4	<2	23	4	6	2	13	30	2	7
Fecal Coliform (3x5)	MPN/100 mL	2-1600	200/100 ¹		<2	<2	<2	4	<2	70	<2	<2	<2	23	<2	4	<2	<2	4	<2	23	4	6	2	13	30	2	7

Table AQ 11-7. Summary of Analytical Results for Water Quality Samples Collected during the Spring 2007 Sampling Event (continued)

				Station	RR-1 RM35.9	HH-1(S)	HH-1	HH-2(S)	HH-2	HH-3(S)	HH-3	RR-2 RM30.2	RR-3 RM 22.8	SFRR-1 RM0.2	RR-4 RM22.5	RR-5 RM3.8	RR-6 RM3.5	RR-7 RM0.7	NFLC-1 RM3.2	NFLC-2 RM2.9	NFLC-3 RM0.3	SFLC-1 RM3.4	SFLC-2 RM3.1	SFLC-3 RM0.2	LCC-1 RM11.3	LCC-2 RM0.3
				Date	5/24/2007	5/22/2007	5/22/2007	5/22/2007	5/22/2007	5/22/2007	5/22/2007	5/22/2007	5/23/2007	5/23/2007	5/23/2007	5/23/2007	5/21/2007	5/21/2007	5/21/2007	5/15/2007	5/15/2007	5/15/2007	5/15/2007	5/15/2007	5/15/2007	5/21/2007
				Time	10:40	13:45	13:00	11:00	10:30	12:00	11:30	14:00	11:40	11:00	12:20	9:20	10:15	14:45	13:30	14:10	10:20	11:30	11:55	9:30	8:50	9:40
General Parameters				Units	PQL	WQ Criteria																				
Calcium	mg/L	0.5	NS	2.5	3.2	2.9	2.8	2.9		2.9	2.8	2.8	4.4	2.4	3.6	5.2	5	5.3	2.5	2.6	2.9	2.7	3.2	2.6	3	4.7
Chloride	mg/L	1.0	250 ¹	1.2	ND	ND	ND	ND		ND	ND	ND	5.3	ND	4.2	3.5	3	2.9	1	1.1	1.2	1	1	1.1	1	1.4
Hardness (as CaCO ₃)	mg/L	1.0	NS	8.3	11	9.6	9.3	9.6		9.6	9.3	9.3	14	8.2	12	17	16	17	9.2	9.6	11	10	12	9.7	11	17
Magnesium	µg/L	100	NS	ND	670	570	560	580		570	560	550	730	530	640	900	950	1000	730	750	830	810	970	780	880	1200
Nitrate/Nitrite (NO ₃)	mg/L	0.20	1 ¹	ND	ND	ND	ND	ND		ND	ND	ND	ND	ND	ND	ND	ND	ND	0.2	ND	ND	ND	ND	ND	ND	ND
Ammonia as N	mg/L	0.100	1.5	ND	ND	ND	ND	ND		ND	ND	ND	ND	ND	ND	ND	0.62	ND	ND	ND	ND	ND	ND	ND	ND	ND
Total Kjeldahl Nitrogen (TKN)	mg/L	0.100	NS	ND	ND	ND	0.56	2.2		1.1	0.84	0.56	ND	ND	ND	ND	0.84	0.56	0.56	0.56	0.56	0.56	0.56	0.56	0.56	0.56
Total Phosphorus	mg/L	0.100	NS	ND	ND	ND	ND	ND		ND	ND	ND	0.56	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Ortho-phosphate	mg/L	0.010	NS	ND	ND	ND	ND	ND		ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Potassium	mg/L	0.20	NS	ND	ND	ND	ND	ND		ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Sodium	mg/L	0.50	NS	ND	1.7	1.4	1.3	1.4		1.4	1.4	1.4	3.8	1.5	3	2.9	2.9	2.9	1.8	1.9	2.3	1.7	2.1	1.9	2.3	2.6
Sulfate (SO ₄)	mg/L	0.50	250 ¹	ND	0.59	0.62	0.66	0.62		0.69	0.61	0.77	0.74	ND	0.66	1.3	1.1	1.3	ND	ND	ND	ND	ND	ND	ND	0.67
Total Dissolved Solids	mg/L	10	500 ¹	40	38	20	20	20		20	16	28	50	34	90	62	60	48	22	50	48	48	40	44	36	86
Total Suspended Solids	mg/L	10	NS	ND	ND	ND	ND	ND		ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Turbidity	NTU	0.10	(5)	0.16	0.44	0.25	0.32	0.35		0.19	0.15	0.15	0.29	0.24	0.15	0.25	0.12	0.11	0.18	0.22	0.46	ND	ND	0.3	0.44	0.19
Organic Carbon, Total (TOC)	mg/L	1.00	NS	2.3	1.7	1.9	1.7	2		1.7	2.1	1.2	ND	1	ND	ND	ND	ND	1.1	ND	ND	ND	ND	ND	ND	ND
Total Alkalinity	mg/L	5.0	>20 ³	22	12	12	9.8	9.8		12	12	12	16	12	14	22	22	20	12	12	18	18	16	14	16	22
Metals-Dissolved																										
Arsenic	µg/L	0.20	10 ¹	0.330	0.220	0.200 ^B	0.190 ^B	0.210		0.200 ^B	0.210	0.210	0.190 ^B	0.060 ^U	0.170 ^B	0.160 ^B	0.140 ^B	0.160 ^B	0.060 ^U	0.070 ^B	0.150 ^B	0.080 ^B	0.090 ^B	0.140 ^B	0.140 ^B	0.160 ^B
Cadmium	µg/L	0.010	(6)	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U		0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	
Copper	mg/L	0.00020	(6)	0.000200 ^B	0.000270	0.000490	0.000270	0.000290		0.000250	0.000260	0.000310	0.000430	0.000130 ^B	0.000380	0.000360	0.000330	0.000350	0.000100 ^B	0.000090 ^B	0.000200 ^B	0.000100 ^B	0.000110 ^B	0.000130 ^B	0.000150 ^B	0.000200 ^B
Iron	mg/L	0.005	0.3 ¹	0.014700	0.001400 ^U	0.001400 ^U	0.001400 ^U	0.001400 ^U		0.001400 ^U	0.001400 ^U	0.001400 ^U	0.001400 ^U	0.001400 ^U	0.001400 ^U	0.001400 ^U	0.001400 ^U	0.001400 ^U	0.001400 ^U	0.001400 ^U	0.0091	0.001400 ^U	0.003100 ^B	0.001400 ^U	0.003600 ^B	0.001600 ^B
Lead	µg/L	0.050	(6)	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U		0.010 ^U	0.010 ^U	0.010 ^U	0.050 ^B	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	
Manganese	µg/L	0.05	50 ¹	*	*	*	*	*		*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*	*
Nickel	µg/L	0.20	(6)	0.090 ^B	0.100 ^B	0.100 ^B	0.100 ^B	0.100 ^B		0.090 ^B	0.090 ^B	0.090 ^B	0.100 ^B	0.100 ^B	0.090 ^B	0.130 ^B	0.120 ^B	0.140 ^B	0.040 ^U	0.040 ^U	0.050 ^B	0.040 ^U	0.040 ^U	0.040 ^U	0.040 ^U	0.100 ^B
Chromium-Total	µg/L	0.15	50 ¹	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U		0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	
Metals-Total																										
Mercury	µg/L	0.0004	0.05 ²	0.000480	0.000510	0.000650	0.000350 ^B	0.000680		0.000520	0.000740	0.000480	0.000370 ^B	0.000410	0.000320 ^B	0.000230 ^B	0.000240 ^B	0.000200 ^B	0.000610	0.000770	0.001010	0.000310 ^B	0.000430	0.000440	0.000750	0.000540
Hydrocarbons																										
Methyl-tertiary-butyl Ether (MTBE)	µg/L	0.50	5 ¹		ND	ND	ND	ND		ND	ND															
Total Petroleum Hydrocarbons (as gasoline and as diesel)	µg/L	50	NS		ND	ND	ND	ND		ND	ND															
Oil and Grease	mg/L	4.8	NS		ND	ND	ND	ND		ND	ND															
Bacteria																										
Total Coliform (3x5, 6 hr hold)	MPN/100 mL	2	NS	7	<2	<2	<2	<2		<2	<2	8	30	8	17	30	23	4	<2	<2	2	<2	4	2	2	17
Fecal Coliform (3x5)	MPN/100 mL	2-1600	200/100 ¹	7	<2	<2	<2	<2		<2	<2	8	30	8	17	30	23	4	<2	<2	2	<2	4	2	2	17

Note: Bold results do not meet the listed criteria within specified limits of precision and accuracy during routine laboratory operation conditions.

ND: Not Detected above the PQL

NS: No standard

*: Not sampled

U: Results are less than or equal to the method detection limit (MDL) and are considered 'non-detect'.

B: Results are above the MDL and less than or equal to the practical quantitation limit (PQL) and should be considered estimates.

1: Basin Plan criteria for the Sacramento and San Joaquin Rivers Basins.

2: California Toxics Rule Criteria (CTR)

3: National Toxics Rule Criteria (NTR)

4: pH, temperature and life cycle dependent. See Table 11-11 for criteria and results.

5:Increases in turbidity attributable to controllable water quality factors shall not exceed the following limits: where natural turbidity is between 0 and 5 NTU's, increases shall not exceed 1 NTU. Where natural turbidity is between 5 and 50 NTU's, increases shall not exceed 20%. Where natural turbidity is between 50 and 100 NTU's, increases shall not exceed 10 NTU's. Finally, where natural turbidity is greater than 100 NTU's, increases shall not exceed 10%.

6: Criteria is hardness dependent which is expressed as a function of hardness and decreases as hardness decreases. The actual criteria are calculated based on the hardness (as CaC₉) of the sample water. Refer to Table 11-12 for sample site criteria and results.

Table AQ 11-8. Calculated Ammonia Concentration Criteria for the Spring 2007 Sampling Event.

Sample ID	Location Name	Date	pH	Temperature	Ammonia Criteria Continuous Concentration with fish early life stages present (NTR) ¹	Ammonia Concentration
				(°C)	mg/L	mg/L
DC-1 RM8.9	Duncan Creek above diversion	5/22/2007	7.6	7.24	3.98	#N/A
DC-2 RM8.8	Duncan Creek below diversion	5/22/2007	7.9	7.97	2.99	#N/A
DC-3 RM0.2	Duncan Creek above Middle Fork American River confluence	5/17/2007	8.2	11.16	1.85	#N/A
MFAR-1 RM52.8	Middle Fork American River above French Meadows Reservoir	5/22/2007	7.7	8.23	3.74	#N/A
FM-1 (S)	French Meadows Reservoir surface (lower)	5/30/2007	6.9	16.32	5.43	#N/A
FM-1	French Meadows Reservoir sub-surface (lower)	5/30/2007	6.5	7.17	6.68	ND
FM-2 (S)	French Meadows Reservoir surface (middle)	5/31/2007	6.6	16.12	5.89	#N/A
FM-2	French Meadows Reservoir sub-surface (middle)	5/31/2007	6.5	8.25	6.71	ND
FM-3 (S)	French Meadows Reservoir surface (upper)	5/31/2007	6.6	16.45	5.76	#N/A
FM-3	French Meadows Reservoir sub-surface (upper)	5/31/2007	6.6	9.89	6.55	ND
MFAR-2 RM 46.6	Middle Fork American River below French Meadows Dam at gaging station	5/22/2007	7.4	10.60	4.73	#N/A
MFAR-3 RM39.9	Middle Fork American River above Duncan Creek confluence	5/17/2007	7.7	13.17	3.66	#N/A
MFAR-4 RM39.5	Middle Fork American River below Duncan Creek confluence	5/17/2007	7.8	12.44	3.07	#N/A
MFAR-5 RM36.3	Middle Fork American River above Middle Fork Interbay	5/16/2007	8.4	13.25	1.29	ND
IR-1 RM35.7	In Middle Fork Interbay	5/16/2007	7.2	13.77	5.42	#N/A
MFAR-6 RM35.5	Middle Fork American River below Middle Fork Interbay	5/16/2007	7.7	10.02	3.42	ND
MFAR-7 RM26.1	Middle Fork American River above Ralston Afterbay	5/22/2007	7.4	15.44	4.46	#N/A
RA-1(S)	Ralston Afterbay surface	5/29/2007	6.6	19.15	4.89	ND
RA-1	Ralston Afterbay sub-surface	5/29/2007	6.5	12.02	6.70	ND
MFAR-8 RM24.7	Middle Fork American River below dam	5/21/2007	7.0	18.76	4.43	#N/A
MFAR-9 RM24.3	Middle Fork American River below Oxbow Powerhouse tailrace	5/21/2007	7.3	15.32	4.88	#N/A
MFAR-10 RM9.1	Middle Fork American River below the Drivers Flat Road Rafting Take-Out	5/14/2007	6.8	16.53	5.58	#N/A
MFAR-11 RM0.1	Middle Fork American River above North Fork American River	5/16/2007	7.3	19.73	3.74	ND
NFAR-1 RM20.6	North Fork American River below Middle Fork American River	5/16/2007	7.4	18.51	3.66	#N/A
RR-1 RM35.9	Rubicon River above Reservoir	5/24/2007	7.8	9.60	3.18	#N/A
HH-1 (S)	Hell Hole Reservoir surface (lower)	5/30/2007	7.0	14.52	5.89	#N/A
HH-1	Hell Hole Reservoir sub-surface (lower)	5/30/2007	6.7	6.65	6.49	ND
HH-2 (S)	Hell Hole Reservoir surface (middle)	5/30/2007	6.9	14.72	6.02	#N/A
HH-2	Hell Hole Reservoir sub-surface (middle)	5/30/2007	6.7	7.99	6.46	ND
HH-3 (S)	Hell Hole Reservoir surface (upper)	5/30/2007	7.1	12.72	5.59	#N/A
HH-3	Hell Hole Reservoir sub-surface (upper)	5/30/2007	6.8	7.79	6.28	ND
RR-2 RM30.2	Rubicon River below dam at gaging station	5/22/2007	7.2	7.13	5.53	#N/A
RR-3 RM 22.8	Rubicon River above South Fork Rubicon River confluence	5/23/2007	7.4	12.19	4.59	#N/A
SFR-1 RM0.2	South Fork Rubicon River above Rubicon River confluence	5/23/2007	7.5	11.83	4.29	#N/A
RR-4 RM22.5	Rubicon River below South Fork Rubicon River confluence	5/23/2007	7.5	12.78	4.55	ND
RR-5 RM3.8	Rubicon River above Long Canyon Creek confluence	5/21/2007	6.9	16.30	5.42	#N/A
RR-6 RM3.5	Rubicon River below Long Canyon Creek confluence	5/21/2007	7.3	16.26	4.65	#N/A
RR-7 RM0.7	Rubicon River above Ralston Afterbay	5/21/2007	7.3	19.61	3.61	ND
NFLC-1 RM3.2	North Fork Long Canyon Creek above diversion	5/15/2007	7.5	12.86	4.40	ND
NFLC-2 RM2.9	North Fork Long Canyon Creek below diversion	5/15/2007	7.7	13.8	3.58	#N/A
NFLC-3 RM0.3	North Fork Long Canyon Creek above Long Canyon Creek confluence	5/15/2007	7.3	10.81	4.94	#N/A
SFLC-1 RM3.4	South Fork Long Canyon Creek above diversion	5/15/2007	6.5	11.31	6.66	ND
SFLC-2 RM3.1	South Fork Long Canyon Creek below diversion	5/15/2007	6.6	11.68	6.54	ND
SFLC-3 RM0.2	South Fork Long Canyon Creek above Long Canyon Creek confluence	5/15/2007	7.2	9.51	5.53	#N/A
LCC-1 RM11.3	Long Canyon Creek below North Fork and South Fork Long Canyon creeks confluence	5/15/2007	7.3	9.61	5.08	#N/A
LCC-2 RM0.3	Long Canyon Creek above Rubicon River confluence	5/21/2007	7.5	15.14	4.27	#N/A

¹Ammonia criteria calculated using guidelines from the National Toxics Rule (NTR), which is based on ambient pH and temperature conditions.

ND: Not detected

Table 11-9. Hardness-based Water Quality Criteria for Cadmium, Copper, Lead, and Nickel for the Spring 2007 Sampling Event.

Station ID	DC-1 RM8.9	DC-2 RM8.8	DC-3 RM0.2	MFAR-1 RM51.6	FM-1(S)	FM-1	FM-2(S)	FM-2	FM-3(S)	FM-3	MFAR-2 RM 46.6	MFAR-3 RM39.9	MFAR-4 RM39.5	MFAR-5 RM36.3	IR-1 RM35.7	MFAR-6 RM35.5	MFAR-7 RM26.1	RA-1(S)	RA-1	MFAR-8 RM24.7	MFAR-9 RM24.3	MFAR-10 RM9.1	MFAR-11 RM0.1
Date Sampled	5/22/2007	5/22/2007	5/17/07	5/22/2007	5/31/2007	5/31/2007	5/31/2007	5/31/2007	5/31/2007	5/31/2007	5/22/2007	5/17/2007	5/17/2007	5/16/2007	5/16/2007	5/16/2007	5/22/2007	5/29/2007	5/29/2007	5/21/2007	5/21/2007	5/14/2007	5/16/2007
Time Sampled	9:45	10:40	11:00	11:40	9:30	8:40	10:00	10:40	13:15	12:15	12:30	12:30	12:00	9:25	10:10	8:50	8:00	12:30	10:40	14:00	13:30	15:50	15:10
Hardness (CaCO ₃) (mg/L)	9.5	9.8	16	8.2	7.5	8.1	7.8	7.9	7.8	7.8	9	15	15	17	16	12	23	18	14	16	16	17	18
Cadmium (Cd)																							
Laboratory Result (ug/L)	0.005 ^B	0.005 ^B	0.004 ^U	0.006 ^B	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	
Maximum Criterion (ug/L)	0.20	0.21	0.34	0.18	0.16	0.17	0.17	0.17	0.17	0.17	0.19	0.32	0.32	0.36	0.34	0.26	0.48	0.38	0.30	0.34	0.34	0.36	0.38
Continuous Criterion (ug/L)	0.05	0.05	0.07	0.04	0.04	0.04	0.04	0.04	0.04	0.04	0.05	0.07	0.07	0.07	0.07	0.06	0.09	0.07	0.06	0.07	0.07	0.07	0.07
Copper (Cu)																							
Laboratory Result (mg/L)	0.000150 ^B	0.000160 ^B	0.000130 ^B	0.000160 ^B	0.000190 ^B	0.000220	0.000190 ^B	0.000180 ^B	0.000180 ^B	0.000180 ^B	0.000190 ^B	0.000140 ^B	0.000160 ^B	0.000180 ^B	0.000590	0.000240	0.000330	0.000340	0.000390	0.000310	0.000340	0.000410	0.000300
Maximum Criterion (mg/L)	0.0015	0.0015	0.0024	0.0013	0.0012	0.0013	0.0012	0.0012	0.0012	0.0012	0.0014	0.0022	0.0022	0.0025	0.0024	0.0018	0.0034	0.0027	0.0021	0.0024	0.0024	0.0025	0.0027
Continuous Criterion (mg/L)	0.0012	0.0012	0.0019	0.0011	0.0010	0.0010	0.0010	0.0010	0.0010	0.0010	0.0011	0.0018	0.0018	0.0020	0.0019	0.0015	0.0026	0.0021	0.0017	0.0019	0.0019	0.0020	0.0021
Lead (Pb)																							
Laboratory Result (ug/L)	0.010 ^U	0.010 ^U	0.010 ^U	0.030 ^B	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U
Maximum Criterion (ug/L)	4.63	4.79	8.38	3.91	3.53	3.85	3.69	3.74	3.69	3.69	4.35	7.79	7.79	8.98	8.38	6.04	12.64	9.58	7.20	8.38	8.38	8.98	9.58
Continuous Criterion (ug/L)	0.18	0.19	0.33	0.15	0.14	0.15	0.14	0.15	0.14	0.14	0.17	0.30	0.30	0.35	0.33	0.24	0.49	0.37	0.28	0.33	0.33	0.35	0.37
Nickel (Ni)																							
Laboratory Result (ug/L)	0.180 ^B	0.170 ^B	0.160 ^B	0.080 ^B	0.040 ^U	0.040 ^U	0.040 ^U	0.040 ^U	0.040 ^U	0.040 ^U	0.060 ^B	0.070 ^B	0.110 ^B	0.100 ^B	0.120 ^B	0.090 ^B	0.210	0.090 ^B	0.090 ^B	0.150 ^B	0.130 ^B	0.230	0.250
Maximum Criterion (ug/L)	63.92	65.62	99.35	56.44	52.33	55.85	54.10	54.68	54.10	54.10	61.06	94.07	94.07	104.57	99.35	77.88	135.05	109.76	88.73	99.35	99.35	104.57	109.76
Continuous Criterion (ug/L)	7.10	7.29	11.03	6.27	5.81	6.20	6.01	6.07	6.01	6.01	6.78	10.45	10.45	11.61	11.03	8.65	15.00	12.19	9.86	11.03	11.03	11.61	12.19

Station ID	NFAR-1 RM20.6	RR-1 RM35.9	HH-1(S)	HH-1	HH-2(S)	HH-2	HH-3(S)	HH-3	RR-2 RM30.2	RR-3 RM 22.8	SFRR-1 RM0.2	RR-4 RM22.5	RR-5 RM3.8	RR-6 RM3.5	RR-7 RM0.7	NFLC-1 RM3.2	NFLC-2 RM2.9	NFLC-3 RM0.3	SFLC-1 RM3.4	SFLC-2 RM3.1	SFLC-3 RM0.2	LCC-1 RM11.3	LCC-2 RM0.3
Date Sampled	5/16/2007	5/24/2007	5/22/2007	5/22/2007	5/22/2007	5/22/2007	5/22/2007	5/22/2007	5/22/2007	5/23/2007	5/23/2007	5/23/2007	5/21/2007	5/21/2007	5/21/2007	5/15/2007	5/15/2007	5/15/2007	5/15/2007	5/15/2007	5/15/2007	5/15/2007	5/21/2007
Time Sampled	14:30	10:40	13:45	13:00	11:00	10:30	12:00	11:30	14:00	11:40	11:00	12:20	9:20	10:15	14:45	13:30	14:10	10:20	11:30	11:55	9:30	8:50	9:40
Hardness (CaCO ₃) (mg/L)	21	8.3	11	9.6	9.3	9.6	9.6	9.3	9.3	14	8.2	12	17	16	17	9.2	9.6	11	10	12	9.7	11	17
Cadmium (Cd)																							
Laboratory Result (ug/L)	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	
Maximum Criterion (ug/L)	0.44	0.18	0.23	0.21	0.20	0.21	0.21	0.20	0.20	0.30	0.18	0.26	0.36	0.34	0.36	0.20	0.21	0.23	0.21	0.26	0.21	0.23	0.36
Continuous Criterion (ug/L)	0.08	0.04	0.05	0.05	0.05	0.05	0.05	0.05	0.05	0.06	0.04	0.06	0.07	0.07	0.07	0.05	0.05	0.05	0.05	0.06	0.05	0.05	0.07
Copper (Cu)																							
Laboratory Result (mg/L)	0.000430	0.000200 ^B	0.000270	0.000490	0.000270	0.000290	0.000250	0.000260	0.000310	0.000430	0.000130 ^B	0.000380	0.000360	0.000330	0.000350	0.000100 ^B	0.000090 ^B	0.000200 ^B	0.000100 ^B	0.000110 ^B	0.000130 ^B	0.000150 ^B	0.000200 ^B
Maximum Criterion (mg/L)	0.0031	0.0013	0.0017	0.0015	0.0014	0.0015	0.0015	0.0014	0.0014	0.0021	0.0013	0.0018	0.0025	0.0024	0.0025	0.0014	0.0015	0.0017	0.0015	0.0018	0.0015	0.0017	0.0025
Continuous Criterion (mg/L)	0.0024	0.0011	0.0014	0.0012	0.0012	0.0012	0.0012	0.0012	0.0012	0.0017	0.0011	0.0015	0.0020	0.0019	0.0020	0.0012	0.0012	0.0014	0.0013	0.0015	0.0012	0.0014	0.0020
Lead (Pb)																							
Laboratory Result (ug/L)	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.050 ^B	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U
Maximum Criterion (ug/L)	11.40	3.96	5.47	4.68	4.51	4.68	4.68	4.51	4.51	7.20	3.91	6.04	8.98	8.38	8.98	4.46	4.68	5.47	4.91	6.04	4.74	5.47	8.98
Continuous Criterion (ug/L)	0.44	0.15	0.21	0.18	0.18	0.18	0.18	0.18	0.18	0.28	0.15	0.24	0.35	0.33	0.35	0.17	0.18	0.21	0.19	0.24	0.18	0.21	0.35
Nickel (Ni)																							
Laboratory Result (ug/L)	0.380	0.090 ^B	0.100 ^B	0.100 ^B	0.110 ^B	0.100 ^B	0.090 ^B	0.090 ^B	0.090 ^B	0.100 ^B	0.100 ^B	0.090 ^B	0.130 ^B	0.120 ^B	0.140 ^B	0.040 ^U	0.040 ^U	0.050 ^B	0.040 ^U	0.040 ^U	0.040 ^U	0.040 ^U	0.100 ^B
Maximum Criterion (ug/L)	125.04	57.02	72.36	64.49	62.78	64.49	64.49	62.78	62.78	88.73	56.44	77.88	104.57	99.35	104.57	62.21	64.49	72.36	66.75	77.88	65.05	72.36	104.57
Continuous Criterion (ug/L)	13.89	6.33	8.04	7.16	6.97	7.16	7.16	6.97	6.97	9.86	6.27	8.65	11.61	11.03	11.61	6.91	7.16	8.04	7.41	8.65	7.23	8.04	11.61

Note: Bold results do not meet the calculated criteria

U: Results are less than or equal to the method detection limit (MDL) and are considered 'non-detect'.

B: Results are above the MDL and less than or equal to the practical quantitation limit (POL) and should be considered estimates.

California Toxics Rule (CTR) standard was used for Cu, Pb, and Ni. National Toxics Rule (NTR) standard was used for Cd.

Formulas used are provided in Appendix C.

Table AQ 11-10. Summary of Analytical Results of Water Quality Sampling for Fall 2007.

				Station	DC-1 RM8.9	DC-2 RM8.8	DC-3 RM0.2	MFAR-1 RM51.6	FM-1(S)	FM-1	FM-2(S)	FM-2	FM-3(S)	FM-3	MFAR-2 RM 46.6	MFAR-3 RM39.9	MFAR-4 RM39.5	MFAR-5 RM36.3	IR-1 RM35.7	MFAR-6 RM35.5	MFAR-7 RM26.1	RA-1(S)	RA-1	
				Date	9/25/2007	9/25/2007	*	10/3/2007	10/3/2007	10/3/2007	10/3/2007	10/3/2007	10/3/2007	10/3/2007	10/3/2007	10/3/2007	*	*	9/24/2007	9/24/2007	9/24/2007	9/26/2007	9/26/2007	9/26/2007
				Time	15:30	16:00	*	12:00	9:30	9:00	11:00	10:15	13:00	12:30	11:25	*	*	11:15	10:40	11:50	13:15	10:15	10:40	
General Parameters	Units	PQL	WQ Criteria																					
Calcium	mg/L	0.5	NS		7	6.3	*	4.9	2.4	2.4	2.4	2.5	2.5	2.4	2.7	*	*	6.9	6.8	3.7	6	4	3.7	
Chloride	mg/L	1.0	250 ¹		1	1	*	3.7	1.1	ND	2.2	1	1.3	2.3	2	*	*	1.4	1.3	1.1	1.5	1.8	1.5	
Hardness (as CaCO ₃)	mg/L	1.0	NS		25	22	*	18	8.4	8.4	8.4	8.7	8.8	8.5	9.3	*	*	22	22	12	19	13	12	
Magnesium	µg/L	100	NS		1900	1600	*	1300	590	590	580	600	610	600	630	*	*	1200	1200	670	980	710	660	
Nitrate/Nitrite (NO ₃)	mg/L	0.20	1 ¹		ND	ND	*	ND	ND	ND	ND	ND	ND	ND	ND	*	*	ND	ND	ND	ND	ND	ND	
Ammonia as N	mg/L	0.100	1.5		ND	ND	*	0.121	0.167	0.133	0.117	0.207	0.101	0.122	ND	*	*	ND	ND	ND	ND	ND	ND	
Total Kjeldahl Nitrogen (TKN)	mg/L	0.100	NS		0.268	ND	*	ND	ND	ND	0.173	0.211	0.148	0.102	ND	*	*	0.26	0.32	0.352	0.374	0.317	0.293	
Total Phosphorus	mg/L	0.100	NS		ND	ND	*	ND	ND	ND	ND	ND	ND	ND	ND	*	*	0.058	ND	ND	ND	ND	ND	
Ortho-phosphate	mg/L	0.010	NS		ND	ND	*	ND	ND	ND	ND	ND	ND	ND	ND	*	*	ND	ND	ND	ND	ND	ND	
Potassium	mg/L	0.20	NS		ND	ND	*	ND	ND	ND	ND	ND	ND	ND	ND	*	*	ND	ND	ND	ND	ND	ND	
Sodium	mg/L	0.50	NS		2.8	2.5	*	2.8	1.3	1.3	1.2	1.3	1.3	1.3	1.2	*	*	2	2.2	1.6	1.7	1.8	1.7	
Sulfate (SO ₄)	mg/L	0.50	250 ¹		1.4	1.4	*	1.2	0.65	0.72	0.57	2.9	0.68	0.66	0.83	*	*	1.5	1.5	0.94	2.3	1.1	0.98	
Total Dissolved Solids	mg/L	10	500 ¹		52	52	*	76	58	66	46	52	58	54	52	*	*	52	52	38	38	26	26	
Total Suspended Solids	mg/L	10	NS		ND	ND	*	ND	ND	ND	ND	ND	ND	ND	ND	*	*	ND	ND	ND	ND	ND	ND	
Turbidity	NTU	0.10	(5)		ND	0.8	*	0.41	0.36	0.3	0.5	0.4	0.42	0.41	0.44	*	*	0.19	ND	0.25	0.4	0.76	0.25	
Organic Carbon, Total (TOC)	mg/L	1.00	NS		ND	ND	*	ND	1.59	ND	ND	ND	ND	ND	ND	*	*	ND	ND	1.5	ND	ND	ND	
Total Alkalinity	mg/L	5.0	>20 ³		31	30	*	21	14	14	14	13	13	13	14	*	*	24	29	17	24	17	17	
Metals-Dissolved																								
Arsenic	µg/L	0.20	10 ¹		0.090 ^B	0.150 ^B	*	0.120 ^B	0.150 ^B	0.110 ^B	0.120 ^B	0.150 ^B	0.150 ^B	0.150 ^B	0.110 ^B	*	*	0.100 ^B	0.110 ^B	0.200 ^B	0.200 ^B	0.170 ^B	0.170 ^B	
Cadmium	µg/L	0.010	(6)		0.004 ^U	0.004 ^U	*	0.005 ^B	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	*	*	0.004 ^U	0.004 ^U	0.005 ^B	0.004 ^U	0.004 ^U	0.005 ^B	
Copper	mg/L	0.00020	(6)		0.000170	0.000310	*	0.000210	0.000190	0.000170	0.000200	0.000220	0.000180	0.000220	0.000170	*	*	0.000160	0.000220	0.000380	0.000320	0.000330	0.000310	
Iron	mg/L	0.005	0.3 ¹		0.012300	0.196000	*	0.001400 ^U	0.001400 ^U	0.001400 ^U	0.001400 ^U	0.001400 ^U	0.001400 ^U	0.001400 ^U	0.022800	*	*	0.016500	0.017100	0.018300	0.016300	0.012800	0.012200	
Lead	µg/L	0.050	(6)		0.010 ^U	0.010 ^U	*	0.0510	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	*	*	0.010 ^U	0.022 ^B	0.033 ^B	0.010 ^U	0.010 ^U	0.010 ^U	
Manganese	µg/L	0.05	50 ¹		0.406	46.820	*	1.520	0.299	1.800	0.570	0.355	0.595	1.850	57.700	*	*	1.200	1.100	4.970	0.937	6.700	6.780	
Nickel	µg/L	0.20	(6)		0.050 ^B	0.120 ^B	*	0.040 ^U	0.040 ^U	0.040 ^U	0.040 ^U	0.040 ^U	0.040 ^U	0.040 ^U	0.040 ^U	*	*	0.050 ^B	0.040 ^U	0.060 ^B	0.080 ^B	0.050 ^B	0.040 ^U	
Chromium-Total	µg/L	0.15	50 ¹		0.030 ^U	0.030 ^U	*	0.050 ^B	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	*	*	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	
Metals-Total																								
Mercury	µg/L	0.0004	0.052		0.000230 ^B	0.000410	*	0.000240 ^B	0.000210 ^B	0.000250 ^B	0.000190 ^B	0.000330 ^B	0.000230 ^B	0.000240 ^B	0.000390 ^B	*	*	0.000360 ^B	0.000360 ^B	0.00069	0.000180 ^B	0.000340 ^B	0.000320 ^B	
Hydrocarbons																								
Methyl-tertiary-butyl Ether (MtBE)	µg/L	0.50	5 ¹						ND	ND	ND	ND	ND	ND								ND	ND	
Total Petroleum Hydrocarbons (as gasoline and as diesel)	µg/L	50	NS						ND	ND	ND	ND	ND	ND								ND	ND	
Oil and Grease	mg/L	4.8	NS						ND	ND	ND	ND	ND	ND								ND	ND	
Bacteria																								
Total Coliform (3x5, 6 hr hold)	MPN/100 mL	2	NS		50	70	*	50	<2	2	<2	2	2	<2	13	*	*	220	500	130	80	27	22	
Fecal Coliform (3x5)	MPN/100 mL	2-1600	200/100 ¹		4	<2	*	17	<2	<2	<2	<2	<2	<2	<2	*	*	4	7	<2	11	2	<2	

Table AQ 11-10. Summary of Analytical Results of Water Quality Sampling for Fall 2007 (continued).

				Station	MFAR-8 RM24.7	MFAR-9 RM24.3	MFAR-10 RM9.1	MFAR-11 RM0.1	NFAR-1 RM20.6	RR-1 RM35.9	HH-1(S)	HH-1	HH-2(S)	HH-2	HH-3(S)	HH-3	RR-2 RM30.2	RR-3 RM 22.8	SFRR-1 RM0.2	RR-4 RM22.5
				Date	9/26/2007	9/26/2007	9/24/2007	9/25/2007	9/25/2007	10/2/2007	10/1/2007	10/1/2007	10/1/2007	10/1/2007	10/2/2007	10/2/2007	10/3/2007	9/25/2007	9/25/2007	9/25/2007
				Time	14:15	14:45	13:25	9:00	9:40	11:40	14:55	14:15	12:00	12:50	10:15	9:00	10:20	13:00	12:30	13:30
General Parameters	Units	PQL	WQ Criteria																	
Calcium	mg/L	0.5	NS		4.2	3.8	4.2	5	7	7.9	2.8	2.9	2.8	2.8	2.9	2.9	3	4.3	2.1	4
Chloride	mg/L	1.0	250 ¹		1.4	1.6	1.5	1.5	1.8	24	1	ND	ND	ND	ND	ND	2.4	6.1	ND	5.1
Hardness (as CaCO ₃)	mg/L	1.0	NS		14	12	14	17	24	25	9.3	9.7	9.3	9.3	9.6	9.5	9.8	13	6.6	12
Magnesium	µg/L	100	NS		810	680	940	1100	1700	1200	550	590	570	560	570	560	560	620	330	600
Nitrate/Nitrite (NO ₃)	mg/L	0.20	1 ¹		ND	ND	ND	ND	ND	0.29	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Ammonia as N	mg/L	0.100	1.5		ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	0.118	ND
Total Kjeldahl Nitrogen (TKN)	mg/L	0.100	NS		ND	0.462	0.277	0.253	0.324	ND	ND	0.341	0.246	0.293	ND	ND	ND	0.524	0.601	0.328
Total Phosphorus	mg/L	0.100	NS		0.106	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Ortho-phosphate	mg/L	0.010	NS		ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Potassium	mg/L	0.20	NS		ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Sodium	mg/L	0.50	NS		1.7	1.7	1.8	1.9	2.5	7.3	1.4	1.5	1.4	1.4	1.5	1.4	1.3	3.5	1.1	3.2
Sulfate (SO ₄)	mg/L	0.50	250 ¹		1.2	1	1.5	1.6	2.4	1.2	0.67	0.63	0.72	0.63	0.63	0.65	0.94	0.77	0.86	0.78
Total Dissolved Solids	mg/L	10	500 ¹		36	60	44	34	46	94	46	44	46	50	34	38	86	52	14	32
Total Suspended Solids	mg/L	10	NS		ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Turbidity	NTU	0.10	(5)		0.56	0.46	ND	0.2	0.27	ND	0.21	0.34	0.3	0.36	0.34	0.3	0.54	0.13	ND	ND
Organic Carbon, Total (TOC)	mg/L	1.00	NS		ND	ND	1.3	ND	ND	ND	ND	1.47	ND	ND	ND	ND	ND	ND	ND	ND
Total Alkalinity	mg/L	5.0	>20 ³		17	17	18	22	28	17	15	15	14	15	14	15	12	17	11	14
Metals-Dissolved																				
Arsenic	µg/L	0.20	10 ¹		0.170 ^B	0.180 ^B	0.210	0.240	0.340	0.280	0.210	0.210	0.220	0.190 ^B	0.220	0.200 ^B	0.190 ^B	0.180 ^B	0.060 ^U	0.160 ^B
Cadmium	µg/L	0.010	(6)		0.013	0.004 ^U	0.004 ^U	0.004 ^U	0.005 ^B	0.008 ^B	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U
Copper	mg/L	0.00020	(6)		0.000340	0.000310	0.000320	0.000290	0.000330	0.000140	0.000270	0.000280	0.000260	0.000280	0.000280	0.000270	0.000510	0.000370	0.000130	0.000290
Iron	mg/L	0.005	0.3 ¹		0.049400	0.012700	0.016600	0.014900	0.021300	0.001400 ^U	0.001400 ^U	0.001400 ^U	0.001400 ^U	0.001400 ^U	0.001400 ^U	0.001400 ^U	0.015700	0.008800	0.006400	0.007700
Lead	µg/L	0.050	(6)		0.015 ^B	0.010 ^U	0.010 ^U	0.012 ^B	0.015 ^B	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U	0.010 ^U
Manganese	µg/L	0.05	50 ¹		16.700	7.720	3.560	1.120	1.290	0.847	0.871	0.391	0.354	0.479	1.190	0.696	44.900	0.188	0.334	0.114
Nickel	µg/L	0.20	(6)		0.015 ^B	0.040 ^U	0.130 ^B	0.140 ^B	0.140 ^B	0.040 ^U	0.040 ^U	0.040 ^U	0.040 ^U	0.040 ^U	0.040 ^U	0.040 ^U	0.040 ^U	0.040 ^U	0.050 ^B	0.040 ^U
Chromium-Total	µg/L	0.15	50 ¹		0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.130 ^B	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U
Metals-Total																				
Mercury	µg/L	0.0004	0.052		0.000320 ^B	0.000350 ^B	0.000740	0.000540	0.000460	0.000150 ^U	0.000350 ^B	0.000430	0.000320 ^B	0.000400 ^B	0.000300 ^B	0.000280 ^B	0.001260	0.000150 ^U	0.000200 ^B	0.000230 ^B
Hydrocarbons																				
Methyl-tertiary-butyl Ether (MtBE)	µg/L	0.50	5 ¹								ND	ND	ND	ND	ND	ND				
Total Petroleum Hydrocarbons (as gasoline and as diesel)	µg/L	50	NS								ND	ND	ND	ND	ND	ND				
Oil and Grease	mg/L	4.8	NS								ND	ND	ND	ND	ND	ND				
Bacteria																				
Total Coliform (3x5, 6 hr hold)	MPN/100 mL	2	NS		7	6	240	50	140	8	2	13	2	<2	<2	<2	4	30	8	27
Fecal Coliform (3x5)	MPN/100 mL	2-1600	200/100 ¹		<2	<2	4	7	4	<2	<2	<2	<2	<2	<2	<2	<2	<2	<2	<2

Table AQ 11-10. Summary of Analytical Results of Water Quality Sampling for Fall 2007 (continued).

				Station	RR-5 RM3.8	RR-6 RM3.5	RR-7 RM0.7	NFLC-1 RM3.2	NFLC-2 RM2.9	NFLC-3 RM0.3	SFLC-1 RM3.4	SFLC-2 RM3.1	SFLC-3 RM0.2	LCC-1 RM11.3	LCC-2 RM0.3
				Date	9/27/2007	9/27/2007	9/26/2007	10/2/2007	10/2/2007	10/2/2007	10/2/2007	10/2/2007	10/2/2007	10/2/2007	9/27/2007
				Time	9:45	10:20	13:45	12:10	12:30	11:10	13:00	13:20	11:20	10:00	10:00
General Parameters	Units	PQL	WQ Criteria												
Calcium	mg/L	0.5	NS		5	5.2	5.8	5.8	5.7	3.7	4.6	4.7	3.7	3.6	9.6
Chloride	mg/L	1.0	250 ¹		5.2	5.2	4.9	ND	ND	1.5	ND	ND	1.9	1.7	3.8
Hardness (as CaCO ₃)	mg/L	1.0	NS		16	17	19	21	21	13	17	18	13	13	33
Magnesium	µg/L	100	NS		870	930	1100	1700	1700	980	1400	1400	1000	970	2100
Nitrate/Nitrite (NO ₃)	mg/L	0.20	1 ¹		ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Ammonia as N	mg/L	0.100	1.5		ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Total Kjeldahl Nitrogen (TKN)	mg/L	0.100	NS		2.72	0.34	0.267	ND	ND	ND	ND	ND	0.123	0.108	0.32
Total Phosphorus	mg/L	0.100	NS		ND	ND	ND	ND	ND	ND	0.103	ND	ND	ND	ND
Ortho-phosphate	mg/L	0.010	NS		ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Potassium	mg/L	0.20	NS		2	ND	2.2	ND	ND	ND	ND	ND	ND	ND	ND
Sodium	mg/L	0.50	NS		3	3.1	3.3	4	4	3.9	2.7	2.7	3.3	3.5	4.2
Sulfate (SO ₄)	mg/L	0.50	250 ¹		1.4	1.5	1.8	0.98	ND	0.63	ND	ND	1	0.88	2.1
Total Dissolved Solids	mg/L	10	500 ¹		38	46	50	64	92	84	84	66	66	66	72
Total Suspended Solids	mg/L	10	NS		ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Turbidity	NTU	0.10	(5)		ND	0.1	0.27	ND	0.28	0.15	0.16	0.1	ND	0.2	ND
Organic Carbon, Total (TOC)	mg/L	1.00	NS		ND	ND	ND	ND	ND	ND	ND	ND	ND	ND	ND
Total Alkalinity	mg/L	5.0	>20 ³		19	20	22	35	32	24	29	28	23	23	40
Metals-Dissolved															
Arsenic	µg/L	0.20	10 ¹		0.120 ^B	0.130 ^B	0.130 ^B	0.150 ^B	0.140 ^B	0.260	0.100 ^B	0.110 ^B	0.180 ^B	0.210	0.210
Cadmium	µg/L	0.010	(6)		0.004 ^U	0.004 ^U	0.005 ^B	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U	0.004 ^U
Copper	mg/L	0.00020	(6)		0.000280	0.000270	0.000280	0.00013 ^B	0.00012 ^B	0.000400	0.000150	0.00012 ^B	0.0002 ^B	0.000300	0.000300
Iron	mg/L	0.005	0.3 ¹		0.001400 ^U	0.001400 ^U	0.013100	0.001400 ^U	0.007100	0.001400 ^U	0.001400 ^U	0.015200	0.001400 ^U	0.001400 ^U	0.001400 ^U
Lead	µg/L	0.050	(6)		0.010 ^U	0.011 ^B	0.064	0.010 ^U	0.010 ^U	0.048 ^B	0.011 ^B	0.010 ^U	0.010 ^U	0.015 ^B	0.015 ^B
Manganese	µg/L	0.05	50 ¹		0.183	0.203	0.404	0.097	21.200	0.716	1.020	6.700	0.434	0.703	0.636
Nickel	µg/L	0.20	(6)		0.040 ^U	0.040 ^U	0.040 ^U	0.040 ^U	0.040 ^U	0.040 ^U	0.040 ^U	0.040 ^U	0.040 ^U	0.040 ^U	0.040 ^U
Chromium-Total	µg/L	0.15	50 ¹		0.060 ^B	0.060 ^B	0.030 ^U	0.030 ^U	0.030 ^U	0.030 ^U	0.050 ^B	0.040 ^B	0.050 ^B	0.040 ^B	0.030 ^U
Metals-Total															
Mercury	µg/L	0.0004	0.052		0.000150 ^U	0.000170 ^B	0.000150 ^U	0.00050	0.001040	0.001230	0.000180 ^B	0.000260 ^B	0.000320 ^B	0.000770	0.000360
Hydrocarbons															
Methyl-tertiary-butyl Ether (MtBE)	µg/L	0.50	5 ¹												
Total Petroleum Hydrocarbons (as gasoline and as diesel)	µg/L	50	NS												
Oil and Grease	mg/L	4.8	NS												
Bacteria															
Total Coliform (3x5, 6 hr hold)	MPN/100 mL	2	NS		300	900	170	4	300	80	170	11	13	23	30
Fecal Coliform (3x5)	MPN/100 mL	2-1600	200/100 ¹		<2	<2	2	<2	300	2	170	2	2	8	2

Note: Bold results do not meet the listed criteria

PQL: Practical Quantitation Limit: the lowest concentration of an analyte that can be reliably measured within specified limits of precision and accuracy during routine laboratory operating conditions.

ND: Not detected above the PQL.

NS: No standard.

*: Sample location was not sampled during the fall sampling event due to dangerous access conditions.

U: Results less than or equal to the method detection limit (MDL) and are considered 'non-detect'.

B: Results are above the MDL and less than or equal to the practical quantitation limit (PQL) and should be considered estimates.

1: Basin Plan criteria for the Sacramento and San Joaquin Rivers Basins.

2: California Toxics Rule Criteria (CTR)

3: National Toxics Rule Criteria (NTR)

4: pH, temperature and life cycle dependent. See Table 11-14 for criteria and results.

5: Increases in turbidity attributable to controllable water quality factors shall not exceed the following limits: where natural turbidity is between 0 and 5 NTU's, increases shall not exceed 1 NTU. Where natural turbidity is between 5 and 50 NTU's, increases shall not exceed 20%. Where natural turbidity is between 50 and 100 NTU's, increases shall not exceed 10 NTU's. Finally, where natural turbidity is greater than 100 NTU's, increases shall not exceed 10%.

6: Criteria are hardness dependent which is expressed as a function of hardness and decreases as hardness decreases. The actual criteria are calculated based on the hardness (as CaCO₃) of the sample water. Refer to Table 11-15 for sample site criteria and results.

Attachment F (b)

ARPS Title 22 Water Quality Sampling Results 2017-2020 /2022
-2025

American River Water Quality Results 2017-2019					
Group/Constituent Identification	Sampling Date	Result	Maximum Contaminant Level (for drinking water purposes only)	Detection Limit for the Purposes of Reporting	Unit
PH, FIELD	2017-01-04	7.2	N/A	0	
ALKALINITY (TOTAL) AS CaCO3	2017-02-14	44	N/A	0	MG/L
BICARBONATE ALKALINITY	2017-02-14	44	N/A	0	MG/L
CARBONATE ALKALINITY	2017-02-14	0	N/A	0	MG/L
TOTAL ORGANIC CARBON (TOC)	2017-02-14	1.36	N/A	0.3	MG/L
HYDROXIDE ALKALINITY	2017-02-14	0	N/A	0	MG/L
PH, FIELD	2017-03-08	7.5	N/A	0	
SOURCE TEMPERATURE C	2017-04-05	15	N/A	0	C
PH, FIELD	2017-05-03	7	N/A	0	
ALKALINITY (TOTAL) AS CaCO3	2017-05-10	46	N/A	0	MG/L
BICARBONATE ALKALINITY	2017-05-10	46	N/A	0	MG/L
CARBONATE ALKALINITY	2017-05-10	0	N/A	0	MG/L
TOTAL ORGANIC CARBON (TOC)	2017-05-10	1.63	N/A	0.3	MG/L
HYDROXIDE ALKALINITY	2017-05-10	0	N/A	0	MG/L
SOURCE TEMPERATURE C	2017-08-02	19	N/A	0	C
NITRATE (AS N)	2017-08-08	0	10	0.4	mg/L
NITRITE (AS N)	2017-08-08	0	1	0.4	mg/L
ARSENIC	2017-08-08	0	10	2	UG/L
CHROMIUM, HEXAVALENT	2017-08-08	0	10	1	UG/L
THALLIUM	2017-08-08	0	2	1	UG/L
NICKEL	2017-08-08	0	100	10	UG/L
SILVER	2017-08-08	0	100	10	UG/L
ANTIMONY	2017-08-08	0	6	6	UG/L
ALUMINIUM	2017-08-08	0	1000	50	UG/L
SELENIUM	2017-08-08	0	50	5	UG/L
PERCHLORATE	2017-08-08	0	6	4	UG/L
TOTAL ORGANIC CARBON (TOC)	2017-11-14	0.93	N/A	0.3	MG/L
ALKALINITY (TOTAL) AS CaCO3	2018-02-13	32.4	N/A	0	MG/L
BICARBONATE ALKALINITY	2018-02-13	39.5	N/A	0	MG/L
CARBONATE ALKALINITY	2018-02-13	0	N/A	0	MG/L
TOTAL ORGANIC CARBON (TOC)	2018-02-13	1	N/A	0.3	MG/L
HYDROXIDE ALKALINITY	2018-02-13	0	N/A	0	MG/L
1,2,3-TRICHLOROPROPANE (1,2,3-TCP)	2018-02-13	0	0.005	0.005	UG/L
TOTAL ORGANIC CARBON (TOC)	2018-05-16	1.2	N/A	0.3	MG/L
1,2,3-TRICHLOROPROPANE (1,2,3-TCP)	2018-05-16	0	0.005	0.005	UG/L
COLOR	2018-08-14	5	15	0	UNITS
ODOR THRESHOLD @ 60 C	2018-08-14	3	3	1	TON
SPECIFIC CONDUCTANCE	2018-08-14	50.3	1600	0	US
PH, LABORATORY	2018-08-14	7.58	N/A	0	
ALKALINITY (TOTAL) AS CaCO3	2018-08-14	21.5	N/A	0	MG/L
BICARBONATE ALKALINITY	2018-08-14	26.2	N/A	0	MG/L
CARBONATE ALKALINITY	2018-08-14	0	N/A	0	MG/L
NITRATE (AS N)	2018-08-14	0	10	0.4	mg/L
NITRITE (AS N)	2018-08-14	0	1	0.4	mg/L
TOTAL ORGANIC CARBON (TOC)	2018-08-14	1.5	N/A	0.3	MG/L
HARDNESS (TOTAL) AS CaCO3	2018-08-14	16	N/A	0	MG/L
CALCIUM	2018-08-14	5	N/A	0	MG/L
MAGNESIUM	2018-08-14	0.8	N/A	0	MG/L
SODIUM	2018-08-14	1.6	N/A	0	MG/L
CHLORIDE	2018-08-14	0.94	500	0	MG/L
SULFATE	2018-08-14	1.60	500	0.5	MG/L
FLUORIDE (F) (NATURAL-SOURCE)	2018-08-14	0	2	0.1	MG/L
ARSENIC	2018-08-14	0.75	10	2	UG/L
BARIUM	2018-08-14	13.32	1000	100	UG/L
BERYLLIUM	2018-08-14	0	4	1	UG/L
CADMIUM	2018-08-14	0	5	1	UG/L
CHROMIUM (TOTAL)	2018-08-14	0	50	10	UG/L
COPPER	2018-08-14	0	1000	50	UG/L
IRON	2018-08-14	0	300	100	UG/L
MANGANESE	2018-08-14	2.93	50	20	UG/L
THALLIUM	2018-08-14	0	2	1	UG/L
NICKEL	2018-08-14	0	100	10	UG/L
SILVER	2018-08-14	0.88	100	10	UG/L
ZINC	2018-08-14	0	5000	50	UG/L
ANTIMONY	2018-08-14	0	6	6	UG/L
ALUMINIUM	2018-08-14	7.2	1000	50	UG/L
SELENIUM	2018-08-14	0	50	5	UG/L
BROMODICHLOROMETHANE (THM)	2018-08-14	0	N/A	1	UG/L
CARBON TETRACHLORIDE	2018-08-14	0	0.5	0.5	UG/L
BROMOFORM (THM)	2018-08-14	0	N/A	1	UG/L
DIBROMOCHLOROMETHANE (THM)	2018-08-14	0	N/A	1	UG/L
CHLOROFORM (THM)	2018-08-14	0	N/A	1	UG/L
TOLUENE	2018-08-14	0	150	0.5	UG/L
BENZENE	2018-08-14	0	1	0.5	UG/L
MONOCHLOROETHYLENE	2018-08-14	0	70	0.5	UG/L
CHLOROETHANE	2018-08-14	0	N/A	0.5	UG/L
ETHYL BENZENE	2018-08-14	0	300	0.5	UG/L
HEXACHLOROBUTADIENE	2018-08-14	0	N/A	0.5	UG/L
BROMOMETHANE	2018-08-14	0	N/A	0.5	UG/L
CHLOROMETHANE	2018-08-14	0	N/A	0.5	UG/L
DICHLOROMETHANE	2018-08-14	0	5	0.5	UG/L
TETRACHLOROETHYLENE	2018-08-14	0	5	0.5	UG/L
TRICHLOROFLUOROMETHANE FREON 11	2018-08-14	0	150	5	UG/L
1,1-DICHLOROETHANE	2018-08-14	0	5	0.5	UG/L
1,1-DICHLOROETHYLENE	2018-08-14	0	6	0.5	UG/L
1,1,1-TRICHLOROETHANE	2018-08-14	0	200	0.5	UG/L

1,1,2-TRICHLOROETHANE	2018-08-14	0	5	0.5	UG/L
1,1,2,2-TETRACHLOROETHANE	2018-08-14	0	1	0.5	UG/L
1,2-DICHLOROETHANE	2018-08-14	0	0.5	0.5	UG/L
1,2-DICHLOROBENZENE	2018-08-14	0	600	0.5	UG/L
1,2-DICHLOROPROPANE	2018-08-14	0	5	0.5	UG/L
TRANS-1,2-DICHLOROETHYLENE	2018-08-14	0	10	0.5	UG/L
1,2,4-TRICHLOROBENZENE	2018-08-14	0	5	0.5	UG/L
1,3-DICHLOROPROPENE (TOTAL)	2018-08-14	0	0.5	0.5	UG/L
1,3-DICHLOROBENZENE	2018-08-14	0	N/A	0.5	UG/L
1,4-DICHLOROBENZENE	2018-08-14	0	5	0.5	UG/L
DICHLORODIFLUOROMETHANE (FREON 12)	2018-08-14	0	N/A	0.5	UG/L
NAPHTHALENE	2018-08-14	0	N/A	0.5	UG/L
TRANS-1,3-DICHLOROPROPENE	2018-08-14	0	0.5	0.5	UG/L
CIS-1,3-DICHLOROPROPENE	2018-08-14	0	0.5	0.5	UG/L
FOAMING AGENTS (MBAS)	2018-08-14	0	0.5	0	MG/L
VINYL CHLORIDE	2018-08-14	0	0.5	0.5	UG/L
TRICHLOROETHYLENE	2018-08-14	0	5	0.5	UG/L
METHYL-TERT-BUTYL-ETHER (MTBE)	2018-08-14	0	13	3	UG/L
TOTAL DISSOLVED SOLIDS	2018-08-14	23	1000	0	MG/L
HYDROXIDE ALKALINITY	2018-08-14	0	N/A	0	MG/L
MERCURY	2018-08-14	0	2	1	UG/L
CIS-1,2-DICHLOROETHYLENE	2018-08-14	0	6	0.5	UG/L
STYRENE	2018-08-14	0	100	0.5	UG/L
O-XYLENE	2018-08-14	0	N/A	0.5	UG/L
1,1-DICHLOROPROPENE	2018-08-14	0	N/A	0.5	UG/L
2,2-DICHLOROPROPANE	2018-08-14	0	N/A	0.5	UG/L
1,3-DICHLOROPROPANE	2018-08-14	0	N/A	0.5	UG/L
1,2,4-TRIMETHYLBENZENE	2018-08-14	0	N/A	0.5	UG/L
ISOPROPYLBENZENE	2018-08-14	0	N/A	0.5	UG/L
N-PROPYLBENZENE	2018-08-14	0	N/A	0.5	UG/L
1,3,5-TRIMETHYLBENZENE	2018-08-14	0	N/A	0.5	UG/L
SEC-BUTYLBENZENE	2018-08-14	0	N/A	0.5	UG/L
TERT-BUTYLBENZENE	2018-08-14	0	N/A	0.5	UG/L
1,2,3-TRICHLOROPROPANE (1,2,3-TCP)	2018-08-14	0	0.005	0.005	UG/L
1,1,1,2-TETRACHLOROETHANE	2018-08-14	0	N/A	0.5	UG/L
DIBROMOMETHANE	2018-08-14	0	N/A	0.5	UG/L
1,2,3-TRICHLOROBENZENE	2018-08-14	0	N/A	0.5	UG/L
XYLENES (TOTAL)	2018-08-14	0	1750	0.5	UG/L
BROMOBENZENE	2018-08-14	0	N/A	0.5	UG/L
TRICHLOROTRIFLUOROETHANE (FREON 113)	2018-08-14	0	1200	10	UG/L
TURBIDITY, LABORATORY	2018-08-14	0.35	5	0.1	NTU
TOTAL TRIHALOMETHANES	2018-08-14	0	80	0	UG/L
2-CHLOROTOLUENE	2018-08-14	0	N/A	0.5	UG/L
4-CHLOROTOLUENE	2018-08-14	0	N/A	0.5	UG/L
N-BUTYLBENZENE	2018-08-14	0	N/A	0.5	UG/L
P-ISOPROPYLTOLUENE	2018-08-14	0	N/A	0	UG/L
BROMOCHLOROMETHANE	2018-08-14	0	N/A	0.5	UG/L
M,P-XYLENE	2018-08-14	0	N/A	0.5	UG/L
NITRATE + NITRITE (AS N)	2018-08-14	0	10	0.4	mg/L
ETHYL-TERT-BUTYL ETHER	2018-08-14	0	N/A	3	UG/L
TERT-AMYL-METHYL ETHER (TAME)	2018-08-14	0	N/A	3	UG/L
DIISOPROPYL ETHER	2018-08-14	0	N/A	3	UG/L
PERCHLORATE	2018-10-19	0	6	4	UG/L
ALKALINITY (TOTAL) AS CaCO3	2018-11-27	29.9	N/A	0	MG/L
BICARBONATE ALKALINITY	2018-11-27	36.5	N/A	0	MG/L
CARBONATE ALKALINITY	2018-11-27	0	N/A	0	MG/L
TOTAL ORGANIC CARBON (TOC)	2018-11-27	1.3	N/A	0.3	MG/L
HYDROXIDE ALKALINITY	2018-11-27	0	N/A	0	MG/L
1,2,3-TRICHLOROPROPANE (1,2,3-TCP)	2018-11-27	0	0.005	0.005	UG/L
ASBESTOS	2018-11-27	0	7	0.2	MFL
TOTAL ORGANIC CARBON (TOC)	2019-02-20	0.97	N/A	0.3	MG/L
TOTAL ORGANIC CARBON (TOC)	2019-05-16	1.1	N/A	0.3	MG/L
COLOR	2019-08-27	9	15	0	UNITS
ODOR THRESHOLD @ 60 C	2019-08-27	2	3	1	TON
SPECIFIC CONDUCTANCE	2019-08-27	38.60	1600	0	US
PH, LABORATORY	2019-08-27	6.94	N/A	0	
ALKALINITY (TOTAL) AS CaCO3	2019-08-27	17.3	N/A	0	MG/L
BICARBONATE ALKALINITY	2019-08-27	17.3	N/A	0	MG/L
CARBONATE ALKALINITY	2019-08-27	0	N/A	0	MG/L
NITRATE (AS N)	2019-08-27	0	10	0.4	mg/L
NITRITE (AS N)	2019-08-27	0	1	0.4	mg/L
TOTAL ORGANIC CARBON (TOC)	2019-08-27	1.1	N/A	0.3	MG/L
HARDNESS (TOTAL) AS CaCO3	2019-08-27	15.3	N/A	0	MG/L
CALCIUM	2019-08-27	4.37	N/A	0	MG/L
MAGNESIUM	2019-08-27	1.08	N/A	0	MG/L
SODIUM	2019-08-27	1.66	N/A	0	MG/L
CHLORIDE	2019-08-27	0.63	500	0	MG/L
SULFATE	2019-08-27	1.29	500	0.5	MG/L
FLUORIDE (F) (NATURAL-SOURCE)	2019-08-27	0	2	0.1	MG/L
ARSENIC	2019-08-27	0	10	2	UG/L
BARIUM	2019-08-27	0	1000	100	UG/L
BERYLLIUM	2019-08-27	0	4	1	UG/L
CADMIUM	2019-08-27	0	5	1	UG/L
CHROMIUM (TOTAL)	2019-08-27	0	50	10	UG/L
COPPER	2019-08-27	0	1000	50	UG/L
IRON	2019-08-27	0	300	100	UG/L
MANGANESE	2019-08-27	0	50	20	UG/L
THALLIUM	2019-08-27	0	2	1	UG/L
NICKEL	2019-08-27	0	100	10	UG/L
SILVER	2019-08-27	0	100	10	UG/L

ZINC	2019-08-27	0	5000	50	UG/L
ANTIMONY	2019-08-27	0	6	6	UG/L
ALUMINUM	2019-08-27	0	1000	50	UG/L
SELENIUM	2019-08-27	0	50	5	UG/L
BROMODICHLOROMETHANE (THM)	2019-08-27	0	N/A	1	UG/L
CARBON TETRACHLORIDE	2019-08-27	0	0.5	0.5	UG/L
BROMOFORM (THM)	2019-08-27	0	N/A	1	UG/L
DIBROMOCHLOROMETHANE (THM)	2019-08-27	0	N/A	1	UG/L
CHLOROFORM (THM)	2019-08-27	0	N/A	1	UG/L
TOLUENE	2019-08-27	0	150	0.5	UG/L
BENZENE	2019-08-27	0	1	0.5	UG/L
MONOCHLOROBENZENE	2019-08-27	0	70	0.5	UG/L
CHLOROETHANE	2019-08-27	0	N/A	0.5	UG/L
ETHYL BENZENE	2019-08-27	0	300	0.5	UG/L
HEXACHLOROBUTADIENE	2019-08-27	0	N/A	0.5	UG/L
BROMOMETHANE	2019-08-27	0	N/A	0.5	UG/L
CHLOROMETHANE	2019-08-27	0	N/A	0.5	UG/L
DICHLOROMETHANE	2019-08-27	0	5	0.5	UG/L
TETRACHLOROETHYLENE	2019-08-27	0	5	0.5	UG/L
TRICHLOROFLUOROMETHANE FREON 11	2019-08-27	0	150	5	UG/L
1,1-DICHLOROETHANE	2019-08-27	0	5	0.5	UG/L
1,1-DICHLOROETHYLENE	2019-08-27	0	6	0.5	UG/L
1,1,1-TRICHLOROETHANE	2019-08-27	0	200	0.5	UG/L
1,1,2-TRICHLOROETHANE	2019-08-27	0	5	0.5	UG/L
1,1,2,2-TETRACHLOROETHANE	2019-08-27	0	1	0.5	UG/L
1,2-DICHLOROETHANE	2019-08-27	0	0.5	0.5	UG/L
1,2-DICHLOROBENZENE	2019-08-27	0	600	0.5	UG/L
1,2-DICHLOROPROPANE	2019-08-27	0	5	0.5	UG/L
TRANS-1,2-DICHLOROETHYLENE	2019-08-27	0	10	0.5	UG/L
1,2,4-TRICHLOROBENZENE	2019-08-27	0	5	0.5	UG/L
1,3-DICHLOROPROPENE (TOTAL)	2019-08-27	0	0.5	0.5	UG/L
1,3-DICHLOROBENZENE	2019-08-27	0	N/A	0.5	UG/L
1,4-DICHLOROBENZENE	2019-08-27	0	5	0.5	UG/L
DICHLORODIFLUOROMETHANE (FREON 12)	2019-08-27	0	N/A	0.5	UG/L
NAPHTHALENE	2019-08-27	0	N/A	0.5	UG/L
TRANS-1,3-DICHLOROPROPENE	2019-08-27	0	0.5	0.5	UG/L
CIS-1,3-DICHLOROPROPENE	2019-08-27	0	0.5	0.5	UG/L
FOAMING AGENTS (MBAS)	2019-08-27	0	0.5	0	MG/L
VINYL CHLORIDE	2019-08-27	0	0.5	0.5	UG/L
TRICHLOROETHYLENE	2019-08-27	0	5	0.5	UG/L
METHYL-TERT-BUTYL-ETHER (MTBE)	2019-08-27	0	13	3	UG/L
TOTAL DISSOLVED SOLIDS	2019-08-27	51	1000	0	MG/L
HYDROXIDE ALKALINITY	2019-08-27	0	N/A	0	MG/L
MERCURY	2019-08-27	0	2	1	UG/L
CIS-1,2-DICHLOROETHYLENE	2019-08-27	0	6	0.5	UG/L
STYRENE	2019-08-27	0	100	0.5	UG/L
O-XYLENE	2019-08-27	0	N/A	0.5	UG/L
1,1-DICHLOROPROPENE	2019-08-27	0	N/A	0.5	UG/L
2,2-DICHLOROPROPANE	2019-08-27	0	N/A	0.5	UG/L
1,3-DICHLOROPROPANE	2019-08-27	0	N/A	0.5	UG/L
1,2,4-TRIMETHYLBENZENE	2019-08-27	0	N/A	0.5	UG/L
ISOPROPYLBENZENE	2019-08-27	0	N/A	0.5	UG/L
N-PROPYLBENZENE	2019-08-27	0	N/A	0.5	UG/L
1,3,5-TRIMETHYLBENZENE	2019-08-27	0	N/A	0.5	UG/L
SEC-BUTYLBENZENE	2019-08-27	0	N/A	0.5	UG/L
TERT-BUTYLBENZENE	2019-08-27	0	N/A	0.5	UG/L
1,1,1,2-TETRACHLOROETHANE	2019-08-27	0	N/A	0.5	UG/L
DIBROMOMETHANE	2019-08-27	0	N/A	0.5	UG/L
1,2,3-TRICHLOROBENZENE	2019-08-27	0	N/A	0.5	UG/L
GLYPHOSATE	2019-08-27	0	700	25	UG/L
XYLENES (TOTAL)	2019-08-27	0	1750	0.5	UG/L
BROMOBENZENE	2019-08-27	0	N/A	0.5	UG/L
TRICHLOROTRIFLUOROETHANE (FREON 113)	2019-08-27	0	1200	10	UG/L
TURBIDITY, LABORATORY	2019-08-27	0.75	5	0.1	NTU
TOTAL TRIHALOMETHANES	2019-08-27	0	80	0	UG/L
2-CHLOROTOLUENE	2019-08-27	0	N/A	0.5	UG/L
4-CHLOROTOLUENE	2019-08-27	0	N/A	0.5	UG/L
N-BUTYLBENZENE	2019-08-27	0	N/A	0.5	UG/L
P-ISOPROPYLTOLUENE	2019-08-27	0	N/A	0	UG/L
BROMOCHLOROMETHANE	2019-08-27	0	N/A	0.5	UG/L
M,P-XYLENE	2019-08-27	0	N/A	0.5	UG/L
PERCHLORATE	2019-08-27	0	6	4	UG/L
ETHYL-TERT-BUTYL ETHER	2019-08-27	0	N/A	3	UG/L
TERT-AMYL-METHYL ETHER (TAME)	2019-08-27	0	N/A	3	UG/L
DIISOPROPYL ETHER	2019-08-27	0	N/A	3	UG/L
DIQUAT	2019-09-12	0	20	4	UG/L
TOTAL ORGANIC CARBON (TOC)	2019-11-20	0.86	N/A	0.3	MG/L

American River Water Quality Results 2020					
Group/Constituent Identification	Sampling Date	Result	Maximum Contaminant Level (for drinking water purposes only)	Detection Limit for the Purposes of Reporting	Unit
TOTAL ORGANIC CARBON (TOC)	2020-02-19	0.61	0	0.3	MG/L
TOTAL ORGANIC CARBON (TOC)	2020-05-14	1.2	0	0.3	MG/L
TOTAL ORGANIC CARBON (TOC)	2020-08-12	1.1	0	0.3	MG/L
BROMODICHLOROMETHANE (THM)	2020-08-12	0	0	1	UG/L
CARBON TETRACHLORIDE	2020-08-12	0	0.5	0.5	UG/L
BROMOFORM (THM)	2020-08-12	0	0	1	UG/L
DIBROMOCHLOROMETHANE (THM)	2020-08-12	0	0	1	UG/L
CHLOROFORM (THM)	2020-08-12	0	0	1	UG/L
TOLUENE	2020-08-12	0	150	0.5	UG/L
BENZENE	2020-08-12	0	1	0.5	UG/L
MONOCHLOROBENZENE	2020-08-12	0	70	0.5	UG/L
CHLOROETHANE	2020-08-12	0	0	0.5	UG/L
ETHYL BENZENE	2020-08-12	0	300	0.5	UG/L
HEXACHLOROBUTADIENE	2020-08-12	0	0	0.5	UG/L
BROMOMETHANE	2020-08-12	0	0	0.5	UG/L
CHLOROMETHANE	2020-08-12	0	0	0.5	UG/L
DICHLOROMETHANE	2020-08-12	0	5	0.5	UG/L
TETRACHLOROETHYLENE	2020-08-12	0	5	0.5	UG/L
TRICHLOROFLUOROMETHANE FREON 11	2020-08-12	0	150	5	UG/L
1,1-DICHLOROETHANE	2020-08-12	0	5	0.5	UG/L
1,1-DICHLOROETHYLENE	2020-08-12	0	6	0.5	UG/L
1,1,1-TRICHLOROETHANE	2020-08-12	0	200	0.5	UG/L
1,1,2-TRICHLOROETHANE	2020-08-12	0	5	0.5	UG/L
1,1,2,2-TETRACHLOROETHANE	2020-08-12	0	1	0.5	UG/L
1,2-DICHLOROETHANE	2020-08-12	0	0.5	0.5	UG/L
1,2-DICHLOROBENZENE	2020-08-12	0	600	0.5	UG/L
1,2-DICHLOROPROPANE	2020-08-12	0	5	0.5	UG/L
TRANS-1,2-DICHLOROETHYLENE	2020-08-12	0	10	0.5	UG/L
1,2,4-TRICHLOROBENZENE	2020-08-12	0	5	0.5	UG/L
1,3-DICHLOROPROPENE (TOTAL)	2020-08-12	0	0.5	0.5	UG/L
1,3-DICHLOROBENZENE	2020-08-12	0	0	0.5	UG/L
1,4-DICHLOROBENZENE	2020-08-12	0	5	0.5	UG/L
DICHLORODIFLUOROMETHANE (FREON 12)	2020-08-12	0	0	0.5	UG/L
NAPHTHALENE	2020-08-12	0	0	0.5	UG/L
TRANS-1,3-DICHLOROPROPENE	2020-08-12	0	0.5	0.5	UG/L
CIS-1,3-DICHLOROPROPENE	2020-08-12	0	0.5	0.5	UG/L
VINYL CHLORIDE	2020-08-12	0	0.5	0.5	UG/L
TRICHLOROETHYLENE	2020-08-12	0	5	0.5	UG/L
METHYL-TERT-BUTYL-ETHER (MTBE)	2020-08-12	0	13	3	UG/L
CIS-1,2-DICHLOROETHYLENE	2020-08-12	0	6	0.5	UG/L
STYRENE	2020-08-12	0	100	0.5	UG/L
O-XYLENE	2020-08-12	0	0	0.5	UG/L
1,1-DICHLOROPROPENE	2020-08-12	0	0	0.5	UG/L
2,2-DICHLOROPROPANE	2020-08-12	0	0	0.5	UG/L
1,3-DICHLOROPROPANE	2020-08-12	0	0	0.5	UG/L
1,2,4-TRIMETHYLBENZENE	2020-08-12	0	0	0.5	UG/L
ISOPROPYLBENZENE	2020-08-12	0	0	0.5	UG/L
N-PROPYLBENZENE	2020-08-12	0	0	0.5	UG/L
1,3,5-TRIMETHYLBENZENE	2020-08-12	0	0	0.5	UG/L
SEC-BUTYLBENZENE	2020-08-12	0	0	0.5	UG/L
TERT-BUTYLBENZENE	2020-08-12	0	0	0.5	UG/L
1,1,1,2-TETRACHLOROETHANE	2020-08-12	0	0	0.5	UG/L
DIBROMOMETHANE	2020-08-12	0	0	0.5	UG/L
1,2,3-TRICHLOROBENZENE	2020-08-12	0	0	0.5	UG/L
XYLENES (TOTAL)	2020-08-12	0	1750	0.5	UG/L
BROMOBENZENE	2020-08-12	0	0	0.5	UG/L
TRICHLOROTRIFLUOROETHANE (FREON 113)	2020-08-12	0	1200	10	UG/L
TOTAL TRIHALOMETHANES	2020-08-12	0	80	0	UG/L
2-CHLOROTOLUENE	2020-08-12	0	0	0.5	UG/L
4-CHLOROTOLUENE	2020-08-12	0	0	0.5	UG/L
N-BUTYLBENZENE	2020-08-12	0	0	0.5	UG/L
P-ISOPROPYLTOLUENE	2020-08-12	0	0	0	UG/L
BROMOCHLOROMETHANE	2020-08-12	0	0	0.5	UG/L
M,P-XYLENE	2020-08-12	0	0	0.5	UG/L
PERCHLORATE	2020-08-12	0	6	4	UG/L
ETHYL-TERT-BUTYL ETHER	2020-08-12	0	0	3	UG/L
TERT-AMYL-METHYL ETHER (TAME)	2020-08-12	0	0	3	UG/L
DIISOPROPYL ETHER	2020-08-12	0	0	3	UG/L
TOTAL ORGANIC CARBON (TOC)	2020-11-10	0.98	0	0.3	MG/L

American River Water Qua

Analyte Name	Sampling Date	Result
CARBON, TOTAL	02-08-2022	0.75
CARBON, DISSOLVED ORGANIC (DOC)	02-08-2022	0.78
ALKALINITY, TOTAL	02-08-2022	30.80
CARBON, TOTAL	05-11-2022	1.00
CARBON, DISSOLVED ORGANIC (DOC)	05-11-2022	1.02
ALKALINITY, TOTAL	05-11-2022	24.00
FLUORIDE	08-10-2022	0
NITRITE	08-10-2022	0
NITRATE	08-10-2022	0
1,3-DICHLOROPROPENE	08-10-2022	0
VINYL CHLORIDE	08-10-2022	0
1,2-DICHLOROETHANE	08-10-2022	0
CARBON TETRACHLORIDE	08-10-2022	0
1,1,2,2-TETRACHLOROETHANE	08-10-2022	0
BENZENE	08-10-2022	0
1,2,4-TRICHLOROBENZENE	08-10-2022	0
DICHLOROMETHANE	08-10-2022	0
P-DICHLOROBENZENE	08-10-2022	0
1,1-DICHLOROETHANE	08-10-2022	0
1,2-DICHLOROPROPANE	08-10-2022	0
TRICHLOROETHYLENE	08-10-2022	0
1,1,2-TRICHLOROETHANE	08-10-2022	0
TETRACHLOROETHYLENE	08-10-2022	0
CIS-1,2-DICHLOROETHYLENE	08-10-2022	0
1,1-DICHLOROETHYLENE	08-10-2022	0
TRANS-1,2-DICHLOROETHYLENE	08-10-2022	0
CHLOROBENZENE	08-10-2022	0
STYRENE	08-10-2022	0
TOLUENE	08-10-2022	0
1,1,1-TRICHLOROETHANE	08-10-2022	0
ETHYLBENZENE	08-10-2022	0
O-DICHLOROBENZENE	08-10-2022	0
XYLENES, TOTAL	08-10-2022	0
XYLENE, META AND PARA	08-10-2022	0
O-XYLENE	08-10-2022	0
MERCURY	08-10-2022	0
THALLIUM, TOTAL	08-10-2022	0
BERYLLIUM, TOTAL	08-10-2022	0
CADMIUM	08-10-2022	0
PERCHLORATE	08-10-2022	0
ARSENIC	08-10-2022	0
METHYL TERT-BUTYL ETHER	08-10-2022	0
DIQUAT	08-10-2022	0

SELENIUM	08-10-2022	0
TRICHLOROFLUOROMETHANE	08-10-2022	0
ANTIMONY, TOTAL	08-10-2022	0
CHROMIUM	08-10-2022	0
NICKEL	08-10-2022	0
TRICHLOROTRIFLUOROETHANE	08-10-2022	0
GLYPHOSATE	08-10-2022	0
ALUMINUM	08-10-2022	0
COPPER, FREE	08-10-2022	0
BARIUM	08-10-2022	0
FOAMING AGENTS (SURFACTANTS)	08-10-2022	0
ODOR	08-10-2022	0
TURBIDITY	08-10-2022	0.50
COLOR	08-10-2022	0
MANGANESE	08-10-2022	0
SILVER	08-10-2022	0
IRON	08-10-2022	0
SULFATE	08-10-2022	1.1
CHLORIDE	08-10-2022	1.16
TDS	08-10-2022	6
CONDUCTIVITY @ 25 C UMHOS/CM	08-10-2022	42
ZINC	08-10-2022	0
MAGNESIUM	08-10-2022	1.04
CARBON, TOTAL	08-10-2022	1.31
CARBON, DISSOLVED ORGANIC (DOC)	08-10-2022	1.34
CALCIUM	08-10-2022	4.76
PH	08-10-2022	6.31
HARDNESS, TOTAL (AS CaCO3)	08-10-2022	16.2
ALKALINITY, TOTAL	08-10-2022	88
ALKALINITY, BICARBONATE	08-10-2022	88
HYDROXIDE AS CALCIUM CARBONATE	08-10-2022	0
SODIUM	08-10-2022	0
ALKALINITY, CARBONATE	08-10-2022	0
TRANS-1,3-DICHLOROPROPENE	08-10-2022	0
CIS-1,3-DICHLOROPROPENE	08-10-2022	0
CARBON, DISSOLVED ORGANIC (DOC)	11-09-2022	1.70
CARBON, TOTAL	11-09-2022	1.73
ALKALINITY, TOTAL	11-09-2022	41.1
ALKALINITY, BICARBONATE	11-09-2022	41.1
HYDROXIDE AS CALCIUM CARBONATE	11-09-2022	0
ALKALINITY, CARBONATE	11-09-2022	0
CARBON, DISSOLVED ORGANIC (DOC)	02-16-2023	1.47
CARBON, TOTAL	02-16-2023	1.9
ALKALINITY, TOTAL	02-16-2023	24.6
ALKALINITY, BICARBONATE	02-16-2023	24.6
HYDROXIDE AS CALCIUM CARBONATE	02-16-2023	0
ALKALINITY, CARBONATE	02-16-2023	0

CARBON, DISSOLVED ORGANIC (DOC)	05-10-2023	0.55
CARBON, TOTAL	05-10-2023	0.83
CARBON, TOTAL	06-07-2023	1.16
CARBON, DISSOLVED ORGANIC (DOC)	06-07-2023	1.79
FLUORIDE	08-17-2023	0
NITRITE	08-17-2023	0
NITRATE-NITRITE	08-17-2023	0
NITRATE	08-17-2023	0
1,3-DICHLOROPROPENE	08-17-2023	0
VINYL CHLORIDE	08-17-2023	0
1,2-DICHLOROETHANE	08-17-2023	0
CARBON TETRACHLORIDE	08-17-2023	0
1,1,2,2-TETRACHLOROETHANE	08-17-2023	0
BENZENE	08-17-2023	0
1,2,4-TRICHLOROBENZENE	08-17-2023	0
DICHLOROMETHANE	08-17-2023	0
P-DICHLOROBENZENE	08-17-2023	0
1,1-DICHLOROETHANE	08-17-2023	0
1,2-DICHLOROPROPANE	08-17-2023	0
TRICHLOROETHYLENE	08-17-2023	0
1,1,2-TRICHLOROETHANE	08-17-2023	0
TETRACHLOROETHYLENE	08-17-2023	0
CIS-1,2-DICHLOROETHYLENE	08-17-2023	0
1,1-DICHLOROETHYLENE	08-17-2023	0
TRANS-1,2-DICHLOROETHYLENE	08-17-2023	0
CHLOROBENZENE	08-17-2023	0
STYRENE	08-17-2023	0
TOLUENE	08-17-2023	0
1,1,1-TRICHLOROETHANE	08-17-2023	0
ETHYLBENZENE	08-17-2023	0
O-DICHLOROBENZENE	08-17-2023	0
XYLENES, TOTAL	08-17-2023	0
MERCURY	08-17-2023	0
THALLIUM, TOTAL	08-17-2023	0
BERYLLIUM, TOTAL	08-17-2023	0
CADMIUM	08-17-2023	0
RADIUM-228	08-17-2023	0
PERCHLORATE	08-17-2023	0
ARSENIC	08-17-2023	0
METHYL TERT-BUTYL ETHER	08-17-2023	0
GROSS ALPHA PARTICLE ACTIVITY	08-17-2023	0.477
SELENIUM	08-17-2023	0
TRICHLOROFLUOROMETHANE	08-17-2023	0
ANTIMONY, TOTAL	08-17-2023	0
CHROMIUM	08-17-2023	0
NICKEL	08-17-2023	0
TRICHLOROTRIFLUOROETHANE	08-17-2023	0

ALUMINUM	08-17-2023	0
COPPER, FREE	08-17-2023	0
CYANIDE	08-17-2023	0
BARIUM	08-17-2023	0
FOAMING AGENTS (SURFACTANTS)	08-17-2023	0
ODOR	08-17-2023	1.5
TURBIDITY	08-17-2023	0.35
COLOR	08-17-2023	10
MANGANESE	08-17-2023	0
TTHM	08-17-2023	0
SILVER	08-17-2023	0
IRON	08-17-2023	0
CHLORIDE	08-17-2023	0.71
SULFATE	08-17-2023	1.40
TDS	08-17-2023	0
CONDUCTIVITY @ 25 C UMHOS/CM	08-17-2023	44.6
ZINC	08-17-2023	0
CARBON, TOTAL	08-17-2023	0.71
CARBON, DISSOLVED ORGANIC (DOC)	08-17-2023	1.03
MAGNESIUM	08-17-2023	1.04
CALCIUM	08-17-2023	4.74
PH	08-17-2023	7.48
AGGRESSIVE INDEX	08-17-2023	9.94
HARDNESS, TOTAL (AS CaCO3)	08-17-2023	16.1
ALKALINITY, TOTAL	08-17-2023	17.9
ALKALINITY, BICARBONATE	08-17-2023	17.9
HYDROXIDE AS CALCIUM CARBONATE	08-17-2023	0
SODIUM	08-17-2023	0
ALKALINITY, CARBONATE	08-17-2023	0
TRANS-1,3-DICHLOROPROPENE	08-17-2023	0
CIS-1,3-DICHLOROPROPENE	08-17-2023	0
CARBON, TOTAL	11-08-2023	1.25
CARBON, DISSOLVED ORGANIC (DOC)	11-08-2023	1.93
ALKALINITY, TOTAL	11-08-2023	29.6
ALKALINITY, BICARBONATE	11-08-2023	29.6
HYDROXIDE AS CALCIUM CARBONATE	11-08-2023	0
ALKALINITY, CARBONATE	11-08-2023	0
ASBESTOS	12-13-2023	0
CARBON, TOTAL	02-20-2024	2.31
CARBON, DISSOLVED ORGANIC (DOC)	02-20-2024	2.55
ALKALINITY, TOTAL	02-20-2024	24.8
ALKALINITY, BICARBONATE	02-20-2024	24.8
HYDROXIDE AS CALCIUM CARBONATE	02-20-2024	0
ALKALINITY, CARBONATE	02-20-2024	0
ALKALINITY, TOTAL	05-15-2024	19
ALKALINITY, BICARBONATE	05-15-2024	19
HYDROXIDE AS CALCIUM CARBONATE	05-15-2024	0

ALKALINITY, CARBONATE	05-15-2024	0
1,2,3-TRICHLOROPROPANE	08-08-2024	0
2,3,7,8-TCDD	08-08-2024	0
HEPTACHLOR	08-08-2024	0
HEPTACHLOR EPOXIDE	08-08-2024	0
1,2-DIBROMO-3-CHLOROPROPANE	08-08-2024	0
ETHYLENE DIBROMIDE	08-08-2024	0
CHLORDANE	08-08-2024	0
BENZO(A)PYRENE	08-08-2024	0
FLUORIDE	08-08-2024	0.26
ENDRIN	08-08-2024	0
BHC-GAMMA	08-08-2024	0
PENTACHLOROPHENOL	08-08-2024	0
NITRITE	08-08-2024	0
NITRATE	08-08-2024	0
TOTAL POLYCHLORINATED BIPHENYLS (PCB)	08-08-2024	0
1,3-DICHLOROPROPENE	08-08-2024	0
VINYL CHLORIDE	08-08-2024	0
1,2-DICHLOROETHANE	08-08-2024	0
CARBON TETRACHLORIDE	08-08-2024	0
ATRAZINE	08-08-2024	0
HEXACHLOROBENZENE	08-08-2024	0
1,1,2-TETRACHLOROETHANE	08-08-2024	0
BENZENE	08-08-2024	0
1,2,4-TRICHLOROBENZENE	08-08-2024	0
DICHLOROMETHANE	08-08-2024	0
P-DICHLOROBENZENE	08-08-2024	0
1,1-DICHLOROETHANE	08-08-2024	0
1,2-DICHLOROPROPANE	08-08-2024	0
TRICHLOROETHYLENE	08-08-2024	0
1,1,2-TRICHLOROETHANE	08-08-2024	0
TETRACHLOROETHYLENE	08-08-2024	0
CIS-1,2-DICHLOROETHYLENE	08-08-2024	0
1,1-DICHLOROETHYLENE	08-08-2024	0
TRANS-1,2-DICHLOROETHYLENE	08-08-2024	0
CHLOROBENZENE	08-08-2024	0
STYRENE	08-08-2024	0
TOLUENE	08-08-2024	0
1,1,1-TRICHLOROETHANE	08-08-2024	0
ETHYLBENZENE	08-08-2024	0
O-DICHLOROBENZENE	08-08-2024	0
XYLENES, TOTAL	08-08-2024	0
AROCLOR 1016	08-08-2024	0
AROCLOR 1221	08-08-2024	0
AROCLOR 1232	08-08-2024	0
AROCLOR 1242	08-08-2024	0
AROCLOR 1248	08-08-2024	0

AROCOR 1254	08-08-2024	0
AROCOR 1260	08-08-2024	0
MERCURY	08-08-2024	0
THALLIUM, TOTAL	08-08-2024	0
LASSO	08-08-2024	0
LASSO	08-08-2024	0
TOXAPHENE	08-08-2024	0
BERYLLIUM, TOTAL	08-08-2024	0
SIMAZINE	08-08-2024	0
CADMIUM	08-08-2024	0
PERCHLORATE	08-08-2024	0
HEXACHLOROCYCLOPENTADIENE	08-08-2024	0
2,4,5-TP	08-08-2024	0
THIOBENCARB (BOLERO)	08-08-2024	0
PICLORAM	08-08-2024	0
DINOSEB	08-08-2024	0
ARSENIC	08-08-2024	0
BENTAZON	08-08-2024	0
MOLINATE	08-08-2024	0
DI(2-ETHYLHEXYL) PHTHALATE	08-08-2024	0
METHYL TERT-BUTYL ETHER	08-08-2024	0
DIQUAT	08-08-2024	0
CARBOFURAN	08-08-2024	0
SELENIUM	08-08-2024	0
TRICHLOROFLUOROMETHANE	08-08-2024	0
DI(2-ETHYLHEXYL) ADIPATE	08-08-2024	0
ANTIMONY, TOTAL	08-08-2024	0
METHOXYCHLOR	08-08-2024	0
CHROMIUM	08-08-2024	0
2,4-D	08-08-2024	0
NICKEL	08-08-2024	0
DALAPON	08-08-2024	0
TRICHLOROTRIFLUOROETHANE	08-08-2024	0
OXAMYL	08-08-2024	0
GLYPHOSATE	08-08-2024	0
ENDOTHALL	08-08-2024	0
ALUMINUM	08-08-2024	0
COPPER, FREE	08-08-2024	0
CYANIDE	08-08-2024	0
BARIUM	08-08-2024	0
FOAMING AGENTS (SURFACTANTS)	08-08-2024	0
ODOR	08-08-2024	0
TURBIDITY	08-08-2024	0
COLOR	08-08-2024	5
MANGANESE	08-08-2024	0
TTHM	08-08-2024	0
SILVER	08-08-2024	0

IRON	08-08-2024	0
CHLORIDE	08-08-2024	0.85
SULFATE	08-08-2024	1.48
TDS	08-08-2024	22
CONDUCTIVITY @ 25 C UMHOS/CM	08-08-2024	42.7
ZINC	08-08-2024	0
CARBON, DISSOLVED ORGANIC (DOC)	08-08-2024	0.57
MAGNESIUM	08-08-2024	1.06
CARBON, TOTAL	08-08-2024	1.44
SODIUM	08-08-2024	1.63
CALCIUM	08-08-2024	4.5
PH	08-08-2024	7.57
AGGRESSIVE INDEX	08-08-2024	9.06
HARDNESS, TOTAL (AS CaCO3)	08-08-2024	15.6
ALKALINITY, TOTAL	08-08-2024	17.6
ALKALINITY, BICARBONATE	08-08-2024	17.6
HYDROXIDE AS CALCIUM CARBONATE	08-08-2024	0
ALKALINITY, CARBONATE	08-08-2024	0
TRANS-1,3-DICHLOROPROPENE	08-08-2024	0
CIS-1,3-DICHLOROPROPENE	08-08-2024	0
CHROMIUM, HEX	11-12-2024	0
CARBON, TOTAL	11-12-2024	1.35
ALKALINITY, TOTAL	11-12-2024	26.5
ALKALINITY, BICARBONATE	11-12-2024	26.5
HYDROXIDE AS CALCIUM CARBONATE	11-12-2024	0
ALKALINITY, CARBONATE	11-12-2024	0
CARBON, DISSOLVED ORGANIC (DOC)	11-12-2024	0
ALKALINITY, TOTAL	02-19-2025	26.5
ALKALINITY, BICARBONATE	02-19-2025	26.5
HYDROXIDE AS CALCIUM CARBONATE	02-19-2025	0
ALKALINITY, CARBONATE	02-19-2025	0
CARBON, DISSOLVED ORGANIC (DOC)	05-13-2025	1.37
CARBON, TOTAL	05-13-2025	1.4
ALKALINITY, TOTAL	05-13-2025	20.4
ALKALINITY, BICARBONATE	05-13-2025	20.4
HYDROXIDE AS CALCIUM CARBONATE	05-13-2025	0
ALKALINITY, CARBONATE	05-13-2025	0
FLUORIDE	08-12-2025	0
CHROMIUM, HEX	08-12-2025	0
NITRITE	08-12-2025	0
NITRATE-NITRITE	08-12-2025	0
NITRATE	08-12-2025	0
1,3-DICHLOROPROPENE	08-12-2025	0
VINYL CHLORIDE	08-12-2025	0
1,2-DICHLOROETHANE	08-12-2025	0
CARBON TETRACHLORIDE	08-12-2025	0
1,1,2,2-TETRACHLOROETHANE	08-12-2025	0

BENZENE	08-12-2025	0
1,2,4-TRICHLOROBENZENE	08-12-2025	0
DICHLOROMETHANE	08-12-2025	0
P-DICHLOROBENZENE	08-12-2025	0
1,1-DICHLOROETHANE	08-12-2025	0
1,2-DICHLOROPROPANE	08-12-2025	0
TRICHLOROETHYLENE	08-12-2025	0
1,1,2-TRICHLOROETHANE	08-12-2025	0
TETRACHLOROETHYLENE	08-12-2025	0
CIS-1,2-DICHLOROETHYLENE	08-12-2025	0
1,1-DICHLOROETHYLENE	08-12-2025	0
TRANS-1,2-DICHLOROETHYLENE	08-12-2025	0
CHLOROBENZENE	08-12-2025	0
STYRENE	08-12-2025	0
TOLUENE	08-12-2025	0
1,1,1-TRICHLOROETHANE	08-12-2025	0
ETHYLBENZENE	08-12-2025	0
O-DICHLOROBENZENE	08-12-2025	0
XYLENES, TOTAL	08-12-2025	0
XYLENE, META AND PARA	08-12-2025	0
O-XYLENE	08-12-2025	0
MERCURY	08-12-2025	0
THALLIUM, TOTAL	08-12-2025	0
BERYLLIUM, TOTAL	08-12-2025	0
CADMIUM	08-12-2025	0
PERCHLORATE	08-12-2025	0
COMBINED URANIUM	08-12-2025	0
RADIUM-228	08-12-2025	0.208
RADIUM-226	08-12-2025	0
ARSENIC	08-12-2025	0
METHYL TERT-BUTYL ETHER	08-12-2025	0
GROSS ALPHA PARTICLE ACTIVITY	08-12-2025	1.71
SELENIUM	08-12-2025	0
TRICHLOROFLUOROMETHANE	08-12-2025	0
LEAD	08-12-2025	0
ANTIMONY, TOTAL	08-12-2025	0
CHROMIUM	08-12-2025	0
NICKEL	08-12-2025	0
TRICHLOROTRIFLUOROETHANE	08-12-2025	0
ALUMINUM	08-12-2025	0
COPPER, FREE	08-12-2025	0
CYANIDE	08-12-2025	0
BARIUM	08-12-2025	0
FOAMING AGENTS (SURFACTANTS)	08-12-2025	0
ODOR	08-12-2025	1.5
TURBIDITY	08-12-2025	0
COMBINED RADIUM (-226 & -228)	08-12-2025	0

COLOR	08-12-2025	9
MANGANESE	08-12-2025	0
SILVER	08-12-2025	0
IRON	08-12-2025	0
CHLORIDE	08-12-2025	1.01
SULFATE	08-12-2025	1.69
TDS	08-12-2025	26
CONDUCTIVITY @ 25 C UMHOS/CM	08-12-2025	45.5
ZINC	08-12-2025	0
MAGNESIUM	08-12-2025	1.20
CARBON, TOTAL	08-12-2025	1.53
SODIUM	08-12-2025	1.99
CALCIUM	08-12-2025	5.10
PH	08-12-2025	8.03
AGGRESSIVE INDEX	08-12-2025	9.63
HARDNESS, TOTAL (AS CaCO3)	08-12-2025	17.7
ALKALINITY, TOTAL	08-12-2025	19
ALKALINITY, BICARBONATE	08-12-2025	19
HYDROXIDE AS CALCIUM CARBONATE	08-12-2025	0
ALKALINITY, CARBONATE	08-12-2025	0
TRANS-1,3-DICHLOROPROPENE	08-12-2025	0
CIS-1,3-DICHLOROPROPENE	08-12-2025	0
ALKALINITY, TOTAL	11-17-2025	35.8
ALKALINITY, BICARBONATE	11-17-2025	35.8
HYDROXIDE AS CALCIUM CARBONATE	11-17-2025	0
ALKALINITY, CARBONATE	11-17-2025	0
CARBON, TOTAL	02-18-2026	2.54
CARBON, DISSOLVED ORGANIC (DOC)	02-18-2026	2.9
PH, FIELD	02-18-2026	7.00
ALKALINITY, TOTAL	02-18-2026	35.4
ALKALINITY, BICARBONATE	02-18-2026	35.4
HYDROXIDE AS CALCIUM CARBONATE	02-18-2026	0
ALKALINITY, CARBONATE	02-18-2026	0
PERFLUOROBUTANE SULFONIC ACID (PFBS)	02-19-2026	0
PERFLUOROHEPTANOIC ACID (PFHPA)	02-19-2026	0
PERFLUOROHXANE SULFONIC ACID (PFHxS)	02-19-2026	0
PERFLUORONONANOIC ACID (PFNA)	02-19-2026	0
PERFLUOROOCTANE SULFONIC ACID (PFOS)	02-19-2026	0
PERFLUOROOCTANOIC ACID (PFOA)	02-19-2026	0
PERFLUORODECANOIC ACID (PFDA)	02-19-2026	0
PERFLUORODODECANOIC ACID (PFDOA)	02-19-2026	0
PERFLUOROHXANOIC ACID (PFHXA)	02-19-2026	0
PERFLUOROTETRADECANOIC ACID (PFTA)	02-19-2026	0
PERFLUOROTRIDECANOIC ACID (PFTRDA)	02-19-2026	0
PERFLUOROUNDECANOIC ACID (PFUNA)	02-19-2026	0
11CL-PF3OUDS	02-19-2026	0
9CL-PF3ONS	02-19-2026	0

ADONA	02-19-2026	0
HFPO-DA	02-19-2026	0
NETFOSAA	02-19-2026	0
NMEFOSAA	02-19-2026	0

lity Results 2022-2026

Maximum Contaminant Level (for
drinking water purposes only)

Detection Limit for the Purposes of Reporting

Unit

N/A	N/A	MG/L
N/A	N/A	MG/L
N/A	N/A	MG/L
N/A	N/A	MG/L
N/A	N/A	MG/L
N/A	N/A	MG/L
2	.1	MG/L
1	.4	MG/L
10	.4	MG/L
.5	.5	UG/L
.5	.5	UG/L
.5	.5	UG/L
.5	.5	UG/L
1	.5	UG/L
1	.5	UG/L
5	.5	UG/L
5	.5	UG/L
5	.5	UG/L
5	.5	UG/L
5	.5	UG/L
5	.5	UG/L
5	.5	UG/L
5	.5	UG/L
6	.5	UG/L
6	.5	UG/L
10	.5	UG/L
70	.5	UG/L
100	.5	UG/L
150	.5	UG/L
200	.5	UG/L
300	.5	UG/L
600	.5	UG/L
1750	0.5	UG/L
N/A	.5	UG/L
N/A	.5	UG/L
2	1	UG/L
2	1	UG/L
4	1	UG/L
5	1	UG/L
6	2	UG/L
10	2	UG/L
13	3	UG/L
20	4	UG/L

[illegible]

N/A	N/A	MG/L
N/A	N/A	MG/L
N/A	N/A	MG/L
N/A	N/A	MG/L
2	.1	MG/L
1	.4	MG/L
10	.4	MG/L
10	.4	MG/L
.5	.5	UG/L
.5	.5	UG/L
.5	.5	UG/L
.5	.5	UG/L
1	.5	UG/L
1	.5	UG/L
5	.5	UG/L
5	.5	UG/L
5	.5	UG/L
5	.5	UG/L
5	.5	UG/L
5	.5	UG/L
5	.5	UG/L
5	.5	UG/L
6	.5	UG/L
6	.5	UG/L
10	.5	UG/L
70	.5	UG/L
100	.5	UG/L
150	.5	UG/L
200	.5	UG/L
300	.5	UG/L
600	.5	UG/L
1750	0.5	UG/L
2	1	UG/L
2	1	UG/L
4	1	UG/L
5	1	UG/L
N/A	1	PCI/L
6	2	UG/L
10	2	UG/L
13	3	UG/L
15	3	PCI/L
50	5	UG/L
150	5	UG/L
6	6	UG/L
50	10	UG/L
100	10	UG/L
1200	10	UG/L

[illegible]

N/A	N/A	MG/L
0.005	0.005	UG/L
0.03	0.005	NG/L
.01	.01	UG/L
.01	.01	UG/L
.2	.01	UG/L
.05	.02	UG/L
.1	.1	UG/L
.2	.1	UG/L
2	.1	MG/L
2	.1	UG/L
.2	.2	UG/L
1	.2	UG/L
1	.4	MG/L
10	.4	MG/L
.5	.5	UG/L
.5	.5	UG/L
.5	.5	UG/L
.5	.5	UG/L
.5	.5	UG/L
1	.5	UG/L
1	.5	UG/L
1	.5	UG/L
1	.5	UG/L
5	.5	UG/L
5	.5	UG/L
5	.5	UG/L
5	.5	UG/L
5	.5	UG/L
5	.5	UG/L
5	.5	UG/L
5	.5	UG/L
5	.5	UG/L
6	.5	UG/L
6	.5	UG/L
10	.5	UG/L
70	.5	UG/L
100	.5	UG/L
150	.5	UG/L
200	.5	UG/L
300	.5	UG/L
600	.5	UG/L
1750	0.5	UG/L
N/A	.5	UG/L
N/A	.5	UG/L
N/A	.5	UG/L
N/A	.5	UG/L
N/A	.5	UG/L

N/A	.5	UG/L
N/A	.5	UG/L
2	1	UG/L
2	1	UG/L
2	1	UG/L
2	1	UG/L
3	1	UG/L
4	1	UG/L
4	1	UG/L
5	1	UG/L
6	1	UG/L
50	1	UG/L
50	1	UG/L
70	1	UG/L
500	1	UG/L
7	2	UG/L
10	2	UG/L
18	2	UG/L
20	2	UG/L
4	3	UG/L
13	3	UG/L
20	4	UG/L
18	5	UG/L
50	5	UG/L
150	5	UG/L
400	5	UG/L
6	6	UG/L
30	10	UG/L
50	10	UG/L
70	10	UG/L
100	10	UG/L
200	10	UG/L
1200	10	UG/L
50	20	UG/L
700	25	UG/L
100	45	UG/L
1000	50	UG/L
1000	50	UG/L
150	100	UG/L
1000	100	UG/L
.5	N/A	MG/L
3	N/A	TON
5	N/A	NTU
15	N/A	UNITS
50	N/A	UG/L
80	N/A	UG/L
100	N/A	UG/L

300	N/A	UG/L
500	N/A	MG/L
500	N/A	MG/L
1000	N/A	MG/L
1600	N/A	UMHO/CM
5000	N/A	UG/L
N/A	N/A	MG/L
N/A	N/A	MG/L
N/A	N/A	MG/L
N/A	N/A	MG/L
N/A	N/A	MG/L
N/A	N/A	pH
N/A	N/A	AGGR
N/A	N/A	MG/L
N/A	N/A	MG/L
N/A	N/A	MG/L
N/A	N/A	MG/L
N/A	N/A	MG/L
N/A	N/A	UG/L
N/A	N/A	UG/L
10	.1	UG/L
N/A	N/A	MG/L
N/A	N/A	MG/L
N/A	N/A	MG/L
N/A	N/A	MG/L
N/A	N/A	MG/L
N/A	N/A	MG/L
N/A	N/A	MG/L
N/A	N/A	MG/L
N/A	N/A	MG/L
N/A	N/A	MG/L
N/A	N/A	MG/L
N/A	N/A	MG/L
N/A	N/A	MG/L
N/A	N/A	MG/L
N/A	N/A	MG/L
N/A	N/A	MG/L
N/A	N/A	MG/L
2	.1	MG/L
10	.1	UG/L
1	.4	MG/L
10	.4	MG/L
10	.4	MG/L
.5	.5	UG/L
.5	.5	UG/L
.5	.5	UG/L
.5	.5	UG/L
1	.5	UG/L

1	.5	UG/L
5	.5	UG/L
5	.5	UG/L
5	.5	UG/L
5	.5	UG/L
5	.5	UG/L
5	.5	UG/L
5	.5	UG/L
5	.5	UG/L
6	.5	UG/L
6	.5	UG/L
10	.5	UG/L
70	.5	UG/L
100	.5	UG/L
150	.5	UG/L
200	.5	UG/L
300	.5	UG/L
600	.5	UG/L
1750	0.5	UG/L
N/A	.5	UG/L
N/A	.5	UG/L
2	1	UG/L
2	1	UG/L
4	1	UG/L
5	1	UG/L
6	1	UG/L
20	1	PCI/L
N/A	1	PCI/L
N/A	1	PCI/L
10	2	UG/L
13	3	UG/L
15	3	PCI/L
50	5	UG/L
150	5	UG/L
N/A	5	UG/L
6	6	UG/L
50	10	UG/L
100	10	UG/L
1200	10	UG/L
1000	50	UG/L
1000	50	UG/L
150	100	UG/L
1000	100	UG/L
.5	N/A	MG/L
3	N/A	TON
5	N/A	NTU
5	N/A	PCI/L

[illegible]

N/A
N/A
N/A
N/A

N/A
N/A
N/A
N/A

NG/L
NG/L
NG/L
NG/L

Attachment G

Environmental Effects of PCWA's 2026 Water Transfer on Folsom Reservoir and the Lower American River

Placer County Water Agency

June 2026

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List of Acronyms

TAF	Thousand acre-feet
ATSP	Automated Temperature Selection Procedure
cfs	cubic feet per second
CISO	California Independent System Operator
CVP	Central Valley Project
F	Fahrenheit
C	Celsius
MET	Meteorological
MFP	Middle Fork American River Project
PCWA	Placer County Water Agency
Reclamation	U.S. Bureau of Reclamation
WWD	Westlands Water District

1.0 SUMMARY

The proposed 2026 Placer County Water Agency (PCWA) temporary water transfer to Westlands Water District (WWD) would provide WWD with 20,000 acre-feet (AF) of water in a year when there is a shortage of agricultural water supply (25% Central Valley Project agriculture allocation), while providing 20,000 AF of additional cold water to Folsom Reservoir and the Lower American River that will enhance instream flows, maintain water temperatures, and provide benefits to fish, wildlife, recreation, and other instream beneficial uses. PCWA would release 21,053 acre-feet (AF)¹ of previously stored water from Middle Fork American River Project (MFP) reservoirs that would not otherwise be released from storage in 2026 to provide the 20,000 AF transfer water (5% conveyance loss).

Transfer water will be released from MFP reservoirs into Folsom Reservoir between approximately July and September, depending on the Water Board approval date (we modeled August–September), and subsequently released from Folsom Reservoir between September and October. For the July–September period, North Fork American River inflow to Folsom Reservoir would increase 15% as a result of the Transfer. Detailed water temperature modeling indicates the Transfer will decrease water temperatures in the North Fork American River by an average of 1.6°F during the transfer period. Additionally, the Transfer will increase the volume of cold water available in the metalimnion in Folsom Reservoir for release into the American River, increase flows in the American River by approximately 165 cfs, and, overall, maintain or slightly reduce water temperature in the lower American River at the Hazel Avenue and Watt Avenue water temperature compliance locations.

In summary, the Transfer would provide the following beneficial effects:

- Increase water supply for agricultural and environmental purposes
- Increase flows in the Lower American River;
- Slightly decrease or maintain water temperatures in the Lower American River; and
- Provide additional ancillary benefits, including increased hydropower generation/grid regulation capacity, and potential enhancement of Middle Fork American River whitewater rafting opportunities.

2.0 INTRODUCTION

The 2026 Transfer to WWD is consistent with other PCWA temporary water transfers from the MFP conducted over the past 30 years (Table 1; Appendix G1). These transfers release water from MFP storage that would not otherwise be released, thereby increasing the availability of water both for environmental and water supply purposes. The Transfer is consistent with the Reclamation and San

¹ PCWA will release 21,053 AF of previously stored MFP water for delivery which accounts for a 5% loss factor asserted from Oxbow Powerhouse (Point of Delivery) to Folsom Reservoir; this results in 20,000 AF of transfer water being made available to WWD out of Folsom Reservoir.

Luis & Delta-Mendota Water Authority 2026-2027 North to South Water Transfers Environmental Impact Report/Environmental Impact Statement (2025) that addresses the environmental effects of July – September PCWA transfers.

PCWA holds consumptive rights for the MFP water under Water Right Permits 13856 and 13858 issued by the State Water Rights Board (predecessor to the current State Water Resources Control Board or State Water Board) on January 10, 1963 (State Water Rights Board Decision D-1104). For the purposes of the transfer, PCWA will exercise Water Right Permit 13856 and will also commit to refill terms to ensure non-injury to downstream legal water users. Historically, depending on the terms of the agreement, the water released from the MFP reservoirs for transfer has only been refilled during subsequent wetter seasons/years when Folsom Reservoir was full or releasing water for flood control and the Delta is in excess conditions.

The 2026 transfer water will be released from PCWA’s MFP storage reservoirs by reducing the normal carryover storage of the MFP reservoirs for this year (approximately 160,000 AF) (i.e., releasing water that otherwise would remain in storage). The transfer water will be released from the cold-water pool of Hell Hole Reservoir and conveyed through 20 miles of tunnels to Middle Fork Interbay and Ralston Afterbay, where it enters the Middle Fork American River downstream of Oxbow Powerhouse (about 24 miles upstream of Folsom Reservoir) (Figure 1). Water released through Oxbow Powerhouse is characteristically cold (typically 40-55°F) upon entering the Middle Fork American River. These cold-water releases, combined with the increased volume of water released due to the transfer, result in reduced water temperatures in both the Middle Fork and North Fork American rivers, as well as in Folsom Reservoir inflow (approximately 65°F). This colder inflow passes through the reservoir’s cold-water metalimnion (approximately 65°F) and is conveyed to the Folsom Dam power penstock shutters for release into the Lower American River. The resulting increase in flows in the Lower American River (due to the addition of transfer water) slightly decreases the rate of downstream warming and provides habitat benefits for anadromous salmonids, particularly over-summering steelhead.

This technical memorandum describes the effects of transferring water from PCWA’s MFP in 2026 for use by WWD downstream of the confluence of the Lower American and Sacramento rivers. The memorandum analyzes the effects of the transfer on North Fork American River inflow hydrology and water temperature into Folsom Reservoir; Folsom Reservoir storage and water temperature; and Lower American River hydrology and water temperature. It also discusses additional effects of the transfer, including increased hydropower generation, improved CAISO grid regulation, and increased whitewater rafting opportunities.

**Attachment G: Water Temperature Effects of PCWA
Water Transfer on Folsom Reservoir
and the Lower American River**

Table 1. PCWA Historical Drier Year Water Transfers (1990-2026).

Calendar Year	Water Transfer (ac-ft)	Monthly Release Amounts (ac-ft)													Transfer Recipient
		Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Total Release ¹ (ac-ft)	
1990	38,597												38,597	38,597	Westlands Water District, San Luis, San Francisco
1991	40,000												40,000	40,000	San Francisco, Santa Clara
1992	10,000												10,000	10,000	State Water Bank
1993															
1994	20,000												20,000	20,000	State Water Bank
1995														0	
1996														0	
1997	12,000							17,000	18,000					12,000	Sac Area Flood Control
1998														0	
1999														0	
2000														0	
2001	20,000									21,800	400			22,200	Environmental Water Account
2002														0	
2003														0	
2004	18,700									7,900	7,900	2,900		18,700	Environmental Water Account
2005														0	
2006														0	
2007														0	
2008	20,000									29	8,139	139	21,268	29,575	Westlands Water District
2009	20,000								5,209	15,415				20,624	San Diego
2010														0	
2011														0	
2012														0	
2013	20,000					20,000								20,000	Westlands Water District (WWD)
2014	40,000				5,000			10,745	12,155	12,100					East Bay Municipal District & WWD
2015	12,000							2,840	6,916	2,244					East Bay Municipal District
2016															
2017															
2018															
2019															
2020	19,000 ¹								9,669	9,331					Westlands Water District
2021	20,000 ¹								8,178	11,823					Westlands Water District
2022	20,000 ¹							1,493	11,224	7,283					East Bay Municipal District
2023															
2024															
2025															
Proposed 2026 ²	20,000 ¹								10,000	10,000					Westlands Water District

¹ In these years release volumes were greater than the transfer amount to account for .

² The 2026 proposed transfer. Actual timing of the transfer was slightly different.

**Attachment G: Water Temperature Effects of PCWA
Water Transfer on Folsom Reservoir
and the Lower American River**

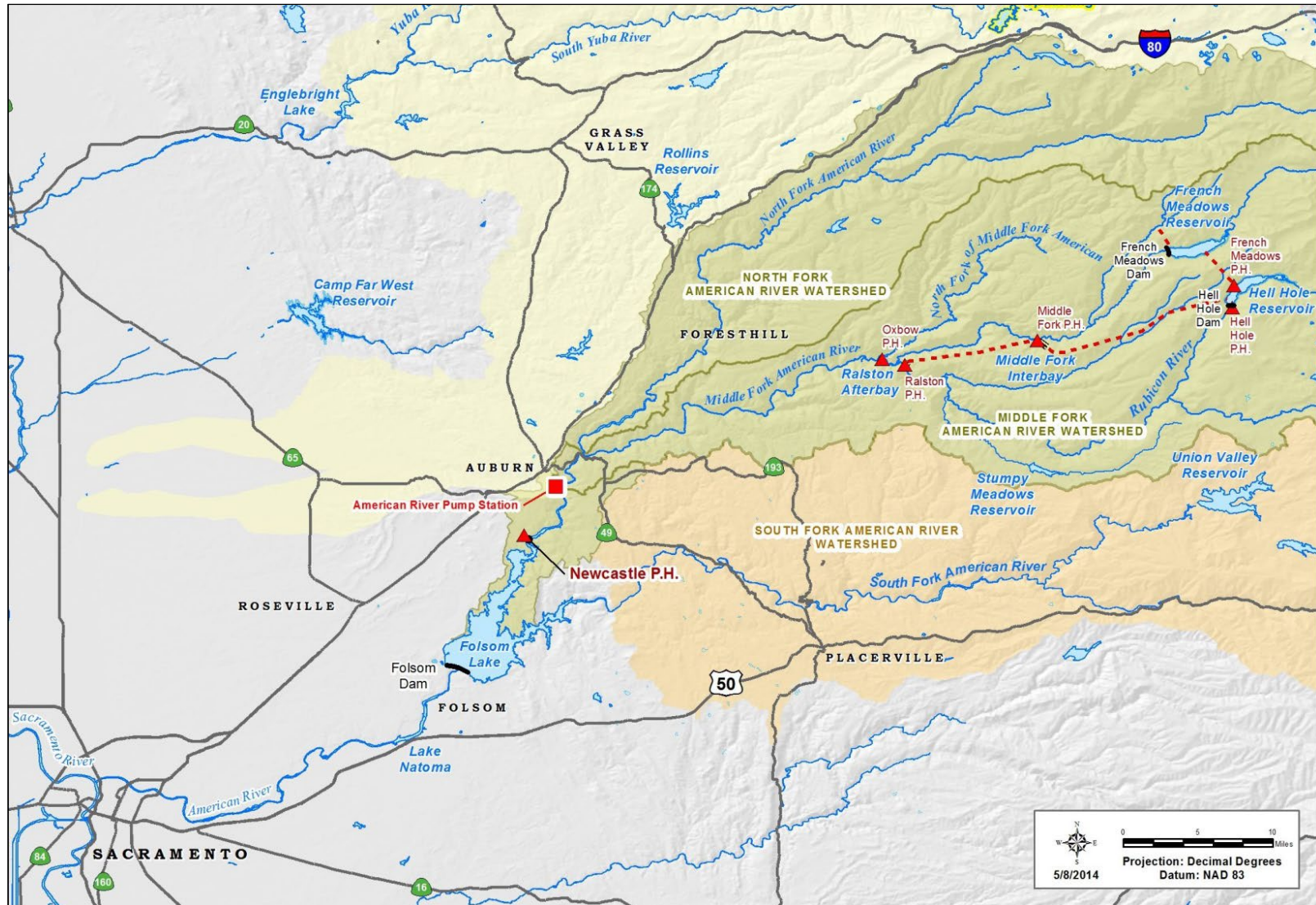


Figure 1. PCWA Middle Fork American River Project, Folsom Reservoir, and Lower American River.

3.0 WATER TRANSFER HYDROLOGY

3.1. Transfer Schedule

The modeled transfer schedule in Table 2 represents the approximate 2026 transfer inflow into and out of Folsom reservoir (August through September). The 2026 transfer water will pass through Folsom Reservoir (stored <30 days) and will be released as transfer water to WWD. The release of transfer water from Folsom Reservoir will occur on top of Reclamation’s forecasted operations (see Section 3.3 Reclamation Operations and Forecast). Following release of the transfer water by Reclamation, the water will enter the Sacramento River at the confluence of the Lower American River and then be delivered to WWD (e.g., Jones pumping plant in the south Delta).

Table 2. Representative Flow Schedule for PCWA’s 2026 MFP Water Transfer Releases into and out of Folsom Reservoir.

Representative Transfer Schedules	Releases into Folsom Reservoir (AF)			Releases from Folsom Reservoir (AF)
	Jul 15 - 31	Aug	Sep	Sep – Oct
Scenario 1	--	10,699	10,354	20,000

3.2. PCWA Operations and Forecast (Folsom Reservoir Inflow)

North Fork American River forecast inflows to Folsom Reservoir with and without the transfer are shown in Table 3. PCWA used their OASIS operations forecast model of the MFP and North Fork American River to project operations. The model is used looking forward with forecasted inflows from the National Weather Service’s California-Nevada River Forecasting Center (CNRFC). For the August–September period, North Fork American River inflow to Folsom Reservoir would increase 15% with the 20 TAF transfer.

Table 3. With and Without Transfers Forecasted PCWA Operations of the MFP¹ at the North Fork American River below the American River Pump Stations (bold text shows changes from baseline) (90 percentile forecast).

River / Scenario	Month (Acre-feet)						
	JUN	JUL	AUG	SEP	OCT	NOV	DEC
North Fork American River Below ARPS¹ Operations Scenario							
Baseline Without Transfer	50,828	63,686	43,370	31,391	7,920	19,481	70,646
With Transfer	50,828	63,686	54,069	41,745	7,920	19,481	70,646

¹ ARPS is American River Pump Station

3.3. Reclamation Operations and Forecast (Folsom Reservoir Storage and Outflow)

The Reclamation May 90 percentile forecast for Folsom Reservoir inflow and outflow operations without and with the PCWA transfer is shown in Table 4 and Figure 2.

Table 4. With and Without Transfers Reclamation Forecasted Folsom Reservoir Inflow and Outflow Operations (Reclamations May 90 Percentile Forecast) (bold text shows changes from baseline).

River / Scenario	Month (Acre-feet)						
	JUN	JUL	AUG	SEP	OCT	NOV	DEC
North Fork American River Below ARPS¹ Operations Scenario							
Baseline Without Transfer	43,846	36,763	37,853	35,081	19,422	26,977	36,585
With Transfer	43,846	36,763	48,552	45,435	19,422	26,977	36,585
South Fork American River							
With and Without Transfer	45,589	38,744	42,731	35,790	30,582	23,026	23,418
Total Folsom Reservoir Inflow							
Baseline Without Transfer	89,435	75,507	80,584	70,872	50,003	50,003	60,003
With Transfer	89,430	75,502	80,579	80,867	60,000	50,000	60,000

¹ ARPS is American River Pump Station

3.1. Middle Fork American River Project Refill

In order to refill MFP reservoirs following the release of the transfer water without injury to downstream water right holders, PCWA will limit the refill of its MFP reservoirs to times when the Delta is in excess and Folsom is releasing excess water for storage management or flood control. The refill restrictions will minimize the potential for refill of MFP reservoirs to affect Folsom Reservoir annual storage after a transfer. PCWA has a typical end-of-the-year (December-February) combined carryover target (storage low point) of 160,000 AF in its MFP reservoirs (French Meadows and Hell Hole). PCWA will carry an approximately 20,000 AF deficit in its carryover storage forward in time until conditions allow PCWA to relieve the deficit in MFP reservoirs (e.g., Folsom Reservoir fills/reaches flood control levels) without injury to downstream water right holders.

3.1. Westlands Water District Water Supply

WWD will receive transfer water in a year of reduced water availability. WWD provides water supply to over 600,000 acres of farmland within Fresno and Kings counties. WWD's long-term source of water supply is the Central Valley Project (CVP) operated by Reclamation. Reclamation's allocation to Westlands Water District this year is 25% of its annual contract amount. As a result, transfers are necessary to help protect high-value agricultural production on these farmlands.

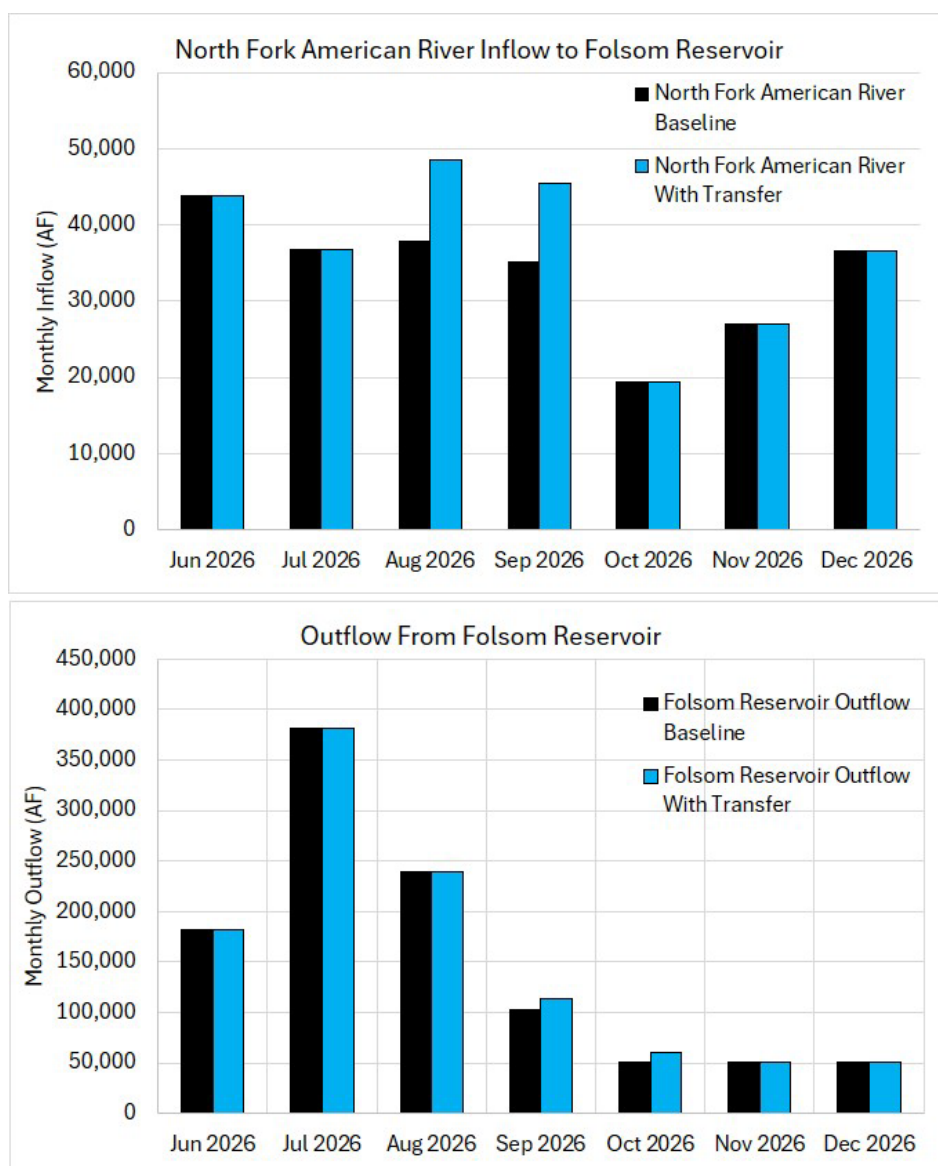


Figure 2. Modeled Folsom Reservoir Inflows (top) and Outflows (bottom) with and without Transfer (based on Reclamation May 90 Percentile Forecast).

4.0 MODELING OVERVIEW

Summer water temperatures in the North Fork American River decrease with increased flow releases from upstream hydropower facilities/deep water reservoirs (Figure 1). The water temperature of the transfer water through Oxbow Powerhouse is cold (typically 40-55°F) when it enters the Middle Fork American River (Figure 3). These cold-water releases result in reduced water temperature in both the Middle Fork and North Fork American rivers, as well as Folsom Reservoir inflow (approximately 65°F to 68°F) (Figure 4a and 4b). The colder Folsom Reservoir inflow travels across the cold-water

metalimnion of the reservoir (approximately 65°F) and provides additional cold water to blend with colder hypolimnion water at the Folsom Dam power penstock shutters to improve temperature release conditions into the Lower American River (Figure 5). The resulting increased flows in the Lower American River (due to the addition of transfer water) also slows the rate of downstream warming, providing additional habitat benefits for anadromous salmonids, including cooler in-river water temperatures (Figure 5).

5.0 INFLOW WATER TEMPERATURE TO FOLSOM RESERVOIR

Inflow water temperatures into Folsom Reservoir were modeled using multivariate regression water temperature models using 25 years of real data that include a wide range of inflow/climate conditions (Appendix G1). The regression models accurately predict inflow water temperature based on flow, air temperature, and time of year (the time of year implicitly accounts for solar radiation) (Appendix G2). Meteorological (MET) data from 2014, a year representative of warm meteorological conditions (Figure 7) was used for the modeling along with data from three other representative years (2011, 2017, and 2020).

5.1. North Fork American River

The water temperature decrease for the 2014 MET data transfer scenario in the North Fork American River, just upstream of Folsom Reservoir, is shown in Figure 8. The temperature decrease averaged 1.6°F. The Folsom Reservoir inflow temperature decrease occurs due to the increased flow from the upstream cold-water reservoirs.

5.2. South Fork American River

South Fork American River inflow water temperature to Folsom Reservoir is unaffected by PCWA transfers. The method used to estimate South Fork American River inflow temperatures is described in Appendix G1. Appendix G2 illustrates the accuracy of the temperature modeling based on the 2014 measured inflow water temperature data.

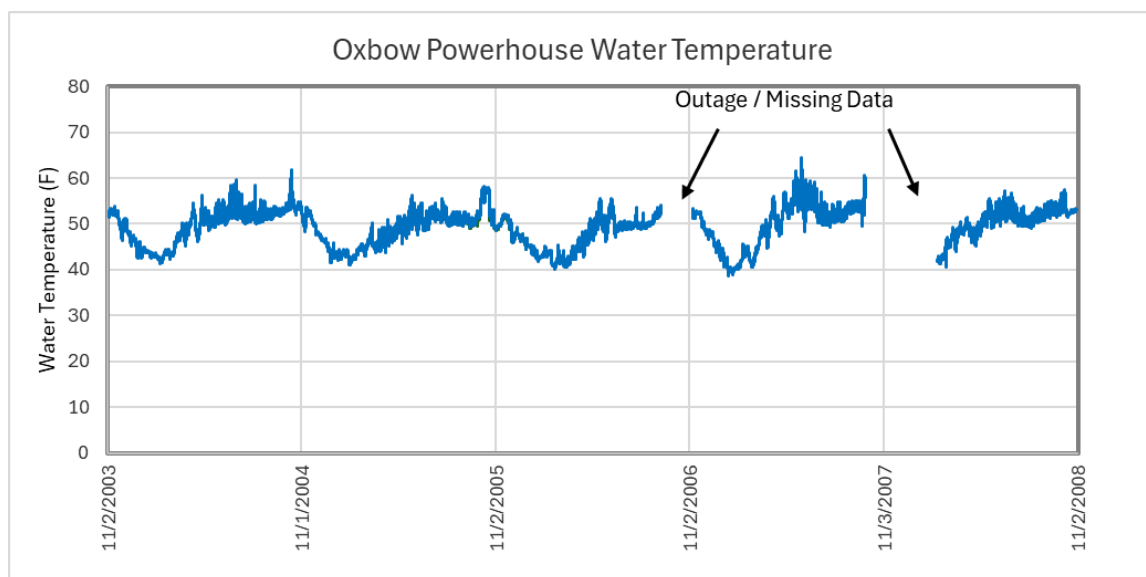


Figure 3. Cold-water releases from Oxbow Powerhouse.

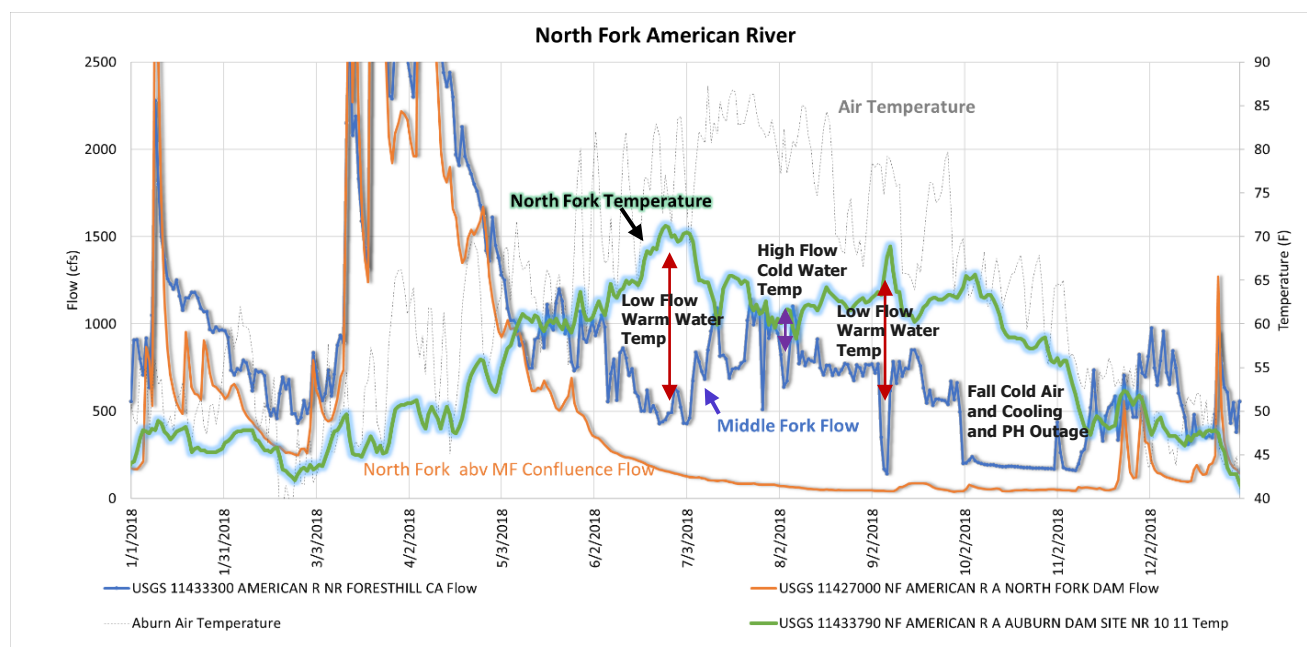


Figure 4a. Effects of increased Middle Fork American River summer inflows, where increased flow decreases the inflow water temperature and decreased flow increases the inflow water temperature.

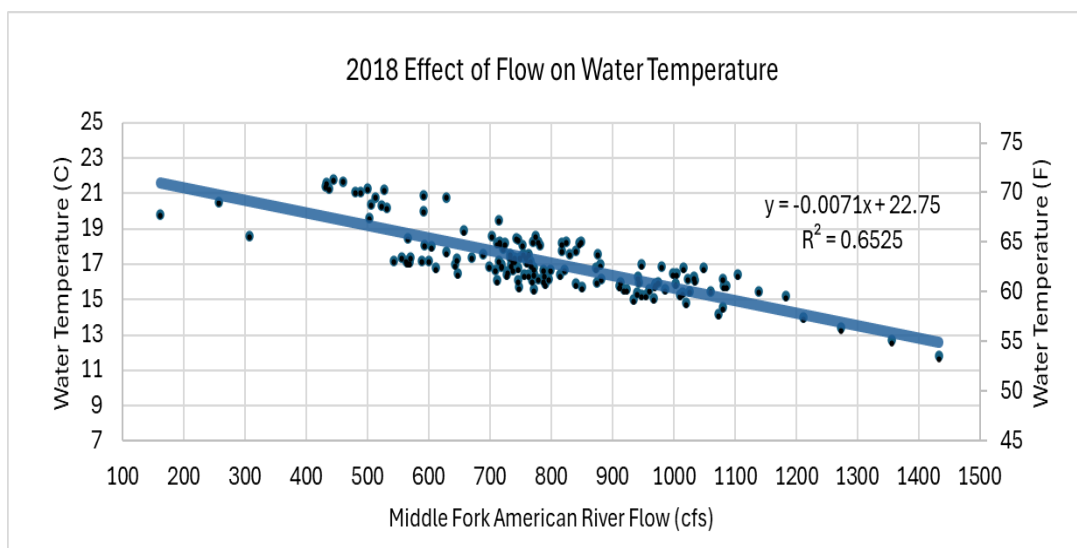


Figure 4a. Effects of increased Middle Fork American River summer inflows, where increased flow decreases the inflow water temperature and decreased flow increases the inflow water temperature.

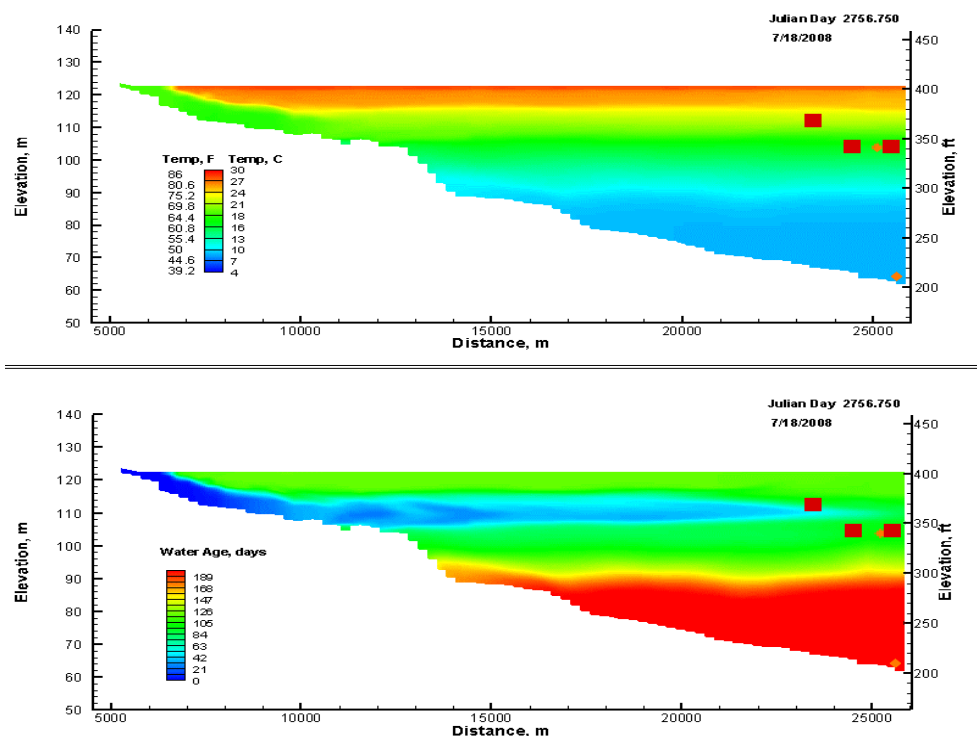


Figure 5. Effects of increased cold-water inflows (65°F) into Folsom Reservoir (top; inflow left side) on metalimnion cold-water interflows to the shutters at Folsom Dam (bottom; blue metalimnion interflow; red squares = shutters at two levels).

**Attachment G: Water Temperature Effects of PCWA
Water Transfer on Folsom Reservoir
and the Lower American River**

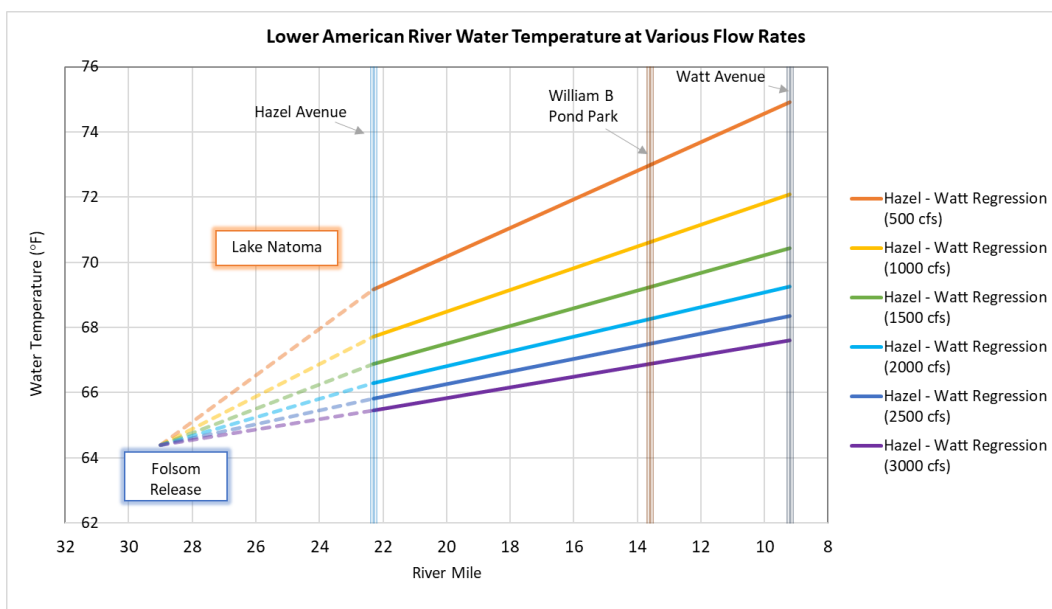


Figure 6. Effects of increased flow releases from Folsom Dam on the water temperature in the Lower American River where increased flow release results in colder water temperature downstream.

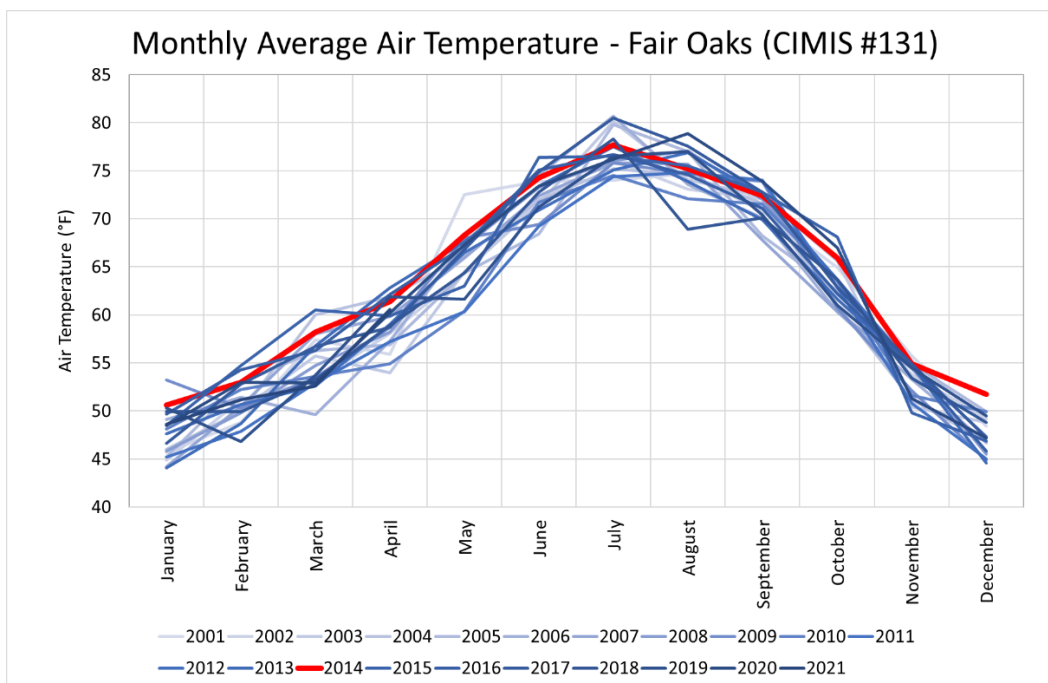


Figure 7. Example of Recent Meteorological (MET) Data (Air Temperature) (2001-2021) and 2014 Data (also years 2011, 2017, and 2020) used for the 2026 Temporary Transfer Water Temperature Modeling

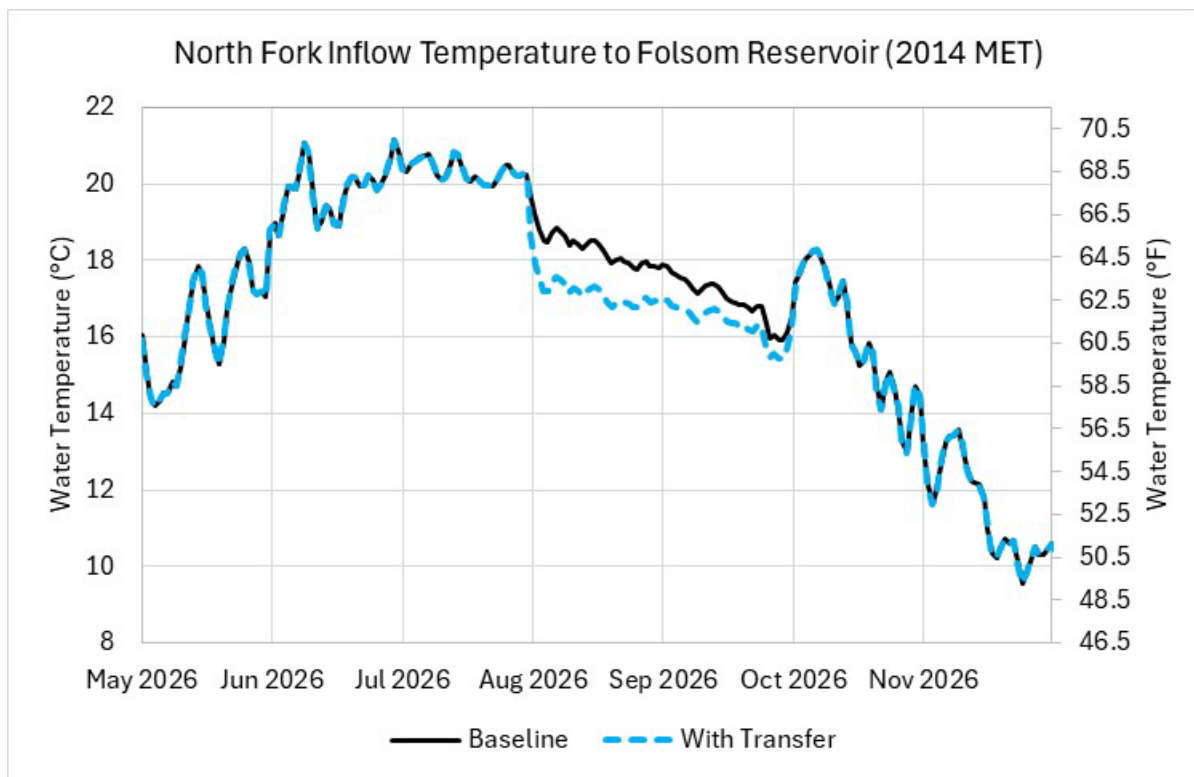


Figure 8. Water Temperature in the North Fork American River upstream of Folsom Reservoir for the Baseline Without Transfer and the 20 TAF Water Transfer Scenario.

6.0 2026 FOLSOM RESERVOIR WATER TEMPERATURE MODELING

Folsom Reservoir water temperature modeling was conducted using a well-calibrated, high-resolution, two-dimensional CE-QUAL-W2 model of Folsom Reservoir (Appendix G3) coupled with accurate regression models of the Lower American River at Hazel Avenue and Watt Avenue (Appendix G4). Meteorological data from 2014 (representing warm year conditions) were used for modeling (e.g., Figure 7) along with data from three additional years (2011, 2017, and 2020). Initial reservoir conditions in May were based on a measured water temperature profile from May 18, 2026. The model was configured to iteratively determine the lowest (coolest) Water Forum Flow Management Standard Automated Temperature Selection Procedure² (ATSP) schedule that was achievable for each scenario in the Lower American River at Watt Avenue, both with and without a November Folsom Powerhouse cold-water bypass, which is often implemented.

² To meet regulatory temperature targets in the Lower American River the Water Forum Flow Management Standard (Water Forum 2007) includes an incremental list of Automated Temperature Selection Procedure (ATSP) schedules. The primary objective of the temperature schedules is to maintain suitable temperatures for Central Valley steelhead during the summer rearing period and Chinook salmon spawning/incubation during the fall months given inflows, available reservoir volume, and outflows.

7.0 LOWER AMERICAN RIVER WATER TEMPERATURE

Modeling results show that the 2026 Transfer results in similar or slightly cooler water temperature regimes in the Lower American River. Folsom Reservoir operations and lower American River water temperature at Hazel Avenue and Watt Avenue are shown in Figure 9. Detailed summary graphics of each modeled MET year without and with a November Folsom Powerhouse cold-water bypass are shown in Figures 10a and 10b, respectively.

8.0 ADDITIONAL WATER TRANSFER EFFECTS

Releasing transfer water, in addition to providing water supply and environmental benefits, increases hydropower generation and CAISO grid regulation capacity and potentially increases commercial and recreational rafting opportunities in the Middle Fork American River. Making additional water available to PCWA's and Reclamation's powerhouses during the peak summer power load period is important for grid regulation in California. Hydroelectric power generation is the primary source of flexible generation used by the California Independent System Operator (California ISO) to regulate the fluctuations of the electric grid in California. The MFP is regularly called upon by California ISO to provide critical grid support services when load changes occur.

9.0 CONCLUSION

The 2026 Transfer releases water from MFP reservoirs that would not otherwise be released in 2026 and would remain in storage absent the transfer. For the August – September period, North Fork American River inflow to Folsom Reservoir would increase 15% as a result of the Transfer. The Transfer would not injure any legal user of the water and would benefit fish, wildlife, recreation, and other instream beneficial uses.

Specifically, the Transfer would provide the following beneficial effects:

- Increase water supply for agricultural and environmental purposes
- Increase flows in the Lower American River;
- Slightly decrease or maintain water temperatures in the Lower American River; and
- Provide additional ancillary benefits, including increased hydropower generation/grid regulation capacity, and potential enhancement of Middle Fork American River whitewater rafting opportunities.

**Attachment G: Water Temperature Effects of PCWA
Water Transfer on Folsom Reservoir
and the Lower American River**

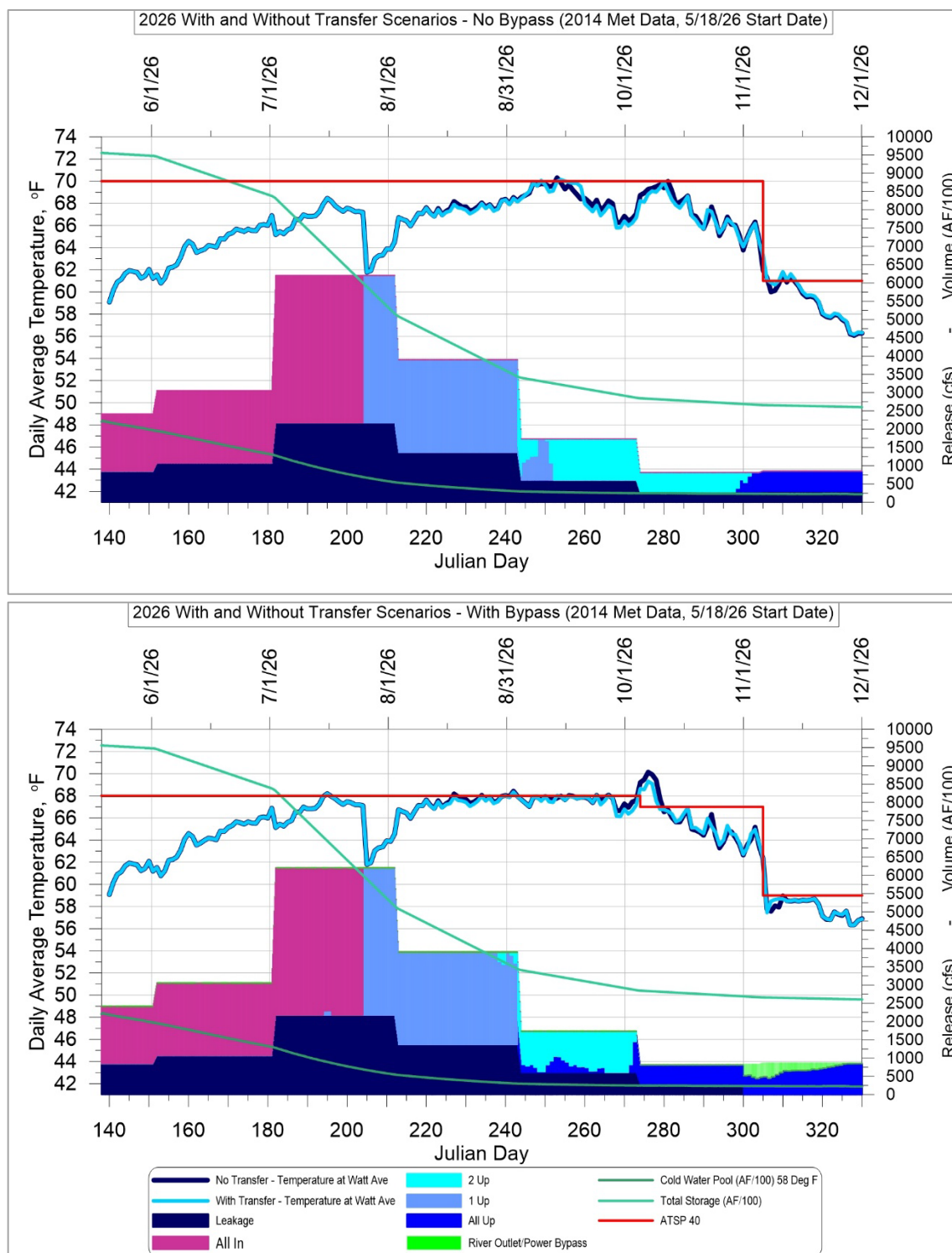


Figure 9. Folsom Reservoir Operations Summary, Lower American Water Temperature, and ATSP Schedules for the Baseline for the 20 TAF Transfer Scenario Without and With Bypass (top to bottom, respectively) for 2014 MET Data.

Attachment G: Water Temperature Effects of PCWA Water Transfer on Folsom Reservoir and the Lower American River

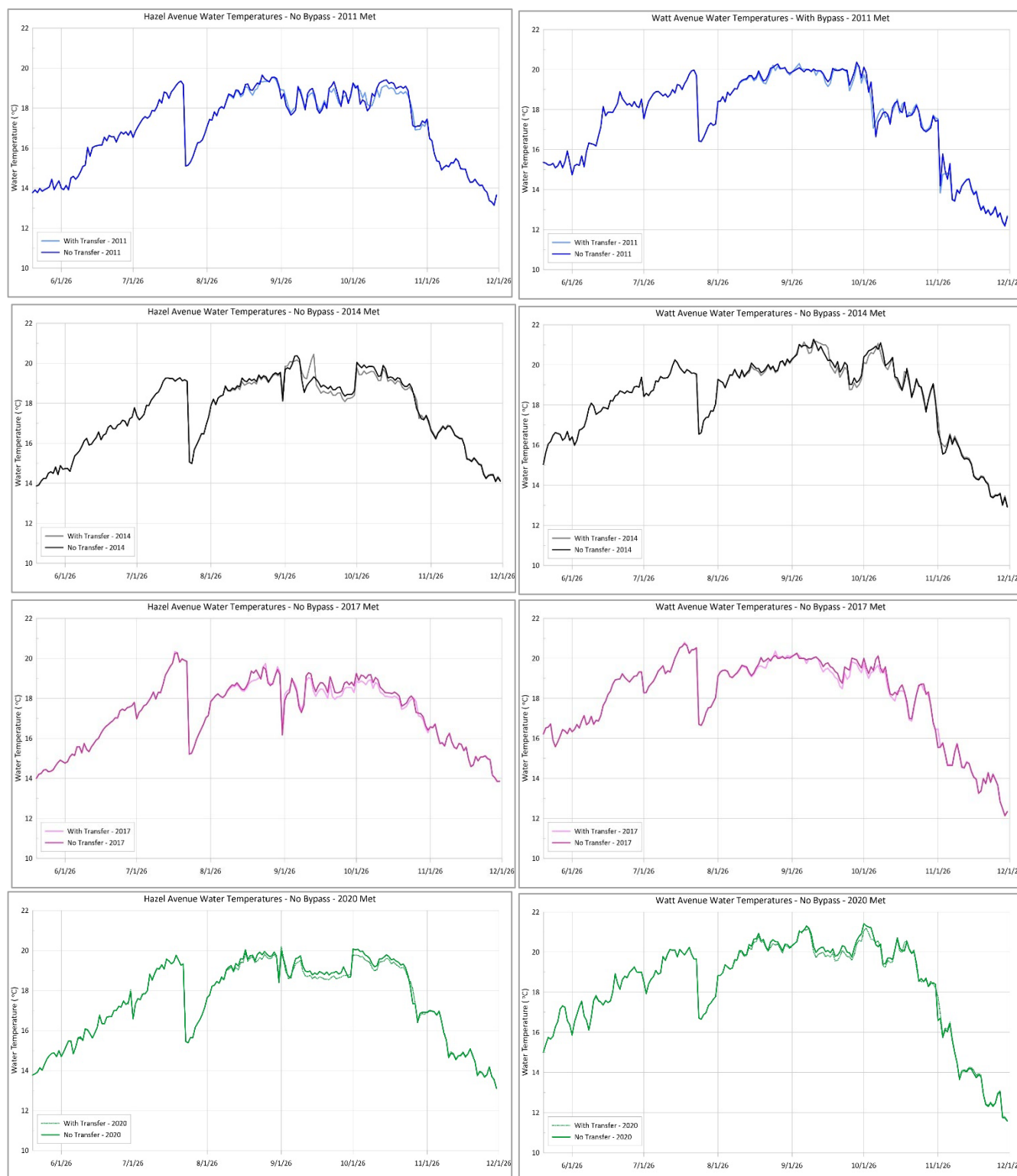


Figure 10a. Lower American River Water Temperature Summary With and Without the 20 TAF Transfer (dark vs light line) at Hazel Avenue (left) and Watt Avenue (right) (2011, 2014, 2017, and 2020 MET Data) for No Bypass Scenario.

Attachment G: Water Temperature Effects of PCWA Water Transfer on Folsom Reservoir and the Lower American River

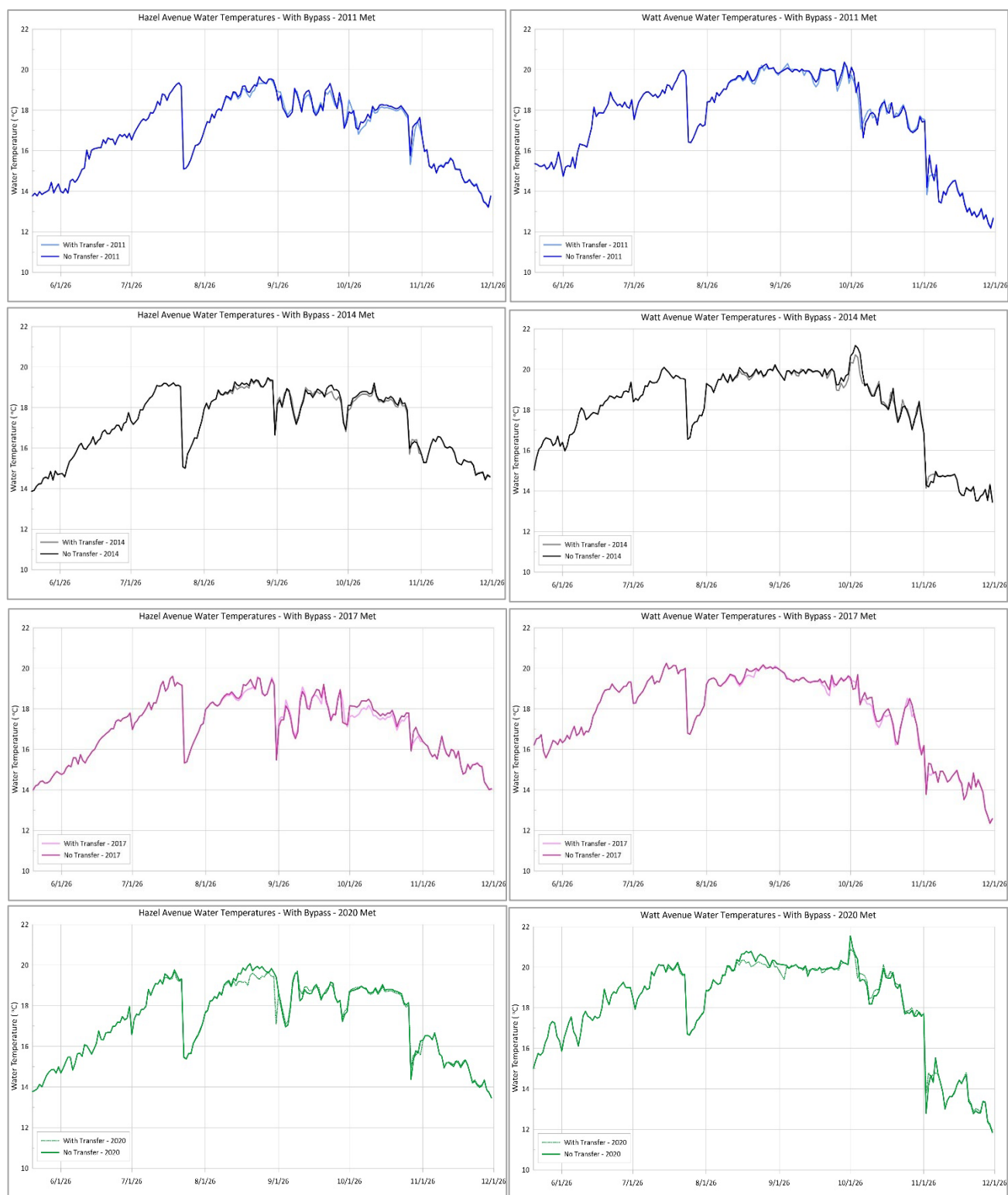


Figure 10b. Lower American River Water Temperature Summary With and Without the 20 TAF Transfer (dark vs light line) at Hazel Avenue (left) and Watt Avenue (right) (2011, 2014, 2017, and 2020 MET Data) for With Bypass Scenario.

APPENDIX G1

FOLSOM RESERVOIR INFLOW WATER TEMPERATURE REGRESSION MODELS

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List of Acronyms

CDEC	California Data Exchange Center
MFAR	Middle Fork American River
NFAR	North Fork American River
SFAR	South Fork American River
USGS	U.S. Geological Survey

Introduction

This appendix documents inflow water temperature into Folsom Reservoir and the relationship between water temperature, air temperature and flow for both the North Fork and South Fork American rivers (NFAR and SFAR). The sources for flow and temperature data, monthly regression relationships between flow, air and water temperatures, and comparisons of empirical versus modeled water temperatures (regression-based) are provided below.

Data Sources

The nearest NFAR and SFAR flow and temperature gages with recent historical data were used to characterize Folsom Reservoir inflow water temperature. Descriptions of the gaging and temperature stations are provided in Appendix G1 Table 1, and the locations are shown on Appendix G1 Map 1. All data were quality controlled prior to use in the analyses.

North Fork/Middle Fork American Rivers

Flow

The nearest active upstream gaging stations to Folsom Reservoir are located on the NFAR at North Fork Dam, CA (USGS gage no. 11427000) and on the MFAR near Foresthill, CA (USGS gage no. 11433300). The MFAR flows into the NFAR downstream of both of these gages. Daily average flows from the MFAR gage were combined with the daily average flows measured on the NFAR gage to produce an estimate of flow at the inlet to Folsom Reservoir (January 2000 – September 2025).

Water Temperature

Historical daily water temperature data were obtained from the USGS gaging station/California Data Exchange Center (CDEC) on the NFAR at Auburn Dam Site near Auburn, CA (USGS gage no. 11433790/station NFA) (July 1999 – June 2025). This location is just upstream of Folsom Reservoir.

South Fork American River

Flow

The nearest active upstream gaging station to Folsom Reservoir located on the SFAR is the USGS gaging station near Placerville, California (USGS gage no. 11444500). This gage does not account for local inflows between the gage site and the inlet to Folsom Reservoir; however very little inflow occurs below this gage during the drier months and in drier years (time period when water temperature is a function of flow).

Water Temperature

Historical water temperature data for the SFAR were obtained from USGS gaging station on the SFAR near Pilot Hill, California (USGS gage no. 11446030).

Flow and Water Temperature Relationships

North Fork/Middle Fork American River and SFAR water temperatures were strongly correlated with flow in the May – September time period and weakly correlated with flow in other months. Monthly regression relationships were developed from the empirical flow and water temperature data. In instances where the regressions needed to be applied on a daily basis throughout the year, the monthly regression coefficients were interpolated from the center of the month.

North Fork American River

For the NFAR water temperature into Folsom Reservoir a multiple regression equation that relates mean monthly North Fork American River flows (USGS gage near North Fork Dam) and mean monthly MFAR inflow (USGS gage near Foresthill) was developed to predict mean monthly water temperatures (January 2000 – September 2025) (Appendix G1 Table 2). Comparisons of the NFAR empirical and modeled water temperature for the inflows into Folsom Reservoir is provided in Appendix G1 Figure 1 and a time series plot showing the empirical and modeled water temperature is shown in Appendix G1 Figure 2.

South Fork American River

For the SFAR water temperature into Folsom Reservoir, a monthly regression relationship was developed from empirical flow and water temperature data from the SFAR average monthly water temperatures (USGS gage near Pilot Hill approximately 0.1 mile downstream of Weber Creek) and SFAR average monthly flows (SFAR USGS gage near Placerville) (January 2000 – September 2025) (Appendix G1 Table 3). Comparison of the SFAR measured and modeled water temperature for the inflows into Folsom Reservoir (January 2000 – September 2025) is provided in Appendix G1 Figure 3 and a time series plot showing the measured and modeled water temperature is shown in Appendix G1 Figure 4.

**APPENDIX G1
TABLES**

Appendix G1 Folsom Reservoir Inflow Water Temperature Regression Models

Appendix G1 Table 1. Data Sources for Folsom Reservoir Inflow Water Temperature Regression Analyses.

River Reach and Attribute	Data Sources					
	Operator	Name	Identification Number	Location (lat/long)	Period of Record Available	Period of Record Used in Regression Analyses
North Fork/ Middle Fork American River Watersheds						
North Fork American River Daily Average Flow	USGS	NF American R a North Fork Dam CA	11427000	38.93611°N/121.0228°W	10/1/1941-present; hourly	1/1/2000-9/30/2025
Middle Fork American River Daily Average Flow	USGS	MF American R nr Foresthill CA	11433300	39.00611°N/120.7597°W	10/1/1958-9/30/2012; daily	
Daily Average Water Temperature	USGS/ CDEC	NF American River at Auburn Dam	11433790/ NFA	38.852000°N/121.057000°W	7/21/1999-present; hourly	
South Fork American River Watershed						
Daily Average Flow	USGS	South Fork American River near Placerville	11444500	38.77111°N/120.8153°W	10/1/1911-9/30/2012; daily	1/1/2000-9/30/2025
Daily Average Water Temperature	USGS	South Fork American River near Pilot Hill	11446030	38.76306°N/121.0072°W	8/4/1999-present; hourly	

Abbreviations:

USGS: United States Geological Survey

CDEC: California Data Exchange Center

Appendix G1 Folsom Reservoir Inflow Water Temperature Regression Models

Appendix G1 Table 2. Monthly Regression Equations to Model North Fork American River Folsom Reservoir Inflow Water Temperatures based on Monthly Average North Fork and Middle Fork American River Flows and Monthly Average Local Air Temperature (based on January 2000 – September 2025 data).

Month	Regression Equation	R ²
X_{UNFA} = Upper North Fork American River Mean Monthly Flow (cfs) X_{MFA} = Middle Fork American River Mean Monthly Flow (cfs) X_{AIR} = Mean Monthly Air Temperature (°F) y = North Fork American River Mean Monthly Temperature (°F) upstream of Folsom Reservoir		
Jan	$y = 3.373 + (0.981)*LOGXUNFA + (0.159)*LOGXMFA + (0.245)*XAIR$	0.52 ¹
Feb	$y = 4.587 + (2.193)*LOGXUNFA + (-2.306)*LOGXMFA + (0.319)*XAIR$	0.55
Mar	$y = 6.987 + (2.960)*LOGXUNFA + (-4.388)*LOGXMFA + (0.366)*XAIR$	0.69
Apr	$y = 13.314 + (1.146)*LOGXUNFA + (-5.473)*LOGXMFA + (0.310)*XAIR$	0.79
May	$y = 18.255 + (-3.806)*LOGXUNFA + (-2.915)*LOGXMFA + (0.328)*XAIR$	0.82
Jun	$y = 23.145 + (-0.900)*LOGXUNFA + (-6.561)*LOGXMFA + (0.210)*XAIR$	0.82
Jul	$y = 30.844 + (1.886)*LOGXUNFA + (-12.165)*LOGXMFA + (0.116)*XAIR$	0.78
Aug	$y = 28.514 + (0.852)*LOGXUNFA + (-10.226)*LOGXMFA + (0.083)*XAIR$	0.61
Sep	$y = 21.365 + (-2.432)*LOGXUNFA + (-4.567)*LOGXMFA + (0.059)*XAIR$	0.52
Oct	$y = 9.897 + (0.858)*LOGXUNFA + (-2.880)*LOGXMFA + (0.443)*XAIR$	0.63
Nov	$y = 6.678 + (0.594)*LOGXUNFA + (-1.007)*LOGXMFA + (0.429)*XAIR$	0.58
Dec	$y = 4.587 + (2.193)*LOGXUNFA + (-2.306)*LOGXMFA + (0.319)*XAIR$	0.49 ¹

Regression Variables:

X_{UNFA} = Upper North Fork American River Mean Monthly Flow (cfs) at the North Fork Dam, CA (USGS gage no. 11427000)

X_{MFA} = Middle Fork American River Mean Monthly Flow (cfs) near Foresthill, CA (USGS Gage 11433300 until Sept 20 2014)(CDEC OXB starting Oct 1, 2014)

X_{AIR} = Air Temperature (°F) at Fair Oaks (CIMIS-131)

y = North Fork American River Mean Monthly Temperature (°F) upstream of Folsom Reservoir

¹ Low r-squared values are the result of a narrow range in temperatures in these months. These regressions represent the average water temperature.

**Appendix G1 Folsom Reservoir Inflow
Water Temperature Regression Models**

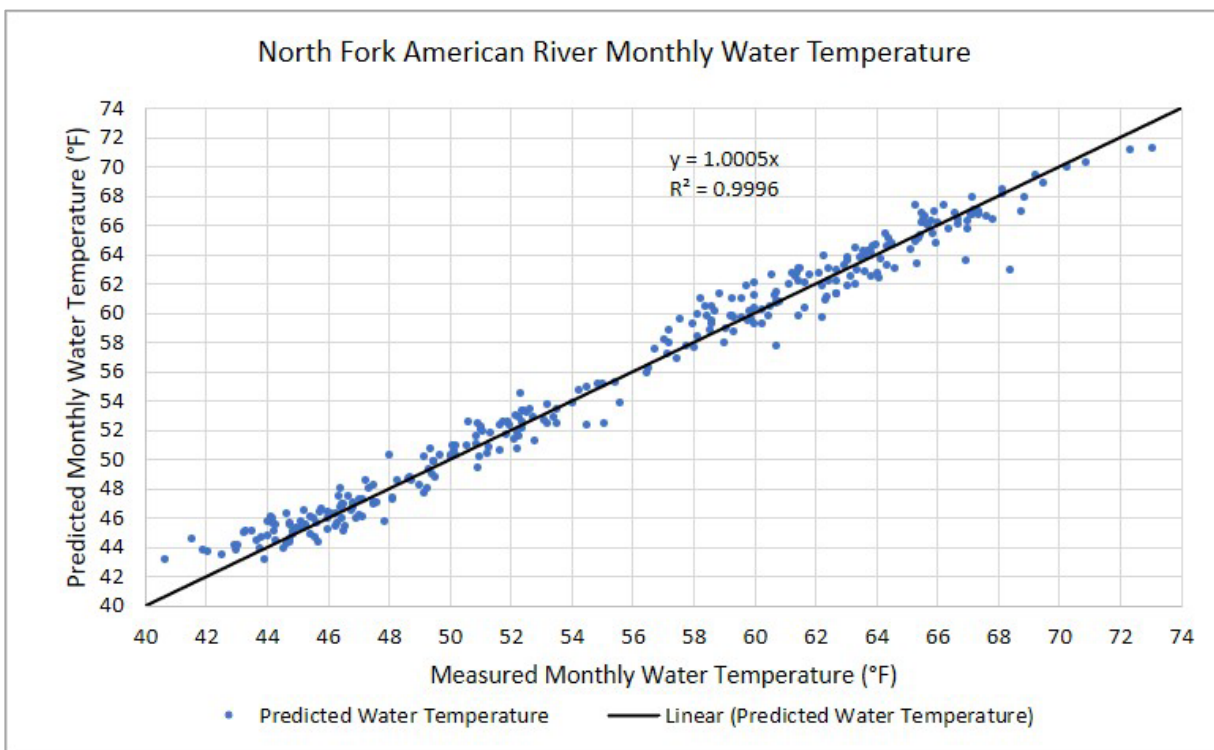
Appendix G1 Table 3. Monthly Regression Equations to Model South Fork American River Folsom Reservoir Inflow Water Temperatures based on Monthly Average South Fork American River Flows and Local Air Temperature (based on January 2000 – September 2025 data).

Month	Regression Equation	R ²
y = Predicted water temperature (°C) x = South Fork American River mean monthly flow (cms) Air = Mean monthly air temperature (°C)		
Jan	$y = 2.487 + (1.162) * \text{LOGXSFA} + (0.271) * \text{XAIR}$	0.46
Feb	$y = 3.977 + (0.244) * \text{LOGXSFA} + (0.270) * \text{XAIR}$	0.30
Mar	$y = 7.585 + (-1.016) * \text{LOGXSFA} + (0.229) * \text{XAIR}$	0.39
Apr	$y = 13.078 + (-3.244) * \text{LOGXSFA} + (0.215) * \text{XAIR}$	0.58
May	$y = 19.225 + (-5.781) * \text{LOGXSFA} + (0.214) * \text{XAIR}$	0.73
Jun	$y = 22.459 + (-6.748) * \text{LOGXSFA} + (0.213) * \text{XAIR}$	0.78
Jul	$y = 24.18 + (-6.193) * \text{LOGXSFA} + (0.132) * \text{XAIR}$	0.52
Aug	$y = 21.187 + (-5.057) * \text{LOGXSFA} + (0.125) * \text{XAIR}$	0.37
Sep	$y = 19.048 + (-3.671) * \text{LOGXSFA} + (0.073) * \text{XAIR}$	0.39
Oct	$y = 11.674 + (-2.488) * \text{LOGXSFA} + (0.293) * \text{XAIR}$	0.50
Nov	$y = 5.793 + (-0.133) * \text{LOGXSFA} + (0.401) * \text{XAIR}$	0.50
Dec	$y = 2.487 + (1.162) * \text{LOGXSFA} + (0.271) * \text{XAIR}$	0.49

Regression Variables:

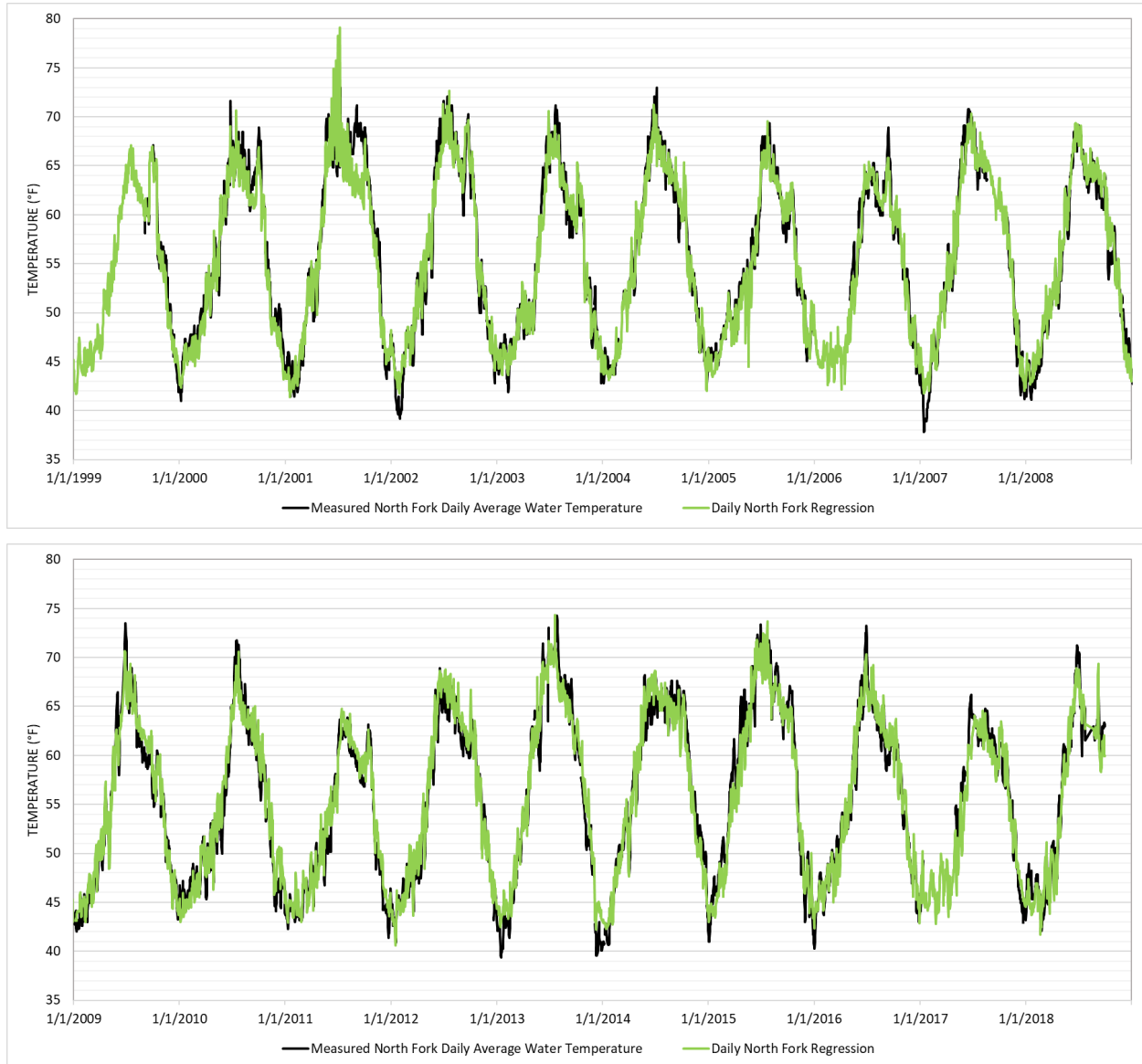
x = South Fork American River mean monthly flow (cms) near Placerville, CA (USGS Gage 11444500 through Sept 30 2014) (CDEC CBR from Oct 1 2015)
 y = South Fork American River Mean Monthly Temperature (°C) near Pilot Hill, CA (USGS gage no. 11446030)
 Air = Mean monthly air temperature at Fair Oaks (CIMIS-131) (°C)

**APPENDIX G1
FIGURES**



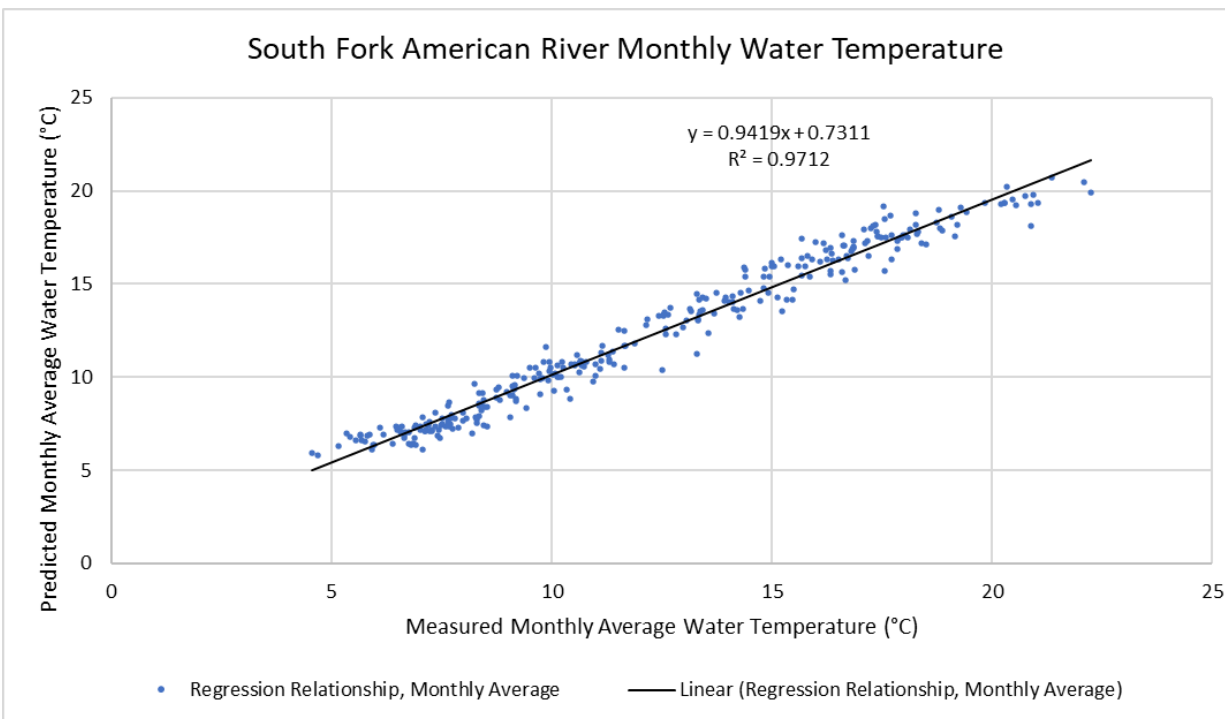
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Appendix G1 Figure 1. Measured versus Modeled (Regression) North Fork American River Temperature into Folsom Reservoir (July 1999-June 2014).



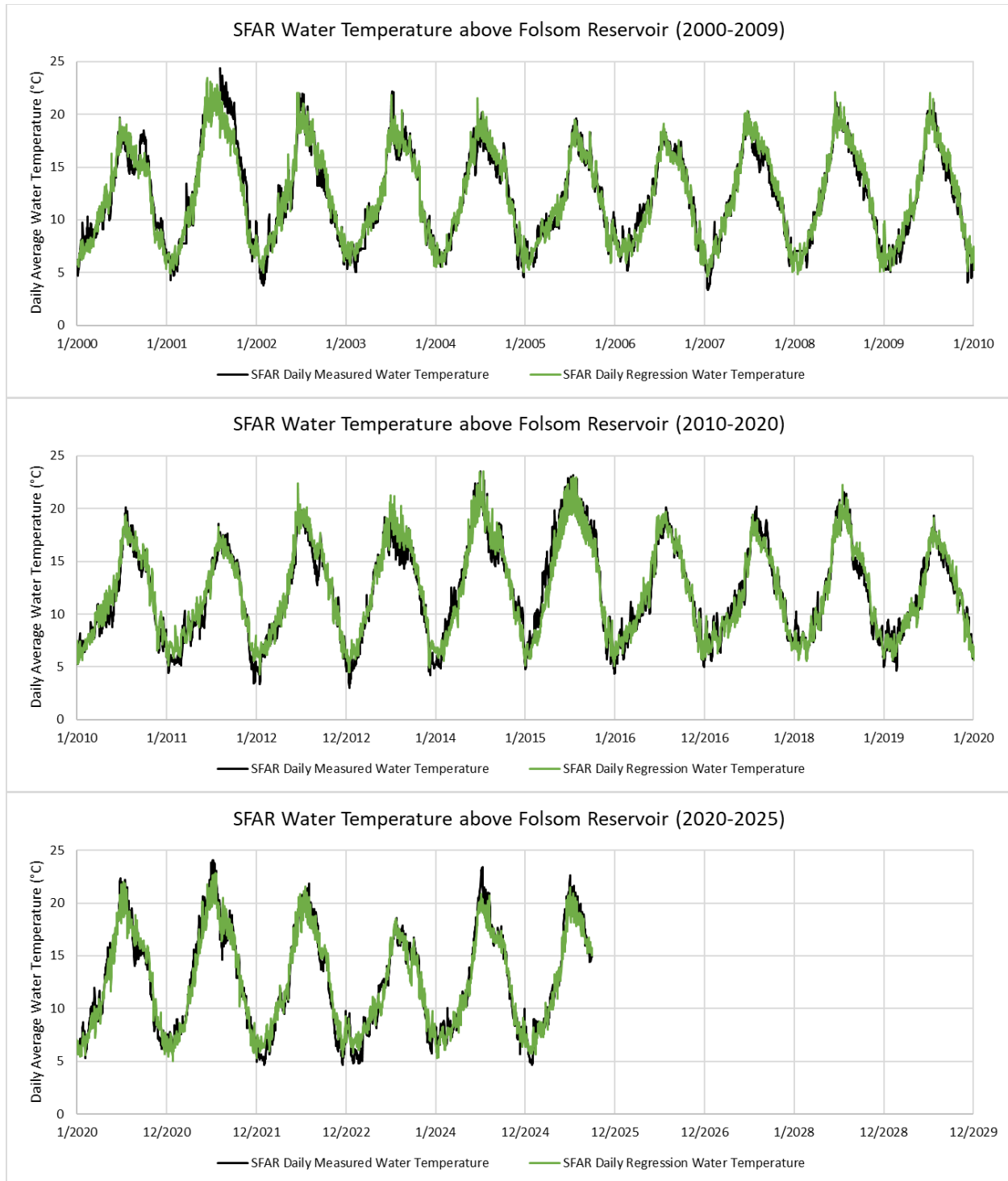
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Appendix G1 Figure 2. Time Series of Measured and Modeled North Fork American River Temperature into Folsom Reservoir (2000-2018).



Data sources: Measured water temperature: Monthly average water temperature (°F) (USGS gage no. 11446030). Modeled (regression) water temperature: Monthly average air temperature (°F) (CIMIS-131) and monthly average flow at Chili Bar (cfs) (USGS gage no. USGS/CDEC gage no. 11444500/CDEC CBR).

Appendix G1 Figure 3. Measured versus Modeled (Regression) South Fork American River Temperature into Folsom Reservoir (January 2000-September 2025).

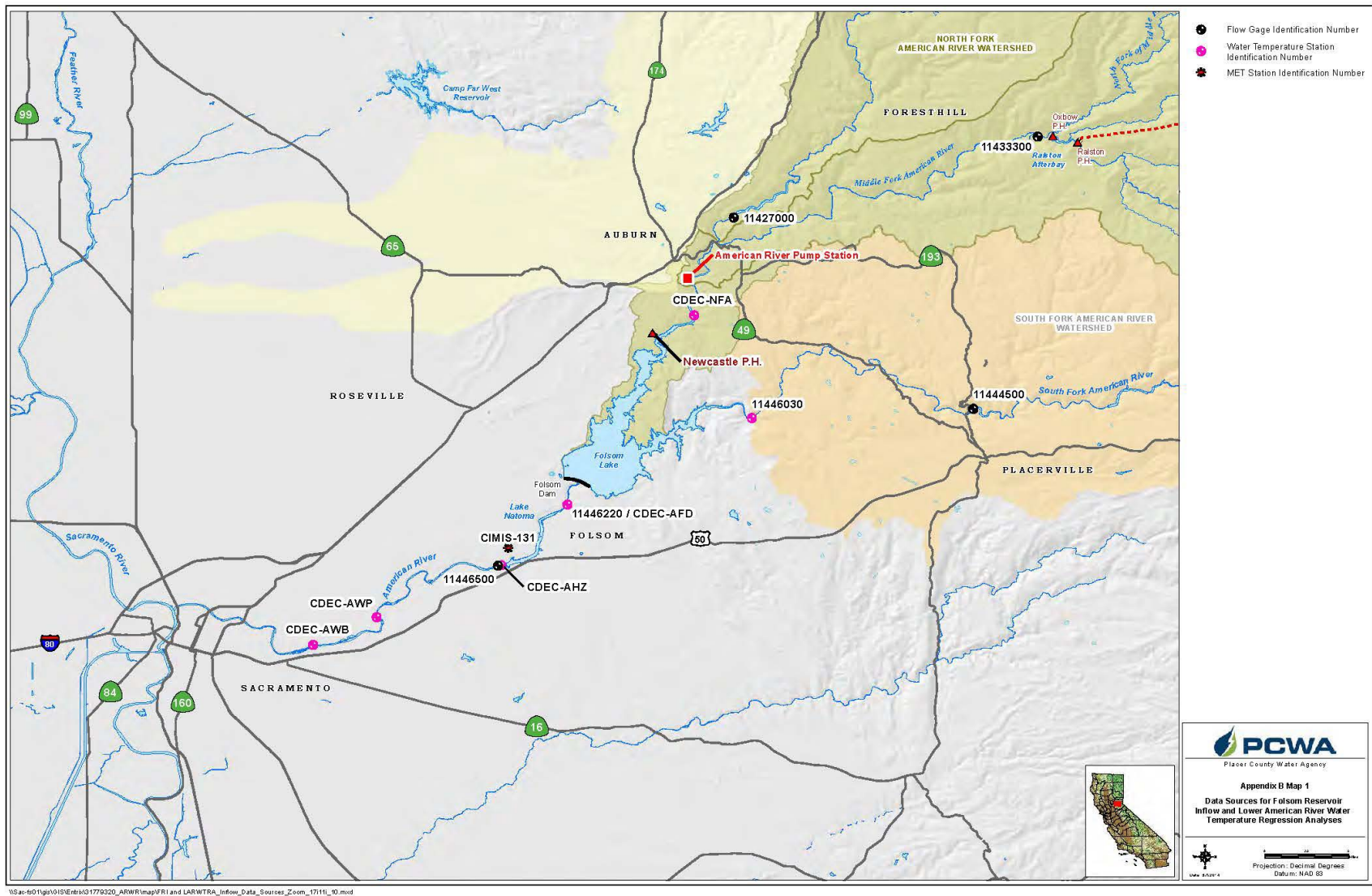


Data sources: Measured Temperatures: South Fork American River monthly average water temperature (°C) (USGS gage no. 11446030). Modeled (regression) water temperature: Monthly average air temperature (°C) (CIMIS-131) and monthly average flow at Chili Bar (cfs) (USGS gage no. 11444500).

Appendix G1 Figure 4. Time Series of Measured and Modeled South Fork American River Temperature (January 2000-September 2025).

**APPENDIX G1
MAP**

Appendix G1 Folsom Reservoir Inflow Water Temperature Regression Models



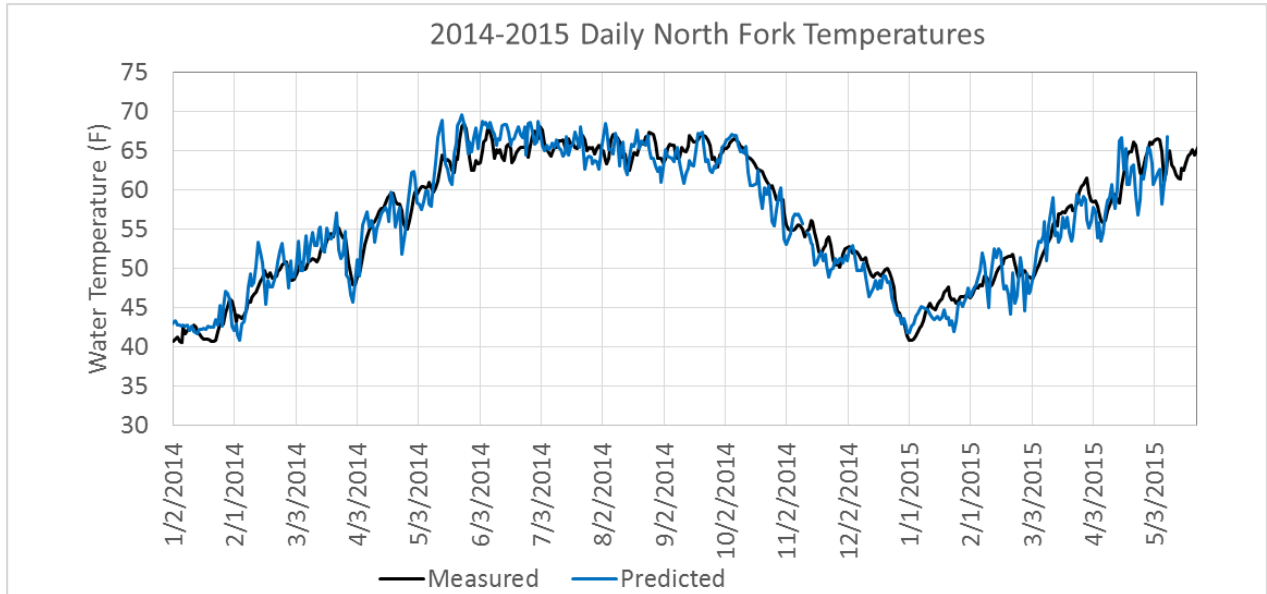
Appendix G1 Map 1. Data Source Locations

***Appendix G2: North Fork, South Fork, and Lower American
River Regression Model Performance for 2014***

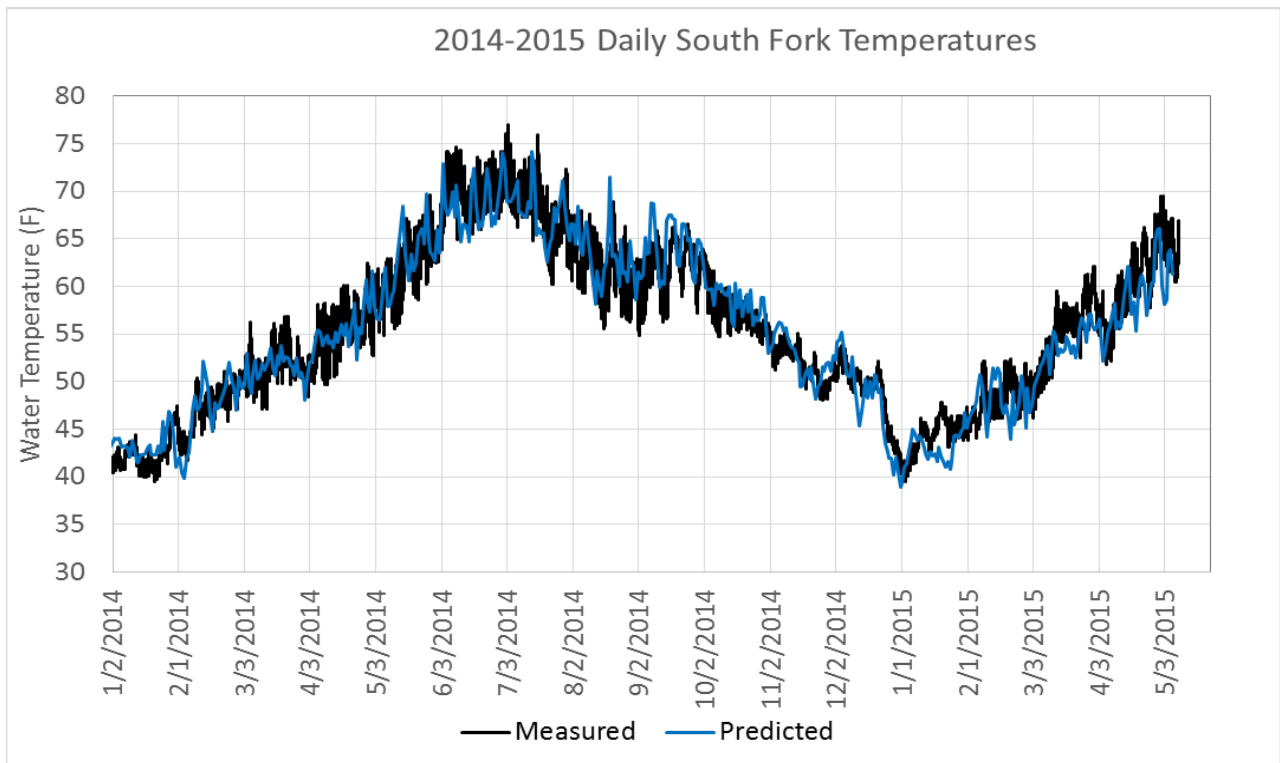
APPENDIX G2

**EXAMPLE NORTH FORK, SOUTH FORK, AND LOWER AMERICAN RIVER REGRESSION MODEL
PERFORMANCE FOR 2014.**

Appendix G2: North Fork, South Fork, and Lower American River Regression Model Performance for 2014

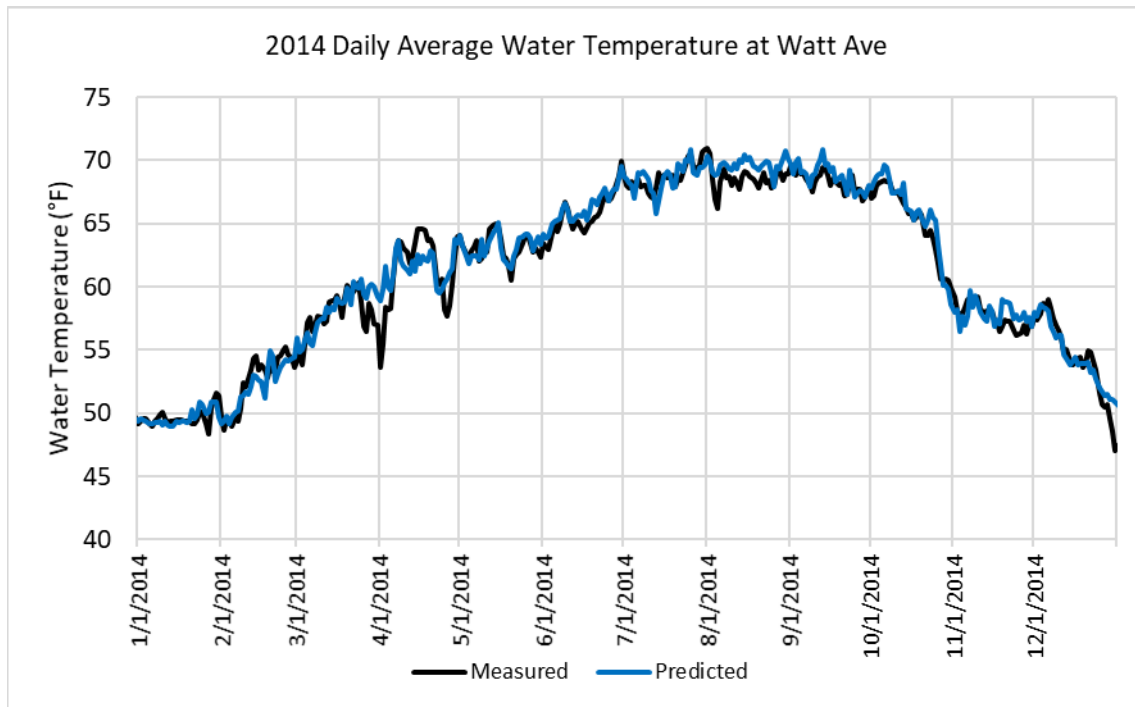


Appendix G2 Figure 1. Measured and Predicted (Regression) North Fork American River Temperature into Folsom Reservoir (January 2014- May 2015).



Appendix G32 Figure 2. Measured and Predicted (Regression) South Fork American River Temperature into Folsom Reservoir (January 2014- May 2015).

Appendix G2: North Fork, South Fork, and Lower American River Regression Model Performance for 2014



Appendix G2 Figure 3. Measured and Predicted (Regression) Lower American River Temperature at Watt Avenue (January 2014 - Jan 2014).

APPENDIX G3

FOLSOM RESERVOIR CE-QUAL-W2 WATER TEMPERATURE MODEL

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List of Acronyms

ATSP	Automated Temperature Selection Procedure
SFAR	South Fork American River
WSE	water surface elevation

Abstract

Folsom Reservoir, located near Sacramento, California, USA, is a deep-storage reservoir that provides municipal water, power generation, and cold water releases for salmonid fish in the Lower American River. The dam has discrete temperature control shutters on the three powerhouse intakes. The shutters can be installed or removed in sections and they allow the dam operator to choose different water levels from each intake to blend outflow water temperature to accommodate downstream temperature requirements. The dam also has a municipal water outlet with a continuously adjustable temperature control device and a set of low-level outlets that are used for water temperature control.

A complex model of the reservoir was developed using the CE-QUAL-W2 model (Cole and Wells 2013) and calibrated to historical operations over a 10-year time period. Absolute mean temperature errors in model profiles and in downstream temperature were 0.56°C and 0.58°C, respectively, well less than the target of <1°C. Significant leakage through the temperature control shutters at the dam was identified during model calibration.

A customized operational model tool was developed using the CE-QUAL-W2 model to automatically determine how best to select outlet shutter positions to maximize efficient use of the limited cold water available within the reservoir to meet the downstream temperature regulatory targets for fish in the Lower American River. The model proved successful in running long-term simulations that can be used to evaluate reservoir operations based on modified or forecasted hydrological and meteorological inputs.

Introduction

A Folsom Reservoir water temperature modeling tool was developed to evaluate alternative inflow hydrology and reservoir operations scenarios and shutter operations for Folsom Dam to meet regulatory temperature targets in the Lower American River (i.e., Automated Temperature Selection Procedure [ATSP] schedules identified in the Water Forum Flow Management Standard [Water Forum 2004; Water Forum 2006]). The primary objective of the temperature schedules are to maintain suitable temperatures for Central Valley steelhead during the summer rearing period and Chinook salmon spawning/incubation during the fall months given inflows, available reservoir volume, and outflows.

Folsom Dam was designed to be able to release water from various elevations within the reservoir simultaneously. Dam operators install or remove discrete temperature shutters on the three powerhouse intakes to take water from different depths to blend outflows to meet downstream regulatory temperature objectives. Operators also adjust the elevation of the municipal water supply outlet and operate the low-level outlets on the dam to modify outflow water temperatures / preserve cold water resources in the reservoir.

The water temperature modeling tool was developed to automatically determine the best shutter settings and flow rates through each of the three powerhouse intakes to meet the coldest ATSP outflow temperature schedule possible and to utilize cold water in the reservoir most effectively. This includes a user specified target temperature for the municipal outlet and use of

the low-level outlets in late fall to access cold water that remains in the reservoir below the powerhouse outlets.

The modeling tool uses CE-QUAL-W2 (Cole and Wells 2013), a 2-D hydrodynamic and temperature model, modified with new model code to enhance and automate temperature shutter modeling capability (including low-level outlets) and ATSP temperature schedule selection capability. The completed modeling tool allows modelers to run scenarios in which the model itself determines the optimal operation of powerhouse shutters, municipal outtake, and low-level outlets to meet downstream temperature targets.

Background Information

Folsom Dam and reservoir are located approximately 20 miles northeast of the city of Sacramento, California, on the American River. This reservoir has a capacity of 976,000 acre-feet (1,203,878,290 cubic meters) and drains an area of approximately 1,875 square miles (4,856 square kilometers). The dam was built by the U.S. Army Corps of Engineers between 1948 and 1956, at which point operation of the dam was transferred to the Bureau of Reclamation (U.S. Dept. of Interior 2013). Downstream of Folsom Dam, the American River provides important habitat for Central Valley steelhead and Chinook salmon. Water temperatures in this section of the river play a critical role in determining the health of these, as well as other aquatic species.

Folsom Dam was constructed with a total of twenty different outlets and outlet structures. Three power generation penstocks are each fitted with discrete, removable/installable shutters that allow for four different configurations (discrete inflow elevations). These configurations allow the operator to pull water from different depths depending on water level and desired outflow temperature. In addition to the powerhouse shutters, a variable elevation temperature control device is used to divert water for municipal use. The remaining structures are all at fixed locations and include eight rectangular river outlets and eight spillway gates. These are generally used only for flood control and occasionally for temperature control in the late fall (low-level outlets). The use of the low-level outlets in the fall results in water bypassing the power generators. The locations of the main features on Folsom Dam are shown in Appendix G3 Figure 1. An earlier model study of Folsom Reservoir by the Bureau of Reclamation (Bender et al. 2007) was conducted in 2007. In that study, the CE-QUAL-W2 model was also used but with a coarser bathymetric grid than what was used in this study (described below).

Model Bathymetry

Bathymetric data for Folsom Reservoir were collected by means of multi-beam sonar and photogrammetry during the fall of 2005 as part of a sedimentation study conducted by the Bureau of Reclamation (Ferrari 2007). These data were used to develop a 3-D bathymetric representation of Folsom Reservoir as seen in Appendix G3 Figure 2. This grid was in turn used to develop the CE-QUAL-W2 model grid, shown in Appendix G3 Figure 3. The grid was divided up into a total of three branches with 191 segments each having an average length of 250 meters. The vertical model resolution was 0.61 meter or 2 feet. The model grid matched the 2005 Sediment Survey volume elevation and surface area elevation curves (Ferrari 2007).

Historical Model Calibration

The model was calibrated for a 10-year period between January 1, 2001, and December 31, 2011. Boundary conditions for inflow, meteorological data, and outflow during this period were developed. A very detailed approach for filling in data gaps was undertaken to provide a good set of boundary conditions for the 10-year period.

Secchi disk data from 1979 were used to estimate the average light extinction coefficient. Calculations show that the light extinction coefficient varied from 0.3 to 0.7 m⁻¹ with an average value close to the CE-QUAL-W2 default value of 0.45 m⁻¹.

Inflows included the North and Middle Forks of the American River, the South Fork American River (SFAR), Mormon Ravine, and Newcastle Powerplant. Outflows included three penstocks with discrete shutter settings, municipal water withdrawals with variable shutter settings, low-level outlet releases, spills, and evaporation.

Air temperature, dew point temperature, wind speed and direction, cloud cover, and solar radiation were collected from various meteorological stations in the vicinity of Folsom Reservoir for this time period. Most of the model development uncertainty was in filling meteorological data gaps (e.g., wind data) and in estimating the amount of leakage into the lower level powerhouse outlets from the shutters.

Almost one thousand temperature profiles were taken over this 10-year period at six stations in Folsom Reservoir with a profile frequency of about once per month (data were collected by Bureau of Reclamation). Appendix G3 Figure 4 compares two representative model predictions with field data for temperature profiles taken in August 2002 and October 2007. Error statistics for the 10-year model period versus measured profiles are shown in Appendix G3 Table 1.

A comparison of all measured profile data to model profiles over the 10-year period is shown in Appendix G3 Figure 5.

Model predicted water temperatures and measured water temperatures immediately downstream of Folsom Dam were also compared (Appendix G3 Figure 6). Absolute mean errors for downstream temperatures were less than 0.6°C.

Automatic Model Simulation Tools

Three individual model tools were developed and verified using boundary condition and meteorological data from the same time period to fully automate shutter operation. The three tools are as follows:

Automatic Municipal Water Intake Elevation

Based on the available historical data, 2006 and 2011, operators of the municipal water intake structure generally tried to extract water at approximately 18°C (65°F) or cooler during most time periods, given operational constraints (e.g., reservoir water surface elevation, minimum and maximum inlet elevations). This capability was built into the model, allowing the modeler to specify the municipal intake constraints: (1) target temperature; (2) maximum and minimum inlet elevations; and (3) minimum inlet elevation below the water surface elevation (WSE).

In addition to these constraints, operation rules were set including the following:

1. On March 1 of each model year, the elevation of the intake was raised as high as possible given the WSE constraint;
2. If not raised to maximum on March 1st, the model continued checking on a daily basis until the intake could be raised to a maximum elevation;
3. If intake temperature criteria were violated, the intake was lowered in 1 meter increments until water temperature met criteria; and
4. The model continued lowering intake elevation as dictated by the temperature criteria until Dec 1 of each model year, or until the minimum water intake elevation was reached.

Automatic Shutter Operations

The automatic shutter operation algorithm was developed to divide flow through each of the three powerhouse penstocks and to determine when to change the shutter configuration to pull water from the appropriate location in the reservoir to achieve target outflow temperatures. Each of the Folsom Dam powerhouse penstock shutters operate independently and have a total of four different elevation settings. The overall flow rate was specified as well as a daily water temperature target that the model was trying to match. A code was developed to calculate the percent flow to be directed through each penstock and the shutter elevations given the following constraints:

1. Minimum and maximum flow through each powerhouse; and
2. Shutter minimum elevation below WSE at any time (8.23 meters); otherwise the shutter opening would be lowered to the next lowest level.

An extensive set of operational rules were set up to apportion flow through each of the powerhouse penstocks and determine when the shutter opening needed to be lowered in order to meet temperature criteria. When all shutter openings were at their lowest level and temperature criteria were still not being met, the model was set up to allow a portion of the outflow water to pass through the lower level river outlets at the bottom of the dam – completely bypassing the powerhouse (a date range can be set in the input data to constrain when this operation can occur).

Automatic Temperature Schedule Choice

An algorithm was developed that allowed the model to run and to converge on the coldest ATSP temperature schedule that could be met. The model user provides ten temperature target “schedules” or daily average temperature time-series files, ranging from coolest (#1) to warmest (#10). The model starts with schedule #5 and runs until it violates a temperature criterion more than three times in a season (either consecutively or cumulatively), at which point it restarts to an earlier time and chooses a warmer target schedule. Conversely if the starting temperature target file was too warm and the outflow temperatures never violate the temperature target, the model restarts to an earlier time and reruns using a cooler temperature target file. This logic for running the model is shown in Appendix G3 Figure 7.

Example Results of Automatic Shutter and Municipal Outlet Scenario

An example of the combined outflow temperature results of the automated temperature model for 2008 is shown compared to an historical operations calibration model in Appendix G3 Figure 8. Compared to actual operations, the model code optimized Lower American River water temperature by releasing warmer water earlier in the summer and maintaining significantly cooler temperatures later into the fall spawning season. Resulting water temperatures approximately 32 km (20 miles) downstream at Watt Avenue are shown in Appendix G3 Figure 9.

Conclusions

Using extensive flow, water temperature, and meteorological empirical data from 2001 to 2011, a fully calibrated CE-QUAL-W2 model of Folsom Reservoir was developed. The model performed very well when compared to in-lake temperature profile and downstream temperature data, with absolute mean errors of less than 0.6°C for both metrics. This calibrated model was then run using a series of tools developed to allow complete automation of the municipal outlet and powerhouse penstock shutters.

Acknowledgements

Calibration data sets were provided by the U.S. Bureau of Reclamation. We benefitted greatly by learning from previous modeling efforts by Chris Hammersmark, CBEC Inc., who has used the 1D Iterative Coldwater Pool Management Model extensively to model Folsom Reservoir.

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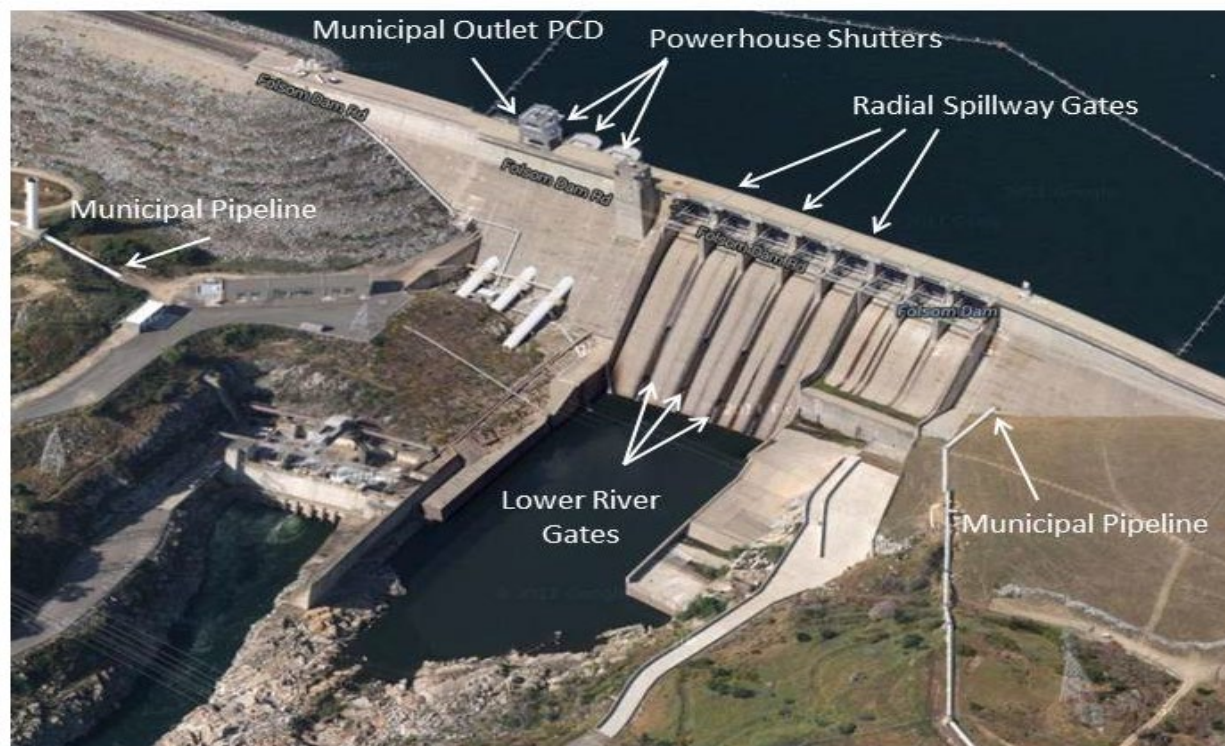
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APPENDIX G3
TABLES

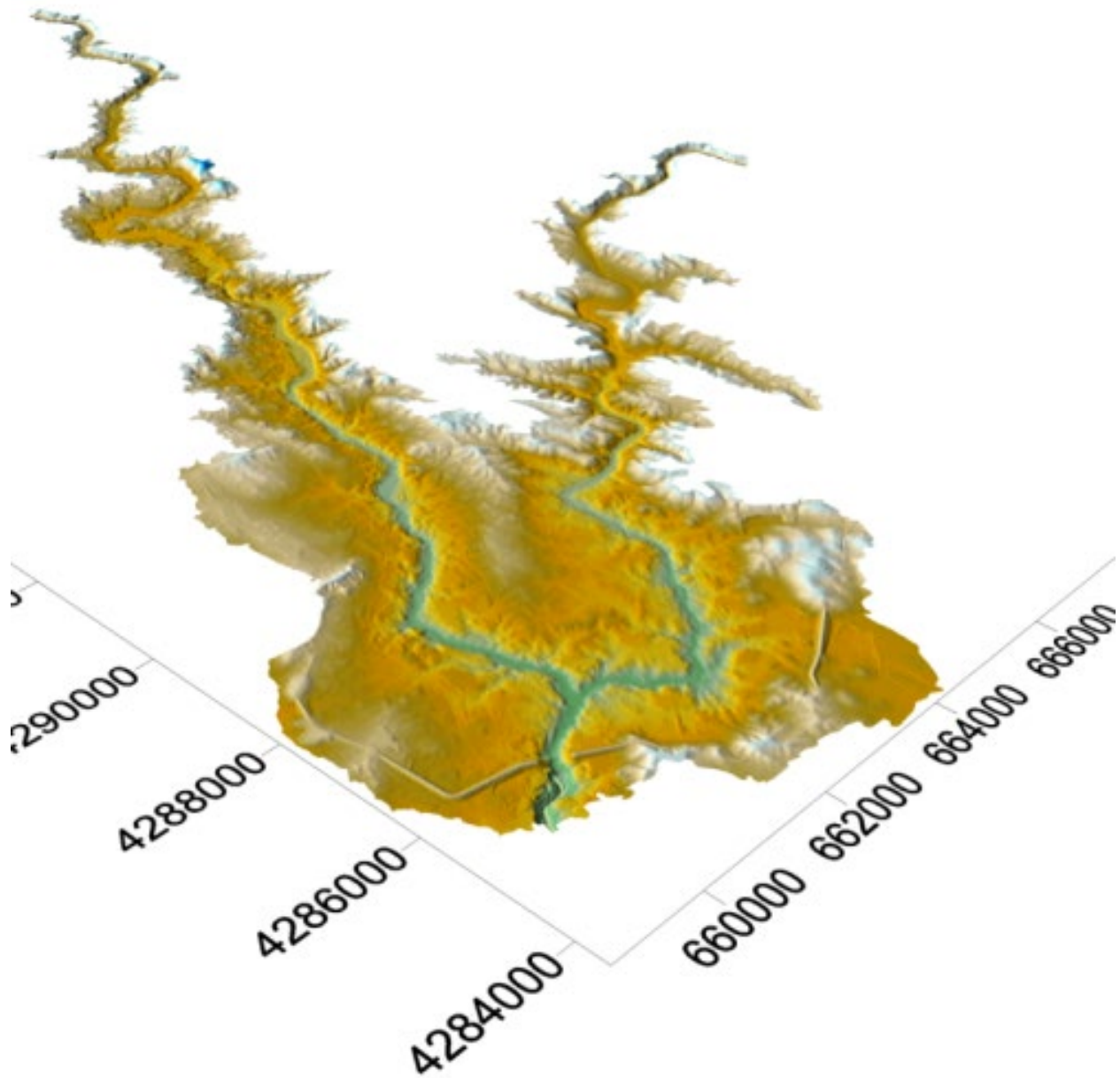
Appendix G3 Table 1. Modeled Versus Measured Temperature Profile Error Statistics.

Temperature Profile Model Segment (USBR Site)	# of Profiles	# of Individual Temperature Observations	Mean Error °C	Absolute Mean Error °C	Root Mean Squared Error °C
63 (Site A)	169	4421	-0.050	0.607	0.772
72 (Site E)	154	4681	-0.093	0.589	0.769
91 (Site C)	154	4861	0.032	0.520	0.669
105 (Dam)	178	7190	-0.049	0.530	0.689
151 (Site B)	154	4283	0.175	0.585	0.726
169 (Site D)	171	5943	0.011	0.506	0.648
Average overall statistics:			0.004	0.556	0.712

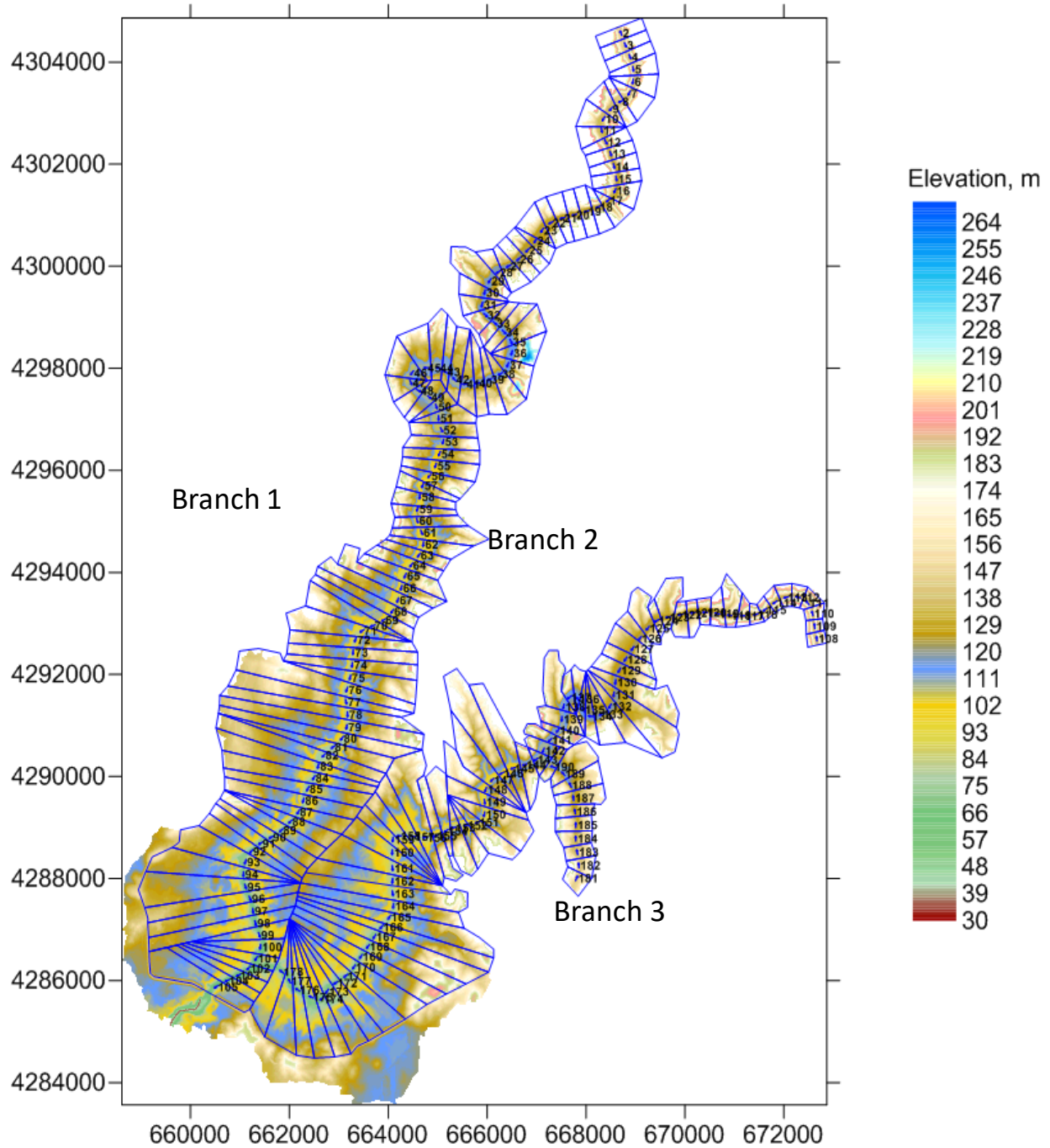
APPENDIX G3
FIGURES



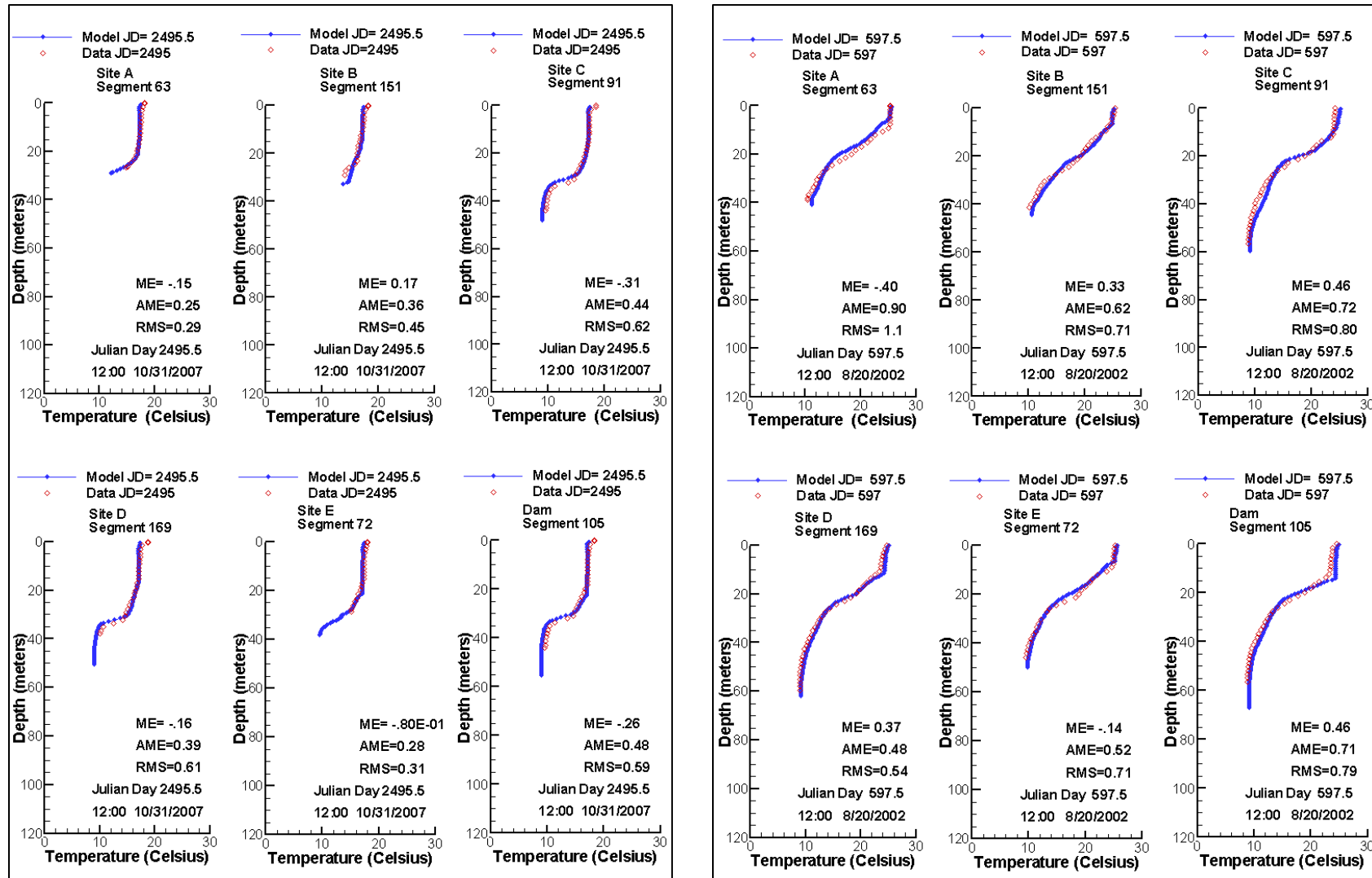
Appendix G3 Figure 1. Folsom Dam Outlet Structures (Google Maps, 2013)



Appendix G3 Figure 2. Folsom Reservoir Bathymetry Showing the North Fork and South Fork of the American River Channels (dimensions are in meters).

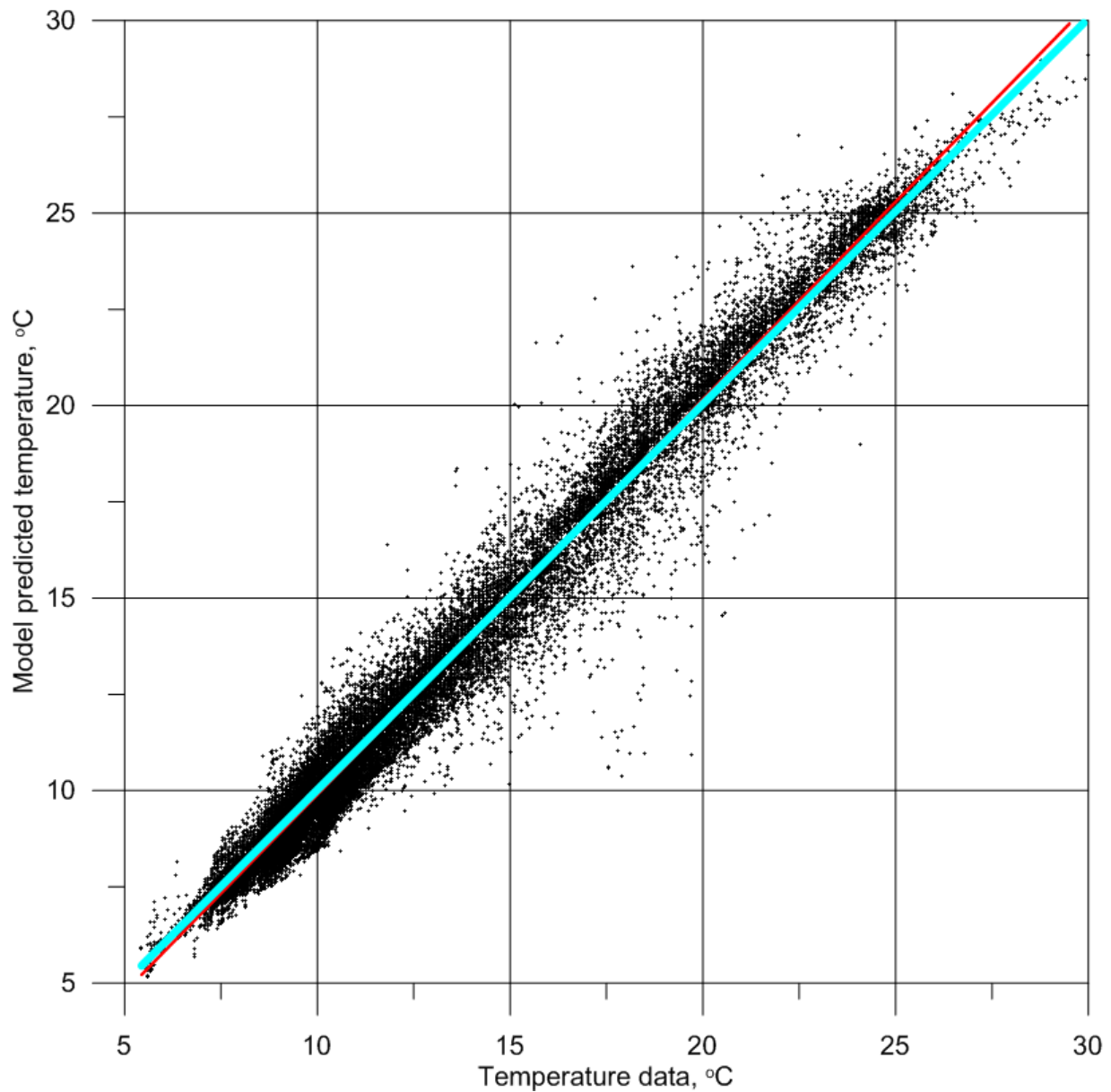


Appendix G3 Figure 3. Model Grid Segment Layout for the Three Model Branches (dimensions are in meters).



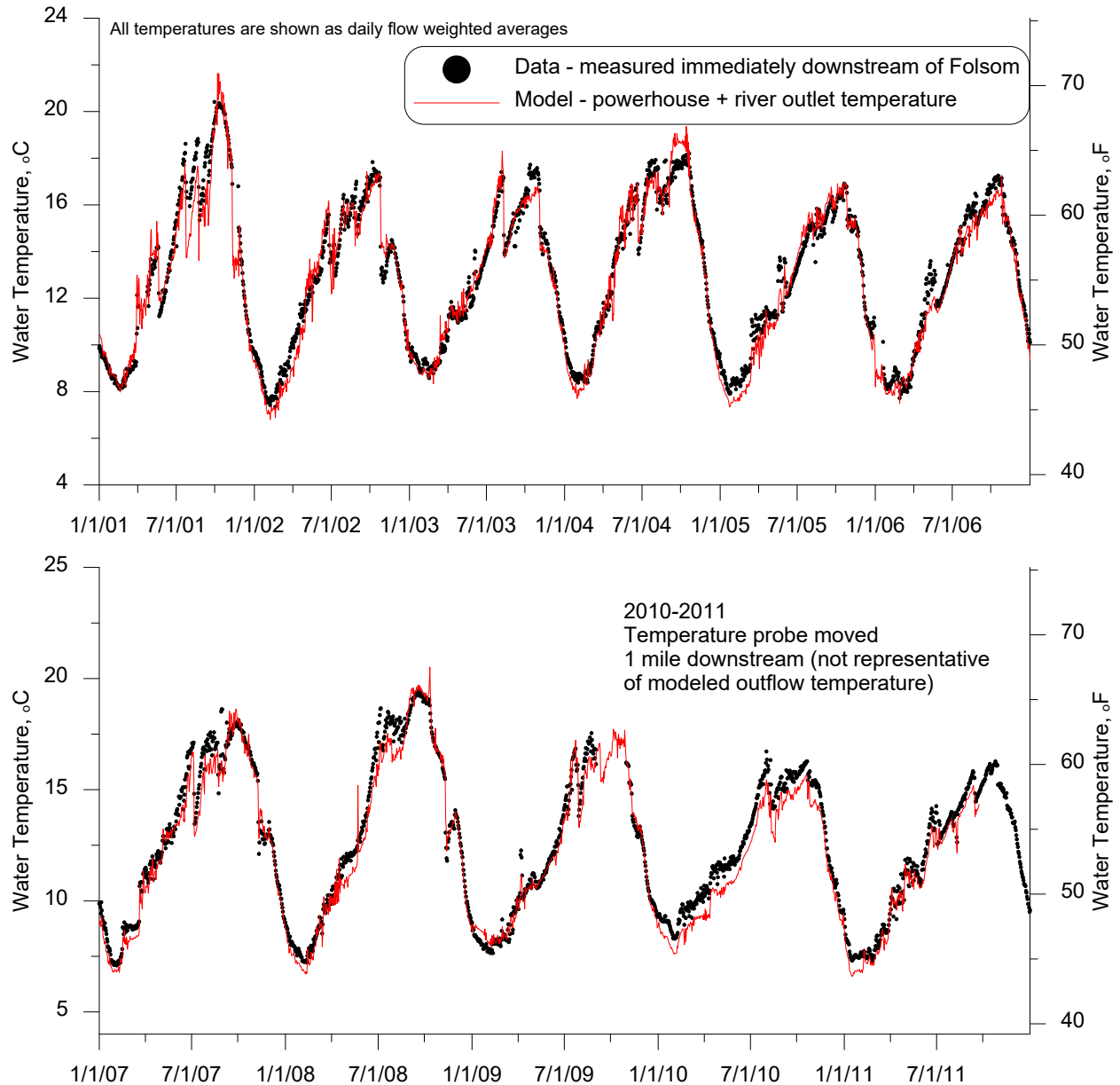
Appendix G3 Figure 4.

Model Temperature Profiles Compared to Measured. Temperature Profiles on August 20, 2002 (left) and October 31, 2007 (right) at Six Different Stations in Folsom Reservoir.



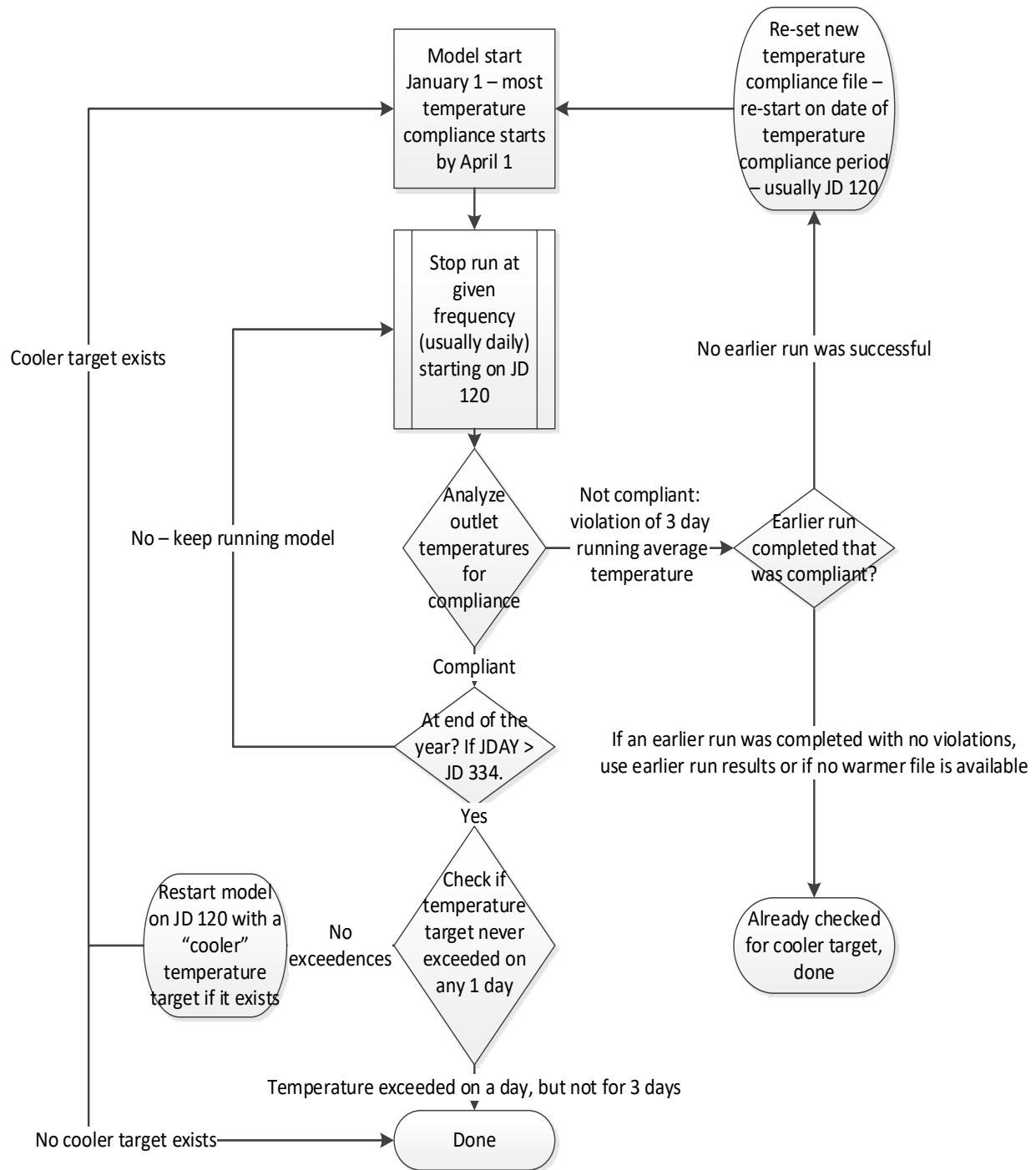
Appendix G3 Figure 5. Comparison of Model Predicted Temperature Profile and Measured Temperature Profile Data between 2001 and 2011. (Slope of the linear regression through the origin is 1.002 with an R2 of 0.996 [red line]; blue line is a 1:1 slope).

Appendix G3 Folsom Reservoir CE-QUAL-W2 Water Temperature Model



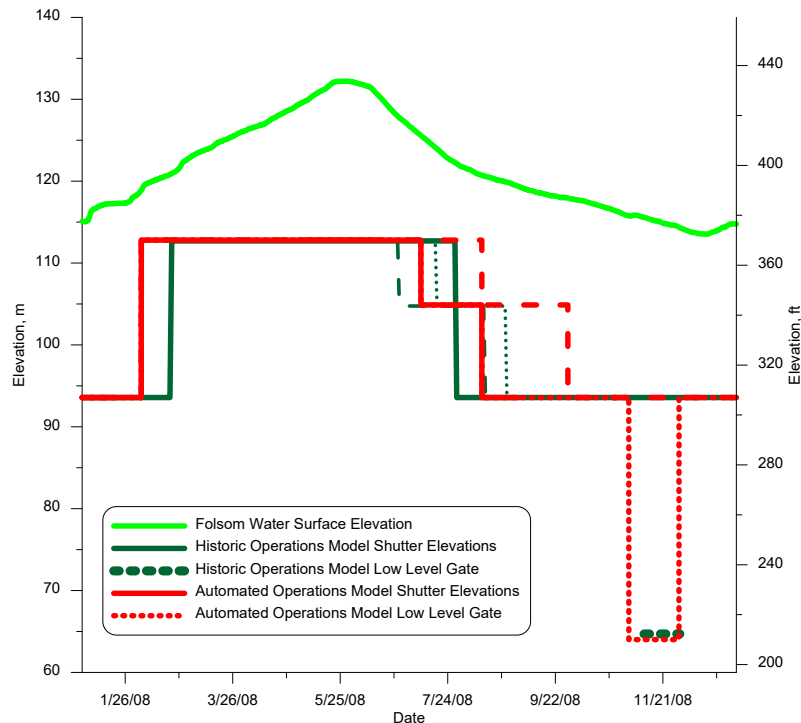
Appendix G3 Figure 6.

Model Predicted Temperatures below Folsom Dam Compared to Measured Temperatures Immediately Downstream of Folsom Dam between 2001 and 2009. For 2010 and 2011, Model Predictions and Observed Data are shown, but not completely comparable because the Observed Data were collected 1 mile downstream of Folsom Dam.



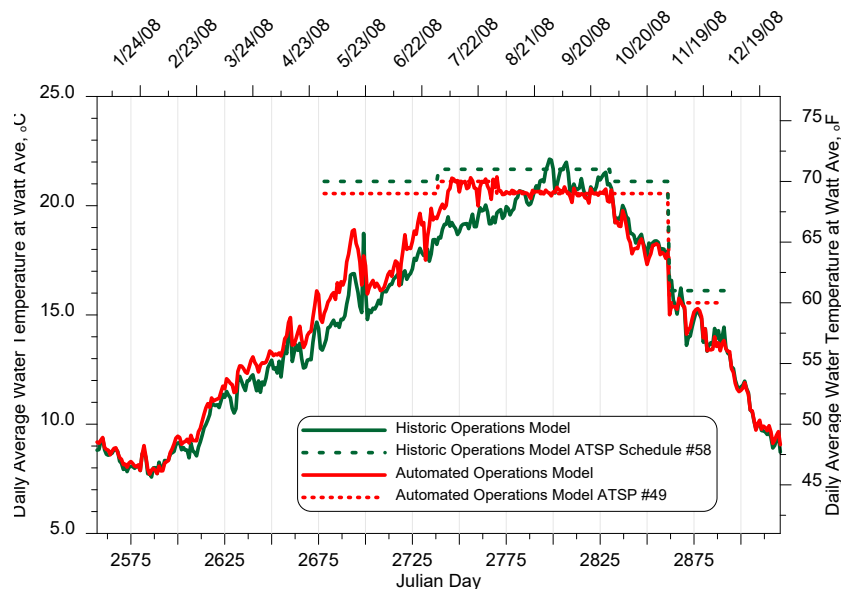
Appendix G3 Figure 7. Flow Chart for Automatic Model Selection of Optimal Temperature Schedule.

Appendix G3 Folsom Reservoir CE-QUAL-W2 Water Temperature Model



Appendix G3 Figure 8

Comparison of Historical Versus Automated Water Temperature Model Shutter Operations below Folsom Dam, 2008 (dark green lines represent historical operation of the three shutters; red lines represent automated operations of the three shutters.)



Appendix G3 Figure 9.

Comparison of Historical Versus Automated Model Operations for Watt Avenue Water Temperature, 2008. (Note: These results were obtained by using a combination of the CE-QUAL-W2 model and an American River water temperature regression between Folsom Dam and Watt Avenue).

APPENDIX G4

LOWER AMERICAN RIVER WATER TEMPERATURE REGRESSION MODELS

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List of Acronyms

ATSP	Automated Temperature Selection Procedure
CDEC	California Data Exchange Center
CIMIS	California Irrigation Management Information System
FOL	Folsom
FSC	Folsom South Canal
LAR	Lower American River
MET	meteorological
RM	river mile
TCD	temperature control device

Introduction

This appendix documents a multiple regression modeling approach for predicting daily average water temperature in the Lower American River (LAR) based on air temperature, Nimbus discharge to the LAR, and Folsom Dam release water temperature. Water temperature regression equations were developed for the LAR at Hazel and Watt Avenues and at any river mile location along the LAR between Nimbus Dam and the confluence with the Sacramento River. The regression relationships are suitable to be used in a variety of ways to predict LAR water temperatures, but were specifically developed to be used in combination with the Folsom Reservoir CE-QUAL-W2 Temperature Model (Appendix G4) to iterate between Automated Temperature Selection Procedure (ATSP) schedules (Water Forum 2004; Water Forum 2006) and to analyze the effects of different alternatives on LAR water temperatures.

Lower American River Data Sources

The sources for the discharge, water temperature, and air temperature data used in the regression equations are provided in Appendix G4 Table 1 and the locations of these data sources are shown in Appendix G4 Map 1. All data were quality controlled prior to use in the analyses.

Methods

Regression Equation Input Data

Water temperature regression variables used for the LAR were 1) daily average discharge in the LAR, 2) daily average water temperature below Folsom Dam, 3) daily average air temperature and 4) river mile / river location (Appendix G4 Table 1). The discharge used in the water temperature regressions was calculated by daily-averaging Folsom Dam outflows (California Data Exchange Center ([CDEC] CDEC-FOL) and subtracting the daily average Folsom South Canal Diversion flows (CDEC-FSC). The resulting discharge approximated the daily average flow in the LAR. The water temperature data for Folsom Dam releases were obtained from the U.S. Geological Survey (USGS) gaging station / CDEC station below Folsom Dam (USGS 11446220/ CDEC-AFD). Historical local air temperature data for the LAR were obtained from the California Irrigation Management Information System (CIMIS) meteorological (MET) station at Fair Oaks (CIMIS-131).

Historical water temperature data for the LAR below Lake Natoma were available from three locations: Hazel Avenue (river mile [RM] 22.3); William B Park (RM 13.3); and Watt Avenue (RM 9.2). In addition, some limited water temperature data (limited years) at various locations on the American River were obtained from CBEC, Inc. (Chris Hammersmark, pers. comm.) and used to “spot” validate the regressions.

Multiple Regression Equation Approach

GENERAL

To predict daily average water temperature at Hazel Avenue or Watt Avenue, a multiple regression equation was developed at each location that related daily average water

temperature at that location to daily average flow releases into the LAR, daily average water temperature of Folsom Dam (CDEC-FOL) releases, and local daily average air temperatures (CIMIS-131 at Fair Oaks) for the period 2001–2009¹. To predict daily average water temperature at any river mile on the LAR, the river mile water temperature regression included the river mile of each water temperature station (Hazel Avenue, William B. Pond, Watt Avenue) in the dataset as an additional parameter.

The daily average water temperature regressions were developed for each month of the year. The monthly approach helped account for seasonal variables not included in the regressions (e.g., solar radiation). The regression relationships were, however, designed to predict daily water temperatures for any day of the year. To do that, the regression equation monthly coefficients and constants are linearly interpolated between the monthly values (with monthly values centered at the middle of each month) to obtain daily regression coefficients for each day of the year.

WATER RELEASE LAG TIME

When water is released from Folsom Dam, it takes between 1 and 8 days for the water to travel through Lake Natoma, be released from Nimbus Dam, and reach Watt Avenue, depending on the flow rate. When flows or the water temperature of Folsom Dam releases were relatively steady from day-to-day, incorporating a release lag time into the regression equations did not significantly increase the accuracy of the regression equations. Conversely, if releases, particularly the water temperature of the releases, changed significantly from day-to-day (e.g., water from different reservoir levels), incorporating the water release lag time into the regression was beneficial. For the Watt Avenue regression, which was specifically intended to be used in conjunction with the Folsom Reservoir CE-QUAL-W2 model to update Folsom Reservoir temperature control device (TCD) operations and meet ATSP schedules on a daily basis, a version of the regression equations was developed that incorporated the released water lag time.

A mathematical relationship for calculating lag time between Folsom Dam and Watt Avenue was developed by analyzing hydrodynamic results from the CE-QUAL-W2 model of Lake Natoma (Technical Memorandum 6 Lake Natoma CE-QUAL-W2 Model and Calibration Report) and the HecRas model of the Lower American (Chris Hammersmark, pers. comm.). The relationship is shown in Appendix G4 Figure 1. The equation is as follows²:

$\text{Lag time (days)} = 3966.8 * (35.314 * \text{Flow(cms)})^{(-0.944)}$	(1)
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Based on sensitivity analyses, it was determined that the best-fit Watt Avenue temperature regression included lagging only the Folsom release temperature using Equation 1. Time lagging other variables (flow rate, air temperature) was not beneficial to the regression.

¹ The location of the gaging station at Watt Avenue moved in 2009; only data prior to this were used in the development of the regression relationships.

² Final equation provided by Chris Hammersmark (CBEC, Inc.) by email to Vanessa Martinez (Cardno) on 1/29/2015

Results

Hazel Avenue

The monthly constants and regression coefficients used to predict daily average water temperature for Hazel Avenue are shown in Appendix G4 Table 2. The overall regression performance is shown in Appendix G4 Figure 2 by plotting measured versus regression-based average daily temperatures at Hazel Avenue. A time series comparison of the predicted and measured water temperatures from 2001 to 2018 at Hazel Avenue is shown in Appendix G4 Figure 3. Flow rate influenced water temperature in the later spring/summer, but had less effect on water temperature in winter/early spring months.

Watt Avenue

The monthly constants and regression coefficients used to predict daily average water temperatures at Watt Avenue are shown in Appendix G4 Table 3 for the Folsom release temperature time lagged regression and in Appendix G4 Table 4 for the “without time lag” regression. The overall regression performance (with lagged release temperature) is shown in Appendix G4 Figure 4 by plotting measured versus regression-based average daily temperatures at Watt Avenue. A time series comparison of the predicted and measured water temperatures from 2001 to 2018 at Watt Avenue is shown in Appendix G4 Figure 5. Discharge influenced water temperature in the later spring/summer, but had less effect on water temperature in winter/early spring months.

River Mile Locations

The monthly constants and regression coefficients used to predict daily average water temperatures at any specified RM along the LAR are shown in Appendix G4 Table 5. The overall regression performance is shown in Appendix G4 Figure 6 by plotting measured versus regression-based average daily temperatures at river mile locations where data are available. Predicted (regression-based) water temperatures at three river mile locations corresponding to Hazel Avenue, William B Pond Park and Watt Avenue for 2001 through 2018 is shown in Appendix G4 Figure 7. Model versus data comparisons are shown at these same three locations along the Lower American River for 2001-2018 in Appendix G4 Figures 8, 9, and 10. Similar to the Hazel Avenue and Watt Avenue regressions, flow rate influenced water temperature more in the spring/summer months than in the winter months, particularly in the lower sections of the reach.

APPENDIX G4
TABLES

Appendix G4 Lower American River Water Temperature Regression Models

Appendix G4 Table 1. Data Sources for the Lower American River Water Temperature Regression Analyses.

Name	Data Collected	Operator	Station No.	Location		Period of Record Available	Period of Record Used in Regression Analyses
				Lat.	Long.		
Flow Stations							
Folsom Lake outflows	Daily Average Flow	US Bureau of Reclamation/ CDEC	CDEC-FOL	38.683	121.183	2/1/1995-present	1/1/2001-8/31/2009
Folsom South Canal	Diversion Flow	US Bureau of Reclamation/ CDEC	CDEC-FSC	38.650	121.183	7/11/2001-present	7/11/2001-8/31/2009
Water Temperature Stations							
American R. below Folsom Dam	Daily Water Temperature	USGS/ CDEC	USGS 11446220/ CDEC-AFD	38.688	121.166	10/24/1998-present	1/1/2001-8/31/2009
American R. at Hazel Ave. Bridge	Daily Water Temperature	USGS/ CDEC	USGS 11446220/ CDEC-AHZ	38.636	121.224	6/29/2001-present	6/29/2001-8/31/2009
American R. at William B. Pond Park	Daily Water Temperature	USGS/ CDEC	USGS 11446700/ CDEC-AWP	38.591	121.332	1/10/2001-present	10/1/2007-8/31/2009
American R. below Watt Ave. Bridge	Daily Water Temperature	USGS/ CDEC	USGS 11446980/ CDEC-AWB	38.567	121.387	11/30/1998-present	1/1/2001-8/31/2009
Meteorological Station							
CIMIS at Fair Oaks	Daily Average Air Temperature	CIMIS	CIMIS at Fair Oaks	38.650	121.218	4/18/1997-present	4/18/1997-8/31/2009

Abbreviations:

CIMIS: California Irrigation Management Information System

USGS: United States Geological Survey

CDEC: California Data Exchange Center

¹ Location of gaging station was moved in 2009; only data prior to this were used in the development of the regressions.

**Appendix G4 Lower American River
Water Temperature Regression Models**

Appendix G4 Table 2. Coefficients Used for the Multiple Regression for Predicting Lower American River Average Daily Water Temperature at Hazel Avenue

Month	Constant	A	B	C	R ²
Predicted Water Temp = Const. + A(Ave Air Temp) + B(Ave Water Temp below Folsom) + C(Log [Ave Flow])					
Jan	1.9464	0.0134	0.9398	-0.6182	0.838
Feb	3.0658	0.0634	0.8055	-0.8259	0.665
Mar	4.8402	0.0304	0.8408	-1.5306	0.859
Apr	8.0496	0.0490	0.6082	-1.7821	0.854
May	7.5008	0.0356	0.8387	-2.4903	0.934
Jun	9.2531	0.0257	0.7968	-2.9129	0.931
Jul	7.0760	-0.0156	0.8855	-1.9229	0.885
Aug	9.1246	0.0316	0.7682	-2.6583	0.751
Sep	9.7662	0.0845	0.6947	-3.2732	0.841
Oct	9.7572	0.0595	0.5984	-2.1663	0.865
Nov	8.1662	0.1901	0.5111	-1.8145	0.673
Dec	1.5390	0.0293	0.8908	-0.2236	0.925

Regression Variables:

Ave Air Temp = Daily average air temperature at CIMIS at Fair Oaks (CIMIS-131) (°C)

Ave Water Temp below Folsom = Daily water temperature below Folsom Data at USGS/CDEC station (USGS gage no. 11446220/CDEC station AFD) (°C)

Ave Flow = Daily-averaged hourly flow below Folsom Reservoir (CDEC station FOL) – South Canal Diversion (CDEC station FSC) (cubic meters per second [cms])

Predicted Temp = Lower American River at Hazel Avenue (°C)

Appendix G4 Lower American River Water Temperature Regression Models

Appendix G4 Table 3. Coefficients Used for the Multiple Regression for Predicting Lower American River Average Daily Water Temperature at Watt Avenue with Time Lagged Water Temperature.

Month	Constant	A	B	C	R ²
Predicted Water Temp = Const. + A(Ave Air Temp) + B(Lagged Ave Water Temp below Folsom) + C(Log[Ave Flow])					
Jan	1.818763	0.112641331	0.73259158	-0.147712419	0.57
Feb	3.539369	0.205141039	0.775380578	-1.499333534	0.45
Mar	4.987294	0.168695197	0.961301503	-2.512509452	0.91
Apr	8.855085	0.158340582	0.718969803	-3.034734768	0.91
May	11.86438	0.138534042	0.742039709	-4.371801735	0.95
Jun	12.62007	0.086480404	0.800890216	-4.43688051	0.95
Jul	13.08971	0.049031621	0.682266998	-3.293149439	0.94
Aug	16.90057	0.072653186	0.622758693	-5.222428569	0.91
Sep	15.26052	0.182748074	0.454786001	-4.508935727	0.84
Oct	2.757994	0.240015186	0.668043404	-0.344582923	0.82
Nov	-1.8198	0.231285327	0.828705359	0.703644524	0.96
Dec	-1.35138	0.167591589	0.685635625	1.786194262	0.87

Regression Variables:

Ave Air Temp = Daily average air temperature at CIMIS at Fair Oaks (CIMIS-131) (°C)

Ave Water Temp below Folsom = Daily water temperature below Folsom Data at USGS/CDEC station (USGS gage no. 11446220/ CDEC station AFD) (°C)

Ave Flow = Daily-averaged hourly flow below Folsom Reservoir (CDEC station FOL) – South Canal Diversion (CDEC station FSC) (cubic meters per second [cms])

Low Flows – water temperatures at low flows were modeled with HEC-5Q as described in the text.

Predicted Temp = Lower American River at Watt Avenue (°C)

¹ Low r-squared values are the result of a narrow range in flows in these months. These regressions represent the average water temperature.

Appendix G4 Lower American River Water Temperature Regression Models

Appendix G4 Table 4. Coefficients Used for the Multiple Regression for Predicting Lower American River Average Daily Water Temperature at Watt Avenue without Time Lagged Water Temperature.

Month	Constant	A	B	C	R ²
Predicted Water Temp = Const. + A(Ave Air Temp) + B(Ave Water Temp below Folsom) + C(Log[Ave Flow])					
Jan	1.96471	0.112234	0.794124	-0.4599	0.59
Feb	2.807373	0.19099	0.859157	-1.40971	0.53
Mar	4.540722	0.158975	0.945175	-2.20309	0.88
Apr	8.476506	0.146524	0.686462	-2.57868	0.92
May	10.9384	0.15328	0.746008	-4.05553	0.93
Jun	12.99852	0.072963	0.790918	-4.44247	0.92
Jul	13.53072	0.058166	0.665339	-3.51614	0.87
Aug	16.56891	0.096824	0.602078	-5.15153	0.84
Sep	13.88743	0.186215	0.494713	-4.14767	0.85
Oct	3.846972	0.205693	0.685195	-0.77901	0.87
Nov	-4.20459	0.209982	0.960059	1.231348	0.93
Dec	1.040451	0.161682	0.754327	0.099866	0.89

Regression Variables:

Ave Air Temp = Daily average air temperature at CIMIS at Fair Oaks (CIMIS-131) (°C)

Ave Water Temp below Folsom = Daily water temperature below Folsom Data at USGS/CDEC station (USGS gage no. 11446220/ CDEC station AFD) (°C)

Ave Flow = Daily-averaged hourly flow below Folsom Reservoir (CDEC station FOL) – South Canal Diversion (CDEC station FSC) (cubic meters per second [cms])

Predicted Temp = Lower American River at Watt Avenue (°C)

¹Low r-squared values are the result of a narrow range in flows in these months. These regressions represent the average water temperature.

Appendix G4 Lower American River Water Temperature Regression Models

Appendix G4 Table 5. Coefficients Used for the River Mile Multiple Regression to Predict Average Daily Water Temperature at Specified Locations along the Lower American River.

Month	Constant	A	B	C	D	R ²
Predicted Water Temp = Constant + A(Ave Air T) + B(Ave Water T below Folsom) + C(Log[Ave Flow]) + D(RM)						
Jan	2.235497	0.055418	0.825738	-0.52645	0.008751	0.62
Feb	3.560284	0.136864	0.811086	-1.0953	-0.03644	0.56
Mar	6.527125	0.093312	0.85848	-1.95242	-0.08413	0.84
Apr	10.22137	0.100764	0.627146	-2.31341	-0.09348	0.87
May	10.58013	0.109122	0.845379	-3.40188	-0.12297	0.92
Jun	14.22662	0.048251	0.753645	-3.97143	-0.12483	0.92
Jul	13.63687	0.019043	0.760111	-3.24759	-0.1279	0.89
Aug	16.68644	0.062428	0.614724	-4.15399	-0.13937	0.84
Sep	14.90653	0.133762	0.548928	-4.02447	-0.11092	0.86
Oct	8.962731	0.133697	0.569276	-1.72354	-0.03133	0.81
Nov	7.706451	0.269051	0.453618	-1.73661	0.008454	0.68
Dec	0.97066	0.095728	0.836114	-0.16038	0.022549	0.90

Regression Variables:

Ave Air Temp = Daily average air temperature at CIMIS at Fair Oaks (CIMIS-131) (°C)

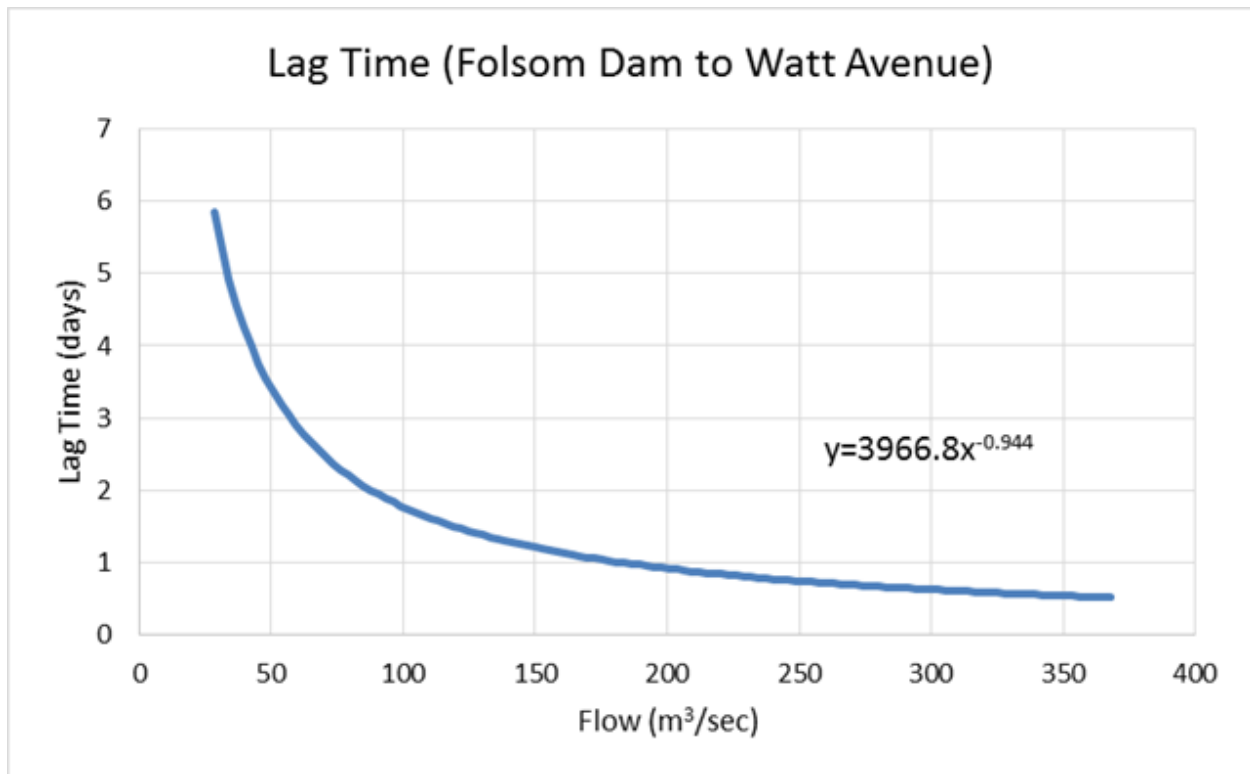
Ave Water Temp below Folsom = Daily water temperature below Folsom Data at USGS/CDEC station (USGS gage no. 11446220/ CDEC station AFD) (°C)

Ave Flow = Daily-averaged hourly flow below Folsom Reservoir (CDEC station FOL) – South Canal Diversion (CDEC station FSC) (cubic meters per second [cms])

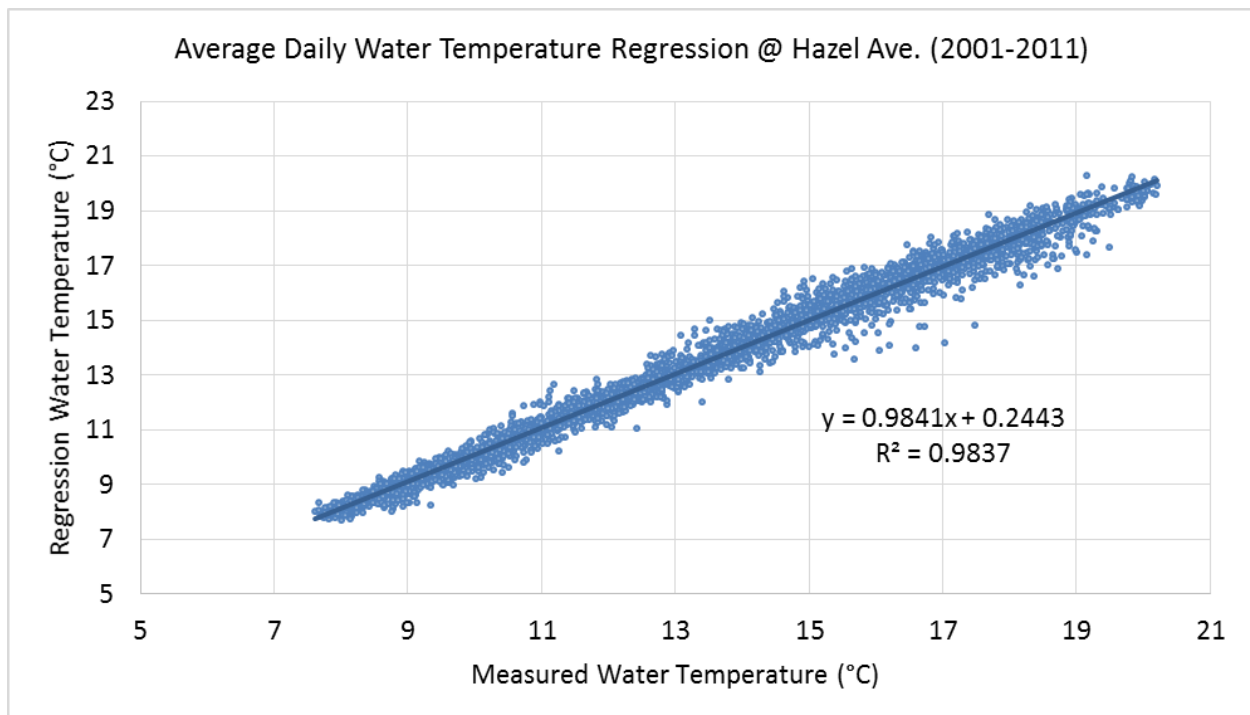
RM = River Mile

Predicted Temp = Lower American River at RM "X" (°C)

APPENDIX G4
FIGURES

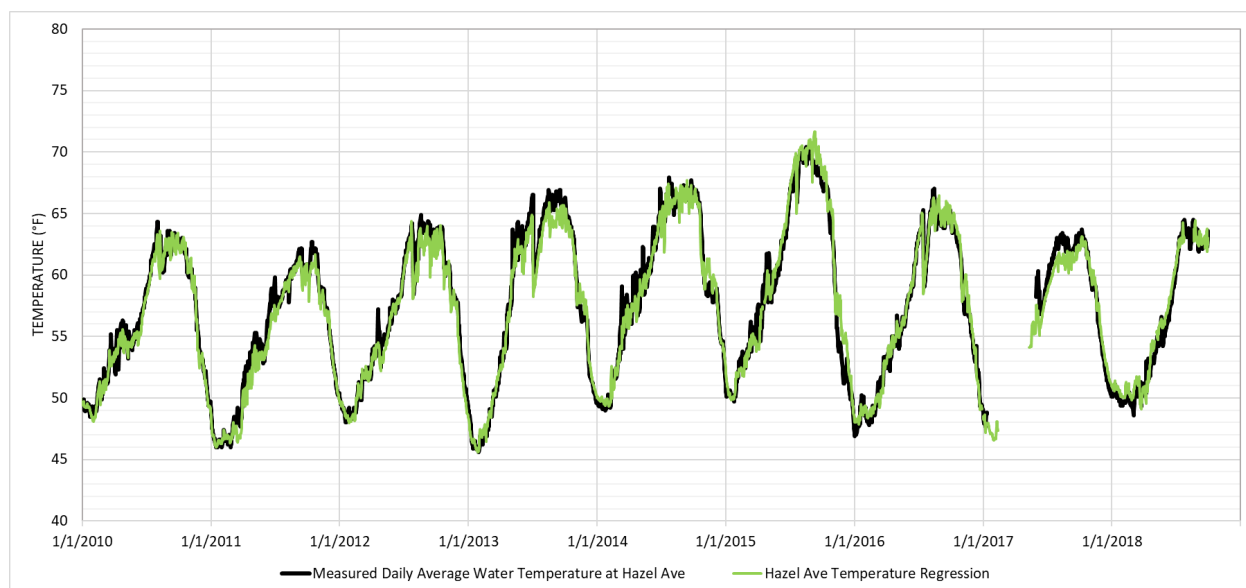
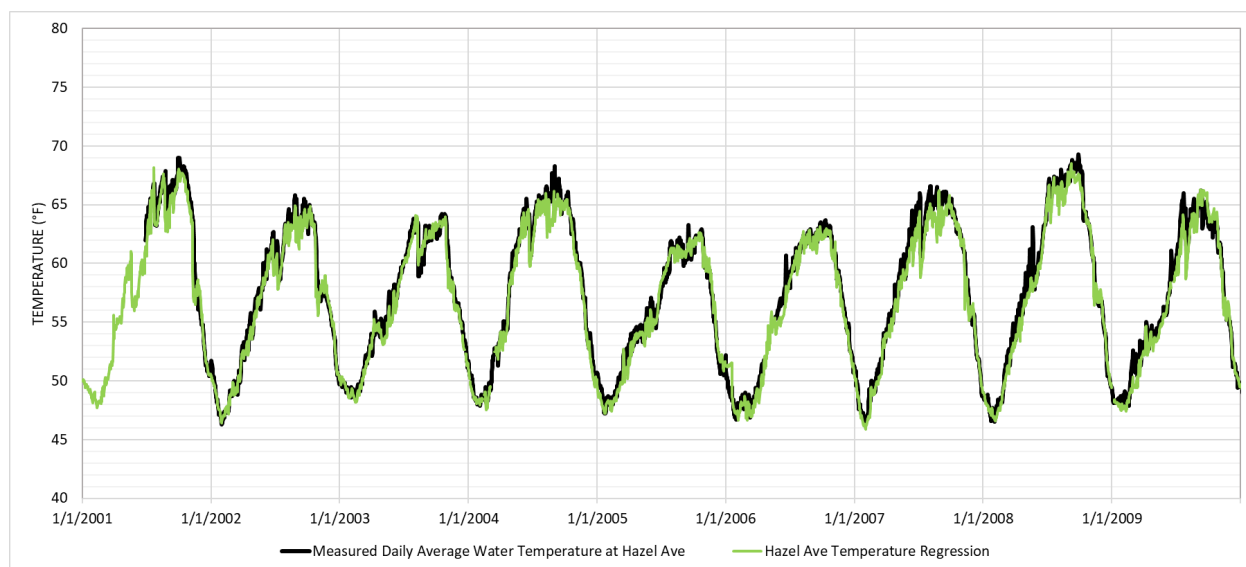


Appendix G4 Figure 1. Flow Travel (Lag) time to Watt Avenue versus Flow.

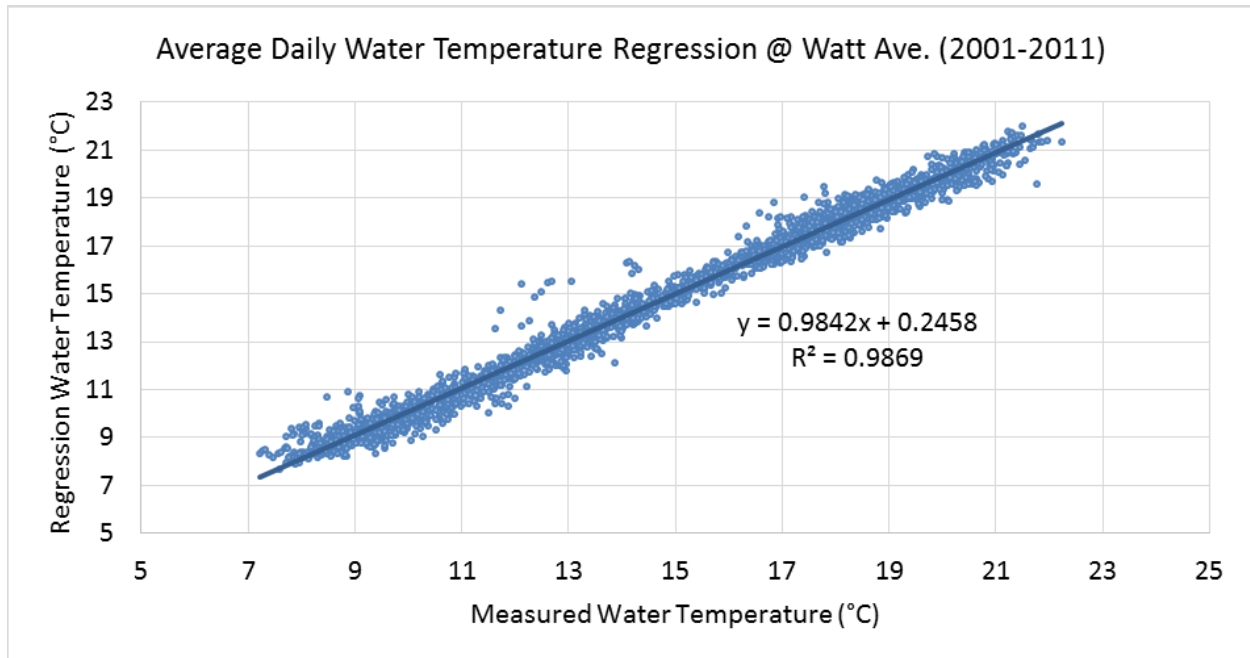


Appendix G4 Figure 2. Measured versus Modeled (Regression) Average Daily Water Temperature at Hazel Avenue.

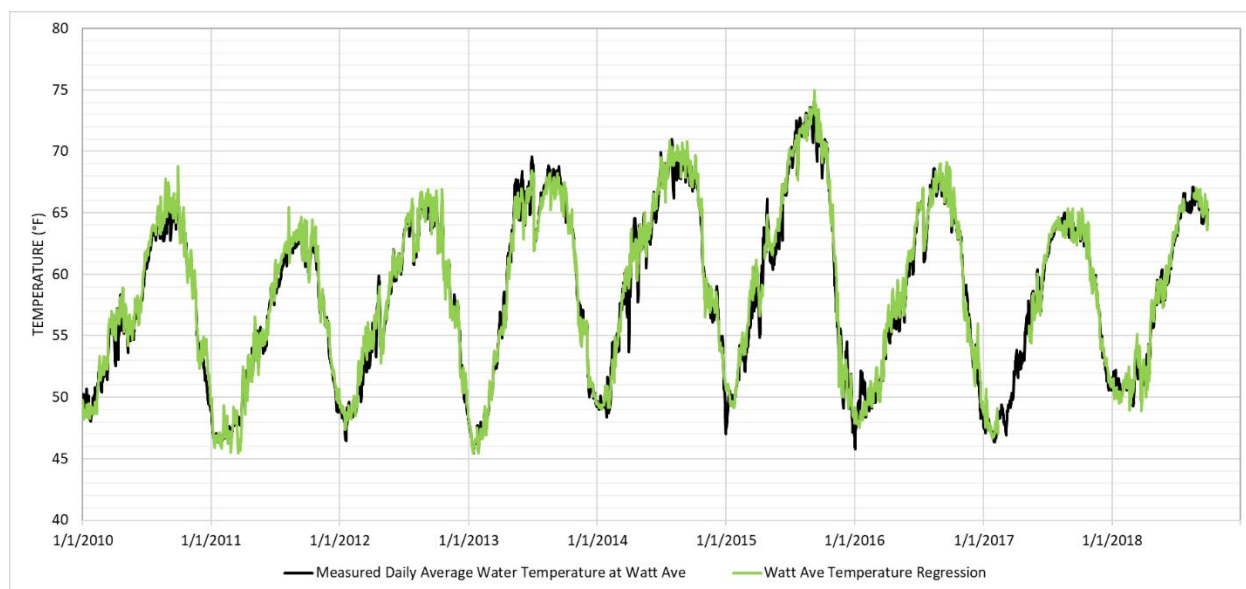
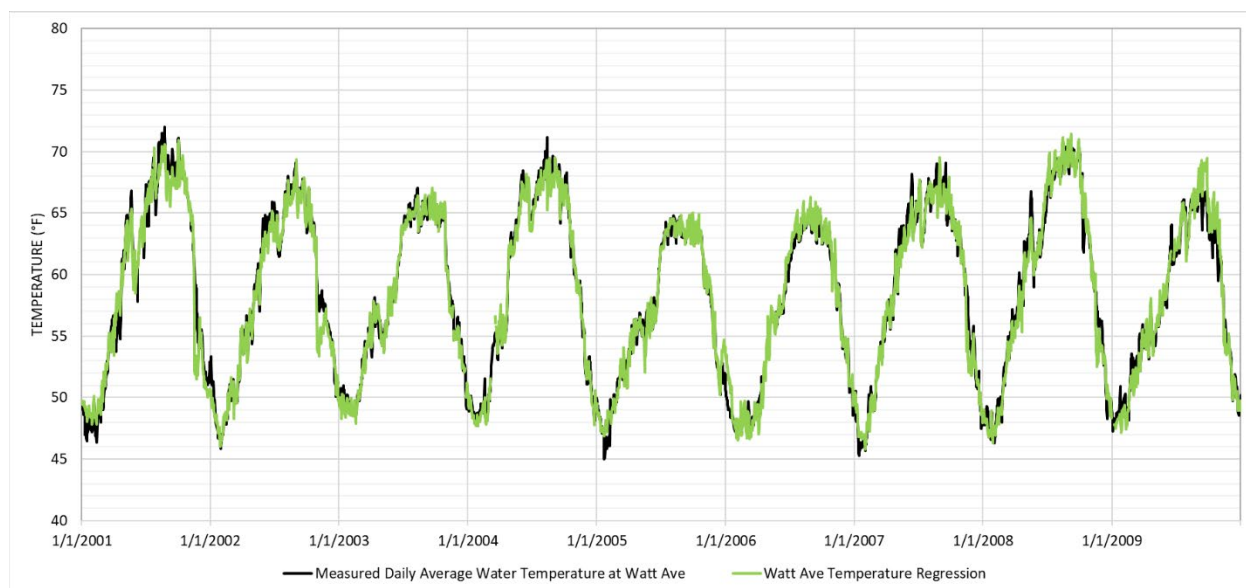
Appendix G4 Lower American River Water Temperature Regression Models



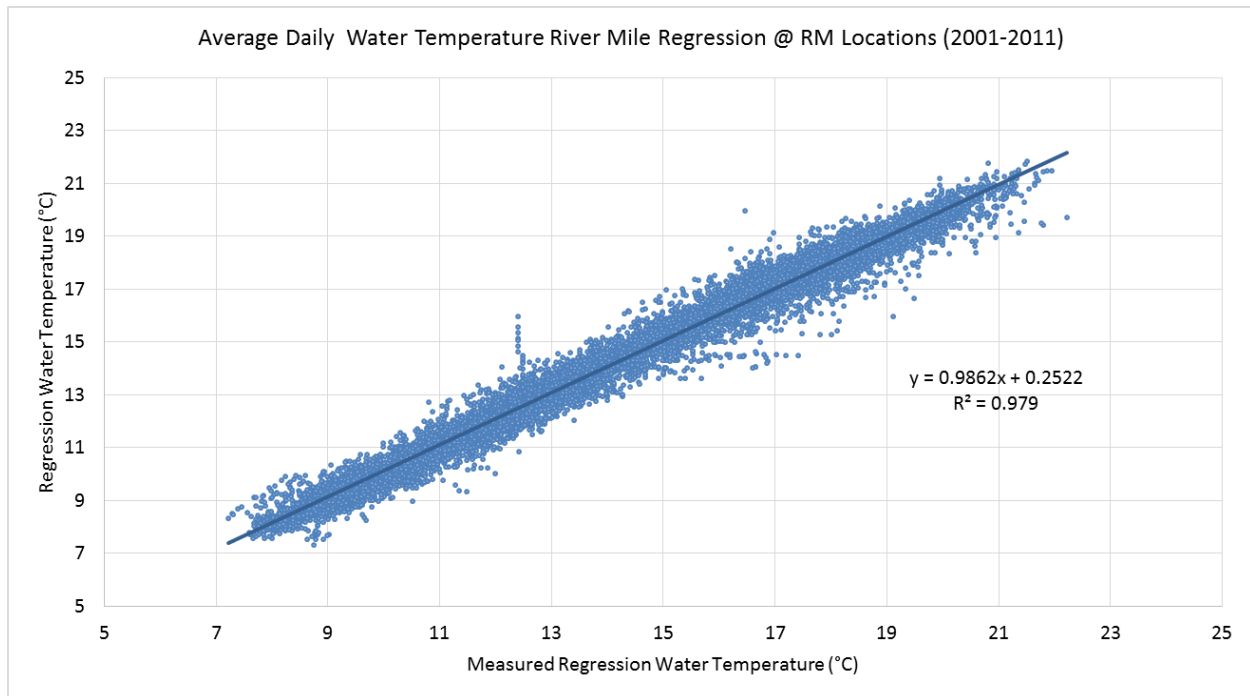
Appendix G4 Figure 3. Comparison of Measured and Modeled (Regression) Water Temperature on the Lower American River at Hazel Avenue (2001-2018): 2001-2009 (top), and 2010-2018 (bottom).



Appendix G4 Figure 4. Measured versus Modeled (Regression) Average Daily Water Temperature at Watt Avenue.

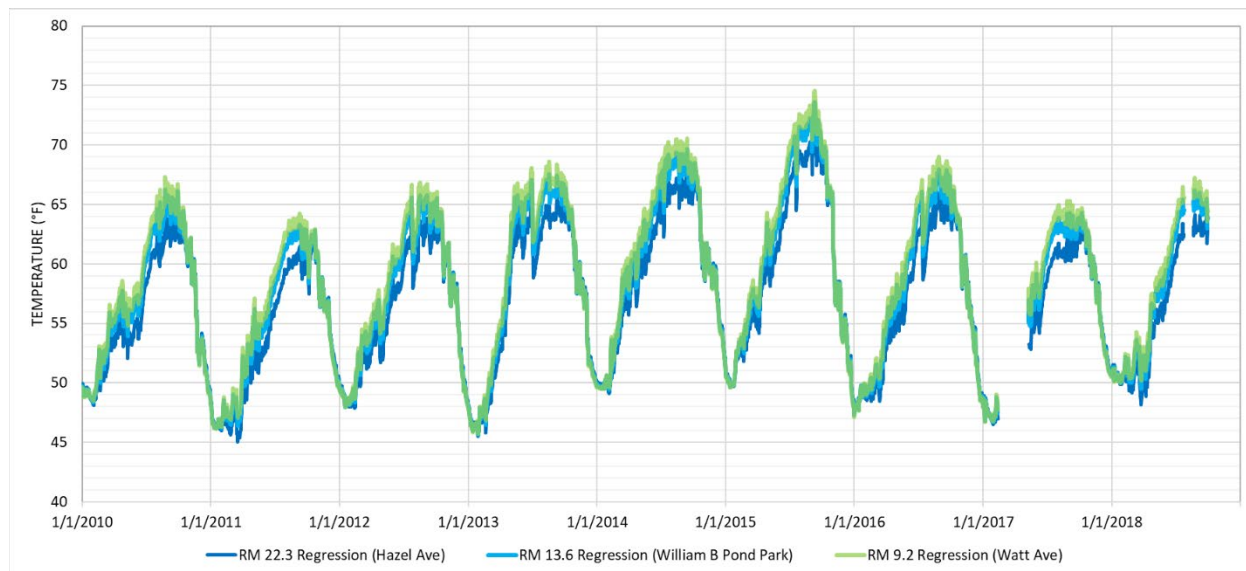
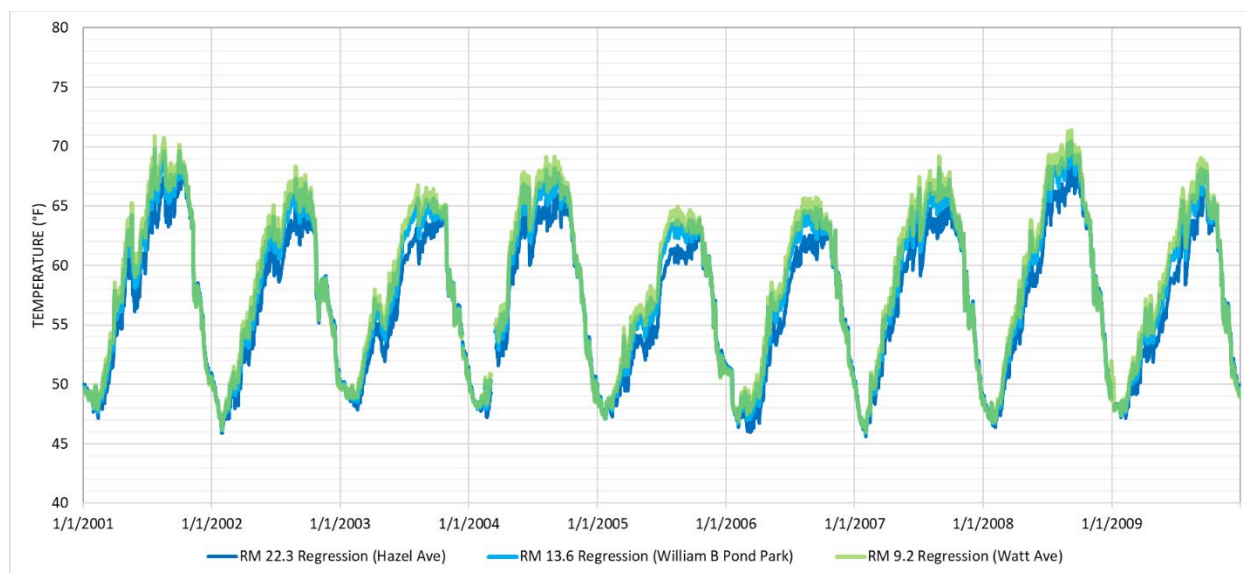


Appendix G4 Figure 5. Comparison of Measured and Modeled (Regression) Water Temperature on the Lower American River at Watt Avenue (2001-2018): 2001-2009 (top), and 2010-2018 (bottom).



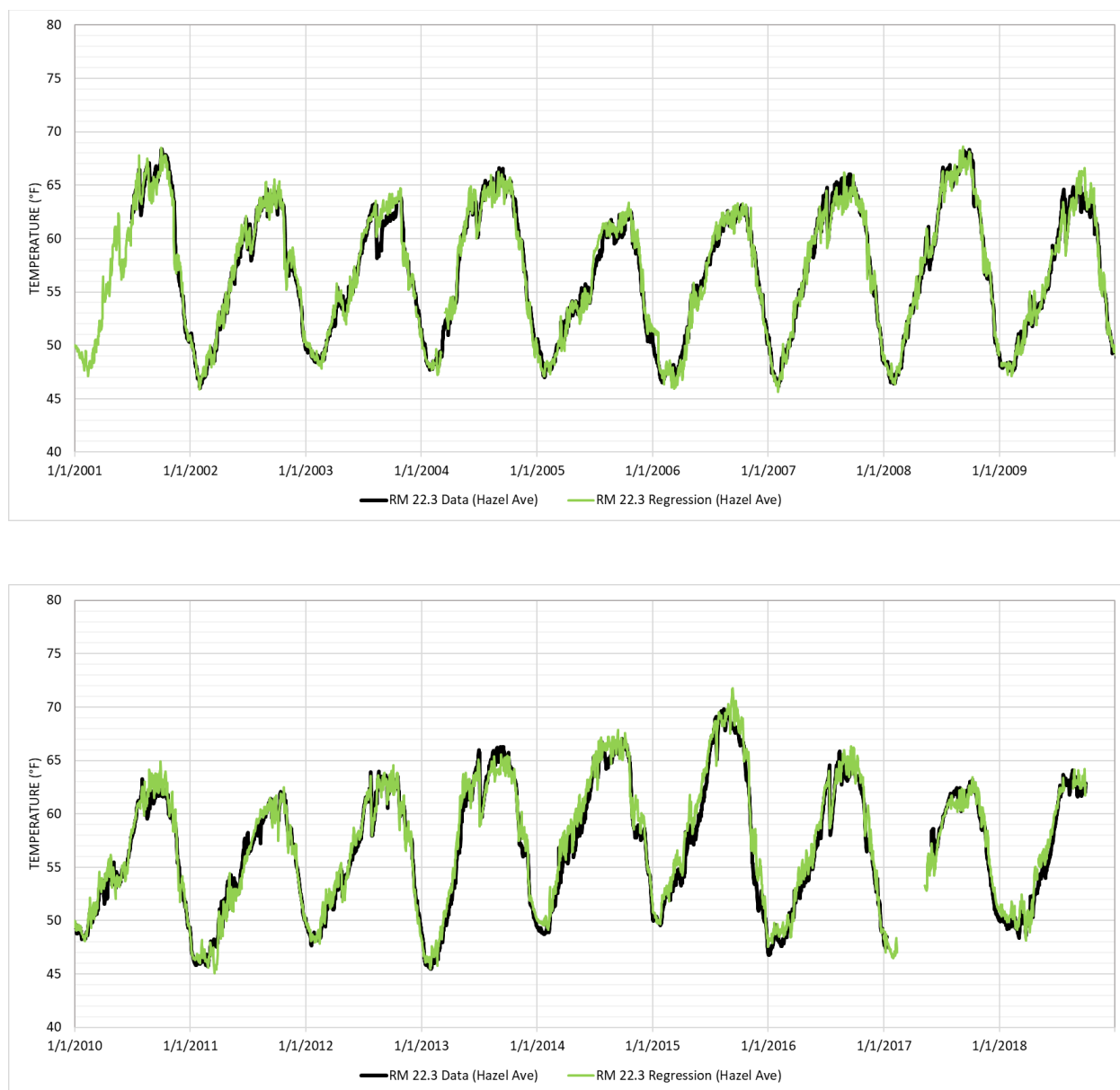
Appendix G4 Figure 6. Measured versus Modeled (Regression) Average Daily Water Temperatures at Various River Mile Locations.

Appendix G4 Lower American River Water Temperature Regression Models



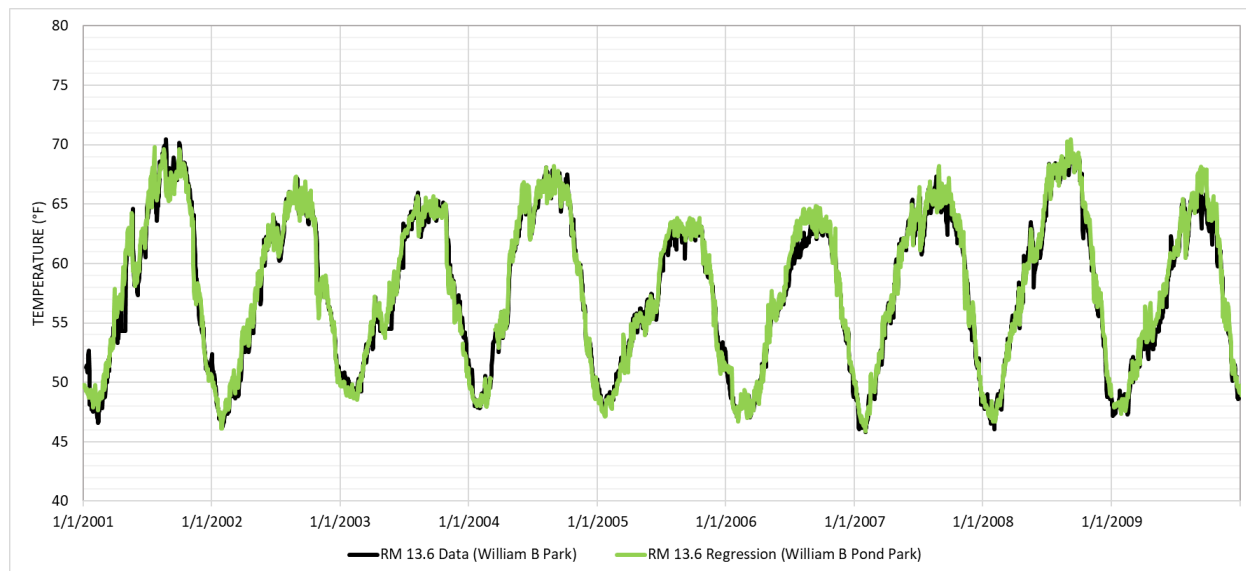
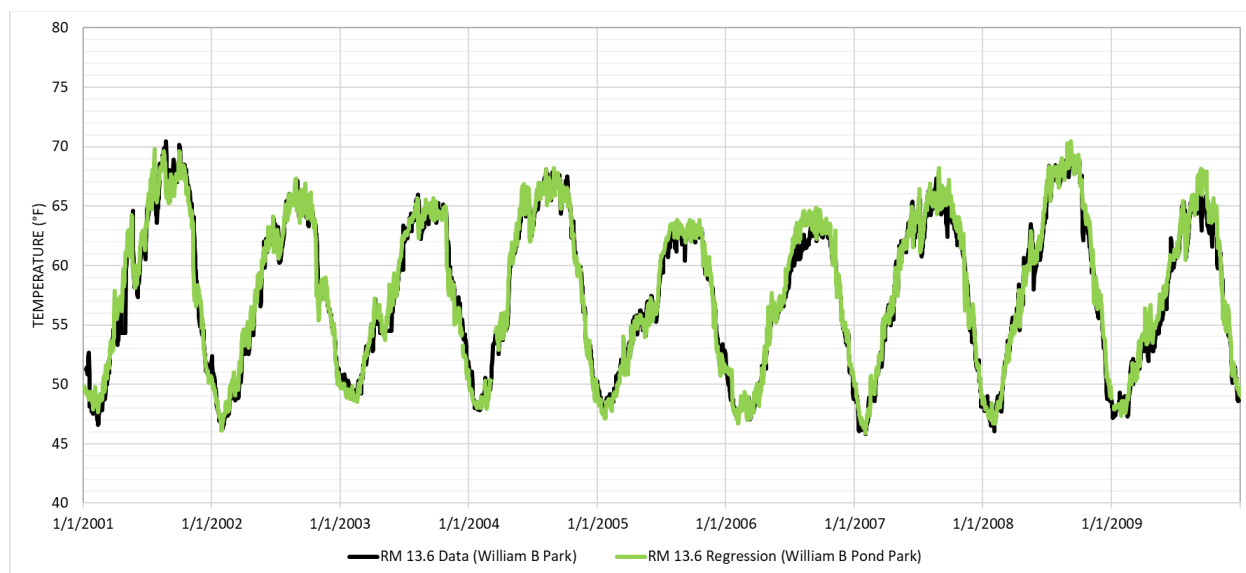
Appendix G4 Figure 7. Comparison of Modeled (River Mile Regression) Water Temperatures at three river mile locations along on the Lower American River (2001-2018): 2001-2009 (top), and 2010-2018 (bottom).

Appendix G4 Lower American River Water Temperature Regression Models

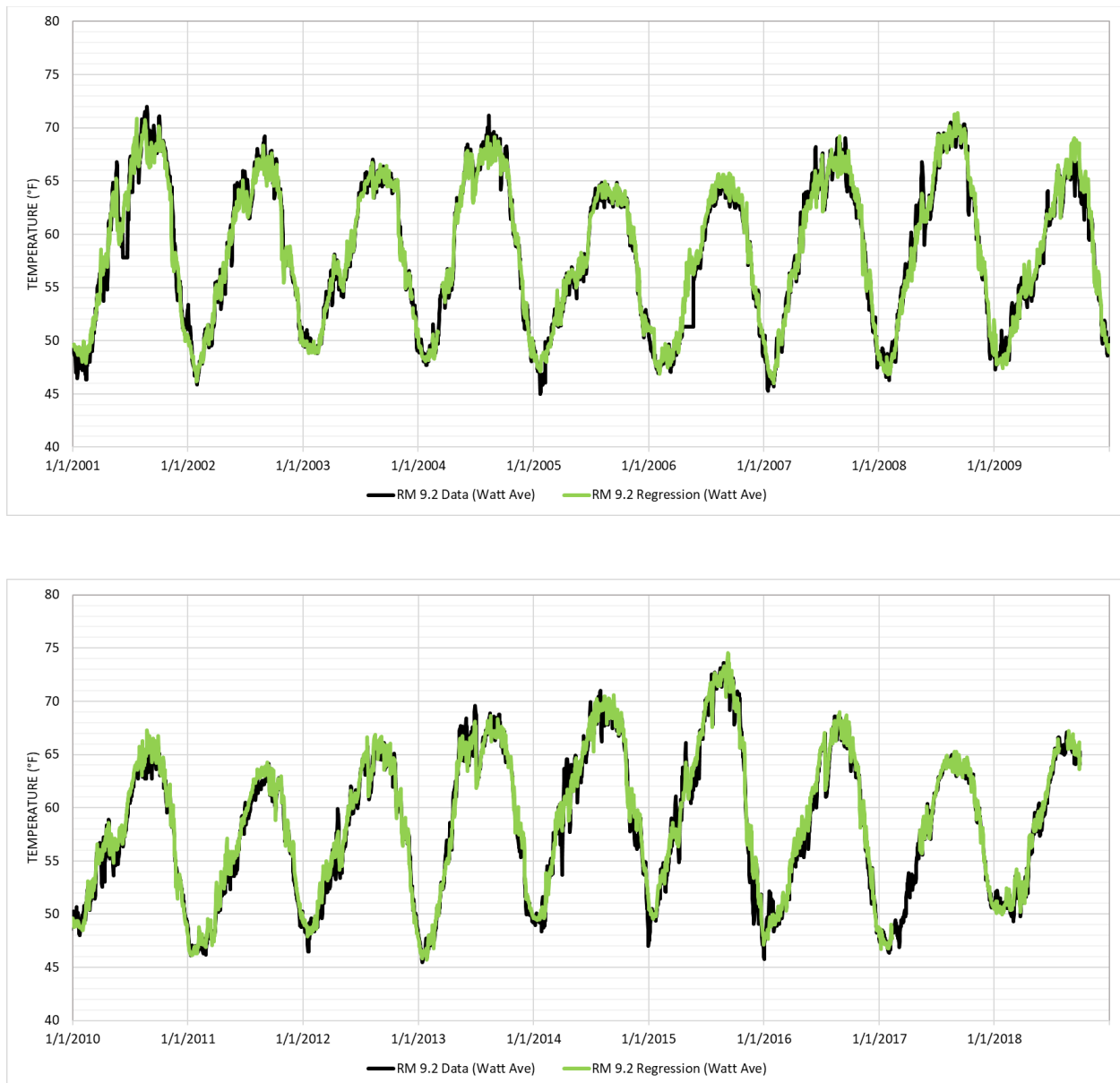


Appendix G4 Figure 8.

Comparison of Measured and Modeled (River Mile Regression) Water Temperature on the Lower American River at river mile 22.3 (Hazel Avenue) (2001-2018): 2001-2009 (top), and 2010-2018 (bottom).



Appendix G4 Figure 9. Comparison of Measured and Modeled (River Mile Regression) Water Temperature on the Lower American River at river mile 13.6 (William B Pond Park) (2001-2018): 2001-2009 (top), and 2010-2018 (bottom).

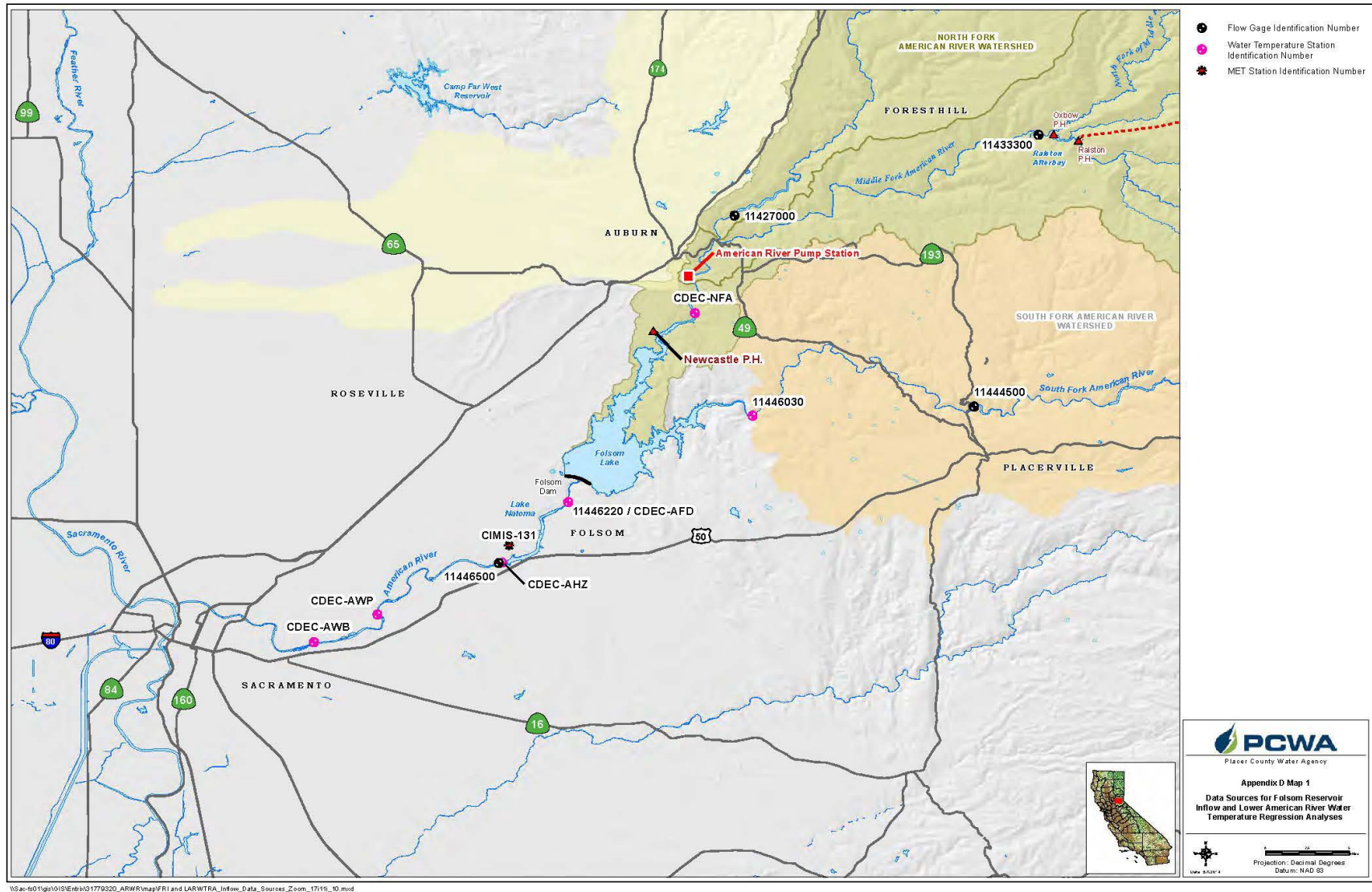


Appendix G4 Figure 10.

Comparison of Measured and Modeled (River Mile Regression) Water Temperature on the Lower American River at river mile 9.2 (Watt Avenue) (2001-2018): 2001-2009 (top), and 2010-2018 (bottom).

**APPENDIX G4
MAP**

Appendix G4 Lower American River Water Temperature Regression Models



Appendix G4 Map 1. Data Source Locations